

Table LWG-9. Lower Granite spillway pattern for fish passage (with RSW operating at pool elevation 734).

Spill Bay								Total Stops	Total Spill
1	2	3	4	5	6	7	8		
3.5	0	0	0	0	0	1	2	6.5	11.9
3.5	0	0	0	1	0	1	2	7.5	13.6
3.5	0	1	0	1	0	1	2	8.5	15.3
3.5	0	1	0	1	1	1	2	9.5	17.0
3.5	0	1	1	1	1	1	2	10.5	18.7
3.5	1	1	1	1	1	1	2	11.5	20.4
3.5	1	1	2	1	1	1	2	12.5	22.2
3.5	1	1	2	2	1	1	2	13.5	24.0
3.5	1	1	2	2	2	1	2	14.5	25.8
3.5	1	2	2	2	2	1	2	15.5	27.7
3.5	2	2	2	2	2	1	2	16.5	29.5
3.5	2	2	2	2	2	2	2	17.5	31.3
3.5	2	2	3	2	2	2	2	18.5	36.6
3.5	2	2	3	3	2	2	2	19.5	35.0
3.5	2	2	3	3	3	2	2	20.5	36.9
3.5	2	3	3	3	3	2	2	21.5	38.7
3.5	3	3	3	3	3	2	2	22.5	40.6
3.5	3	3	4	3	3	2	2	23.5	42.4
3.5	3	3	4	4	3	2	2	24.5	44.3
3.5	3	3	4	4	4	2	2	25.5	46.2
3.5	3	4	4	4	4	2	2	26.5	48.0
3.5	4	4	4	4	4	2	2	27.5	49.9
3.5	4	4	4	4	4	2	3	28.5	51.7
3.5	4	4	4	4	4	3	3	29.5	53.6
3.5	4	4	5	4	4	3	3	30.5	55.5
3.5	4	4	5	5	4	3	3	31.5	57.3
3.5	4	4	5	5	5	3	3	32.5	59.2
3.5	4	5	5	5	5	3	3	33.5	61.0
3.5	5	5	5	5	5	3	3	34.5	62.9
3.5	5	5	5	5	5	3	4	35.5	64.8
3.5	5	5	5	5	5	4	4	36.5	66.6
3.5	5	5	6	5	5	4	4	37.5	68.5
3.5	5	5	6	6	5	4	4	38.5	70.3

Note: Minimum involuntary spill with RSW operating is 11.5 kcfs.

Note: At approximately 3.5 stops, the tainter gate no longer regulates flow through the RSW. The tainter gate should be raised at least 9 stops so the gate does not interfere with the spillbay flow.

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Note: Spillbay discharge at pool elevation 734:

<u>Stops</u>	<u>Discharge (kcfs)</u>
<u>(without RSW in place)</u>	
1	1.7
2	3.5
3	5.4
4	7.2
5	9.1
6	11.0
7	12.8
8	14.7
<u>(with RSW in place)</u>	
RSW 3.5 stops or more	6.7

Table LWG-10. Lower Granite spillway pattern for fish passage (RSW NOT operating, pool elevation 734).

Spillbay Stops								Total Stops	Total Spill (kcfs)
1 (RSW)	2	3	4	5	6	7	8		
<i>Closed</i>	1	1			1	1	2	6.0	10.3
<i>Closed</i>	1	1			1	2	2	7.0	12.1
<i>Closed</i>	2	1			1	2	2	8.0	13.9
<i>Closed</i>	2	2			1	2	2	9.0	15.7
<i>Closed</i>	2	2	1		1	2	2	10.0	17.4
<i>Closed</i>	2	2	1	1	1	2	2	11.0	19.1
<i>Closed</i>	2	2	2	1	1	2	2	12.0	20.9
<i>Closed</i>	2	2	2	1	2	2	2	13.0	22.7
<i>Closed</i>	2	2	2	2	2	2	2	14.0	24.5
<i>Closed</i>	2	2	2	2	2	2	3	15.0	26.4
<i>Closed</i>	2	2	2	2	2	3	3	16.0	28.3
<i>Closed</i>	3	2	2	2	2	3	3	17.0	30.2
<i>Closed</i>	3	3	2	2	2	3	3	18.0	32.1
<i>Closed</i>	3	3	3	2	2	3	3	19.0	34.0
<i>Closed</i>	3	3	3	2	3	3	3	20.0	35.9
<i>Closed</i>	3	3	3	3	3	3	3	21.0	37.8
<i>Closed</i>	3	3	3	3	3	3	4	22.0	39.6
Closed	3	3	3	3	3	4	4	23.0	41.4
<i>Closed</i>	4	3	3	3	3	4	4	24.0	43.2
<i>Closed</i>	4	4	3	3	3	4	4	25.0	45.0
Closed	4	4	4	3	3	4	4	26.0	46.8
<i>Closed</i>	4	4	4	3	4	4	4	27.0	48.6
Closed	4	28.0	50.4						
<i>Closed</i>	4	4	4	4	4	4	5	29.0	52.3
Closed	5	4	4	4	4	4	5	30.0	54.2
<i>Closed</i>	5	4	4	4	4	5	5	31.0	56.1
<i>Closed</i>	5	5	4	4	4	5	5	32.0	58.0
Closed	5	5	5	4	4	5	5	33.0	59.9
<i>Closed</i>	5	5	5	4	5	5	5	34.0	61.8
<i>Closed</i>	5	5	5	5	5	5	5	35.0	63.7
<i>Closed</i>	5	5	5	5	5	5	6	36.0	65.6
<i>Closed</i>	5	5	5	5	5	6	6	37.0	67.5

Notes: Patterns in **bold** were evaluated with the Corps' Lower Granite 1:80 physical general model. These values match preliminary spill patterns for this test condition that were previously sent to RCC via e-mail message on 4/12/02. Values shown in *italics* were added to this expanded table on 6/7/02.

