

FISH OPERATIONS PLAN IMPLEMENTATION REPORT

April 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' April 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in April 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in April displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

¹ Averages reported are consistent with the current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and the Washington TDG criteria adjustments have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented from Monday through Sunday.

The weekly figures begin on March 30 and end on April 26 for the following lower Snake River and lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on March 30 for the lower Snake River and the lower Columbia River projects.

March 30 – April 5	Figures 1 – 4
April 6 – April 12	Figures 5 – 12
April 13 – April 19	Figures 13 – 20
April 20 – April 26	Figures 21 – 28

A. Upper Figure: Displays the average daily %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the Oregon 120%TDG standard modification limit for the tailwater of the dam.
2. The blue dot-dash line represents the Washington 120%TDG criteria adjustment for the tailwater of the dam.
3. The black solid line represents the Washington 115%TDG criteria adjustment for the forebay of the next dam downstream.

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

II. A table is included at the end of the figures that lists the average daily %TDG for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects,

tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the April 2015 Spill Variance Table.³ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour (except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams⁴, which may

³ Involuntary spill conditions appear in the figures, but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

⁴ As specified in the 2015 FOP (p. 14), this applies when the spill level is below 40% of total flow at The Dalles Dam.

range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

April 2015 Operations

The month of April was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the April 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 2.9 MAF (Million Acre Feet) or 64% of average as measured at Lower Granite Dam. For the lower Columbia, the Runoff Processor indicated the April 2015 adjusted volume runoff was below the 30 year average (1981-2010): 11.5 MAF or 83% of average as measured at The Dalles. The monthly precipitation summary for April was well below average at 53% on the Snake River above Ice Harbor Dam and also well below average on the Columbia River above The Dalles Dam at 51%.

During the April 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 20 kcfs, 24 hours/day.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day.

- Lower Monumental Dam - The hourly target spill level was the %TDG cap, 24 hours/day.
- Ice Harbor Dam - The hourly target spill level was 45 kcfs during the daytime and the %TDG cap during the nighttime. From April 10 – 14, the hourly target spill level was 30% of total project outflow, 24 hours/day⁵. Nighttime spill hours are 1800-0500.
- McNary Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- John Day Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level was 100 kcfs, 24 hours/day.

Operational Adjustments

No Operational Adjustments to report.

⁵ Spill operation treatments were rearranged as discussed on page 12 of the 2015 FOP to accommodate a post-construction evaluation of modifications made to Ice Harbor spillbay 2 to improve juvenile fish passage survival. This evaluation is described in FPP Appendix A, and the rearrangement of spill operation treatments was further coordinated through the FPOM on April 9.

April 2015 Spill Variance Table

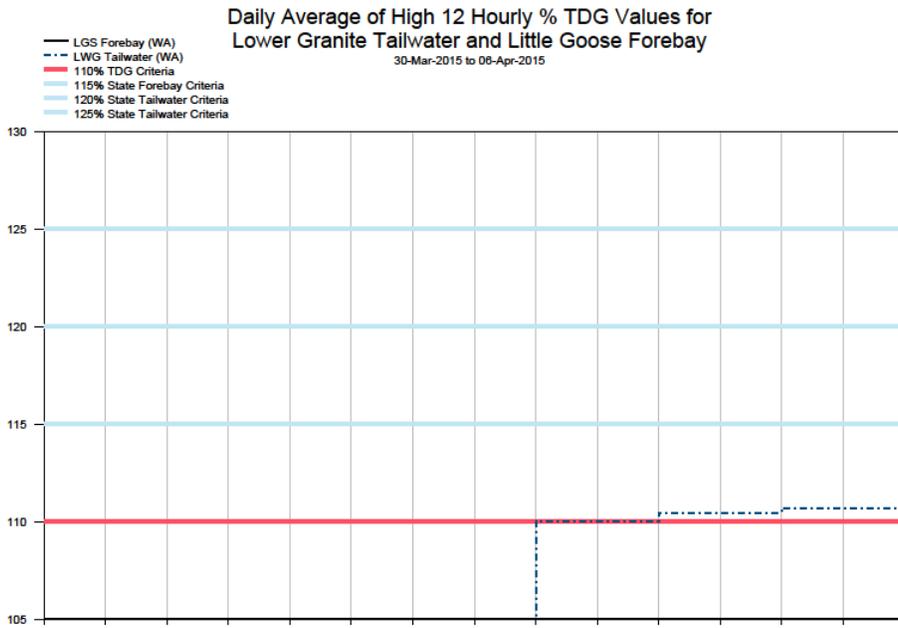
Table 1: April 2015 (4/1 – 4/26) – FOP Implementation Report Table

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Little Goose	Reduced Spill	4/9/15	1700	1	Maintenance	Hourly spill decreased to 28.6% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock for a dam safety inspection. 24-hr avg spill was 29.8%.
Little Goose	Reduced Spill	4/11/15	1600	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range). Reduced spill for safe passage of barge. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/13/15	1700	1	Navigation	Hourly spill decreased to 28.0% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 30.0%.
Little Goose	Reduced Spill	4/15/15	1900	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range). Reduced spill for safe passage of fish barge. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/17/15	0300	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/21/15	1700	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/26/15	1600	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Ice Harbor	Additional Spill	4/13/15	2000 – 2300	4	Operational Limitations	Hourly spill ranged from 35.7% to 42.0% (above 30.0% \pm 1%). Hourly total project outflow ranged from 18.1 to 22.1 kcfs. Due to RSW, minimum spill is fixed at approx 7.5-8.4 kcfs, which results in spill >FOP target when total outflow is approx 17-26 kcfs. 24-hr avg spill was 31.6%.

⁶ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Ice Harbor	Additional Spill	4/23/15	1800	1	Human/Program Error	Hourly spill increased to 50.5 kcfs (above 45 kcfs \pm 2 kcfs range) due to a miscalculation above minimum generation range (8.2-10.0 kcfs).
McNary	Additional Spill	4/12/15	2300	1	Human/Program Error	Hourly spill increased to 41.3% (above 40.0% \pm 1% range) due to a miscalculation. 24-hr avg spill was 40.3%.
John Day	Additional Spill	4/10/15	1400	1	Transmission Stability	Hourly spill increased to 31.1% (above 30.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 29.9%.
John Day	Additional Spill	4/23/15	2300	1	Transmission Stability	Hourly spill increased to 31.3% (above 30.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 30.0%.
The Dalles	Additional Spill	4/13/15	2100	1	Transmission Stability	Hourly spill increased to 41.3% (above 40.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 39.9%.

Figure 1



Lower Granite Dam - Hourly Spill and Flow

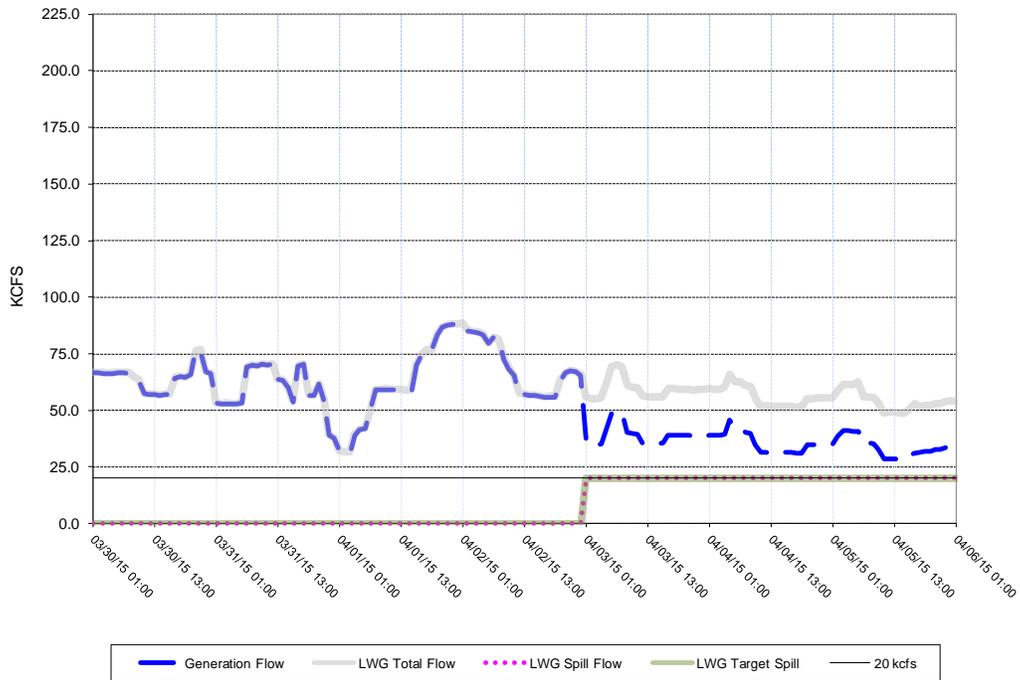
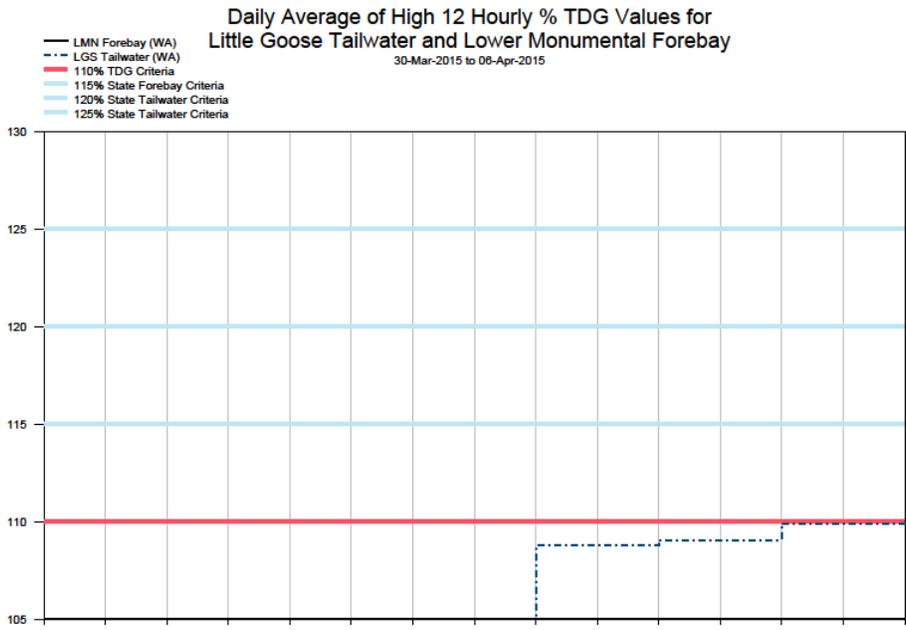


Figure 2



Little Goose Dam - Hourly Spill and Flow

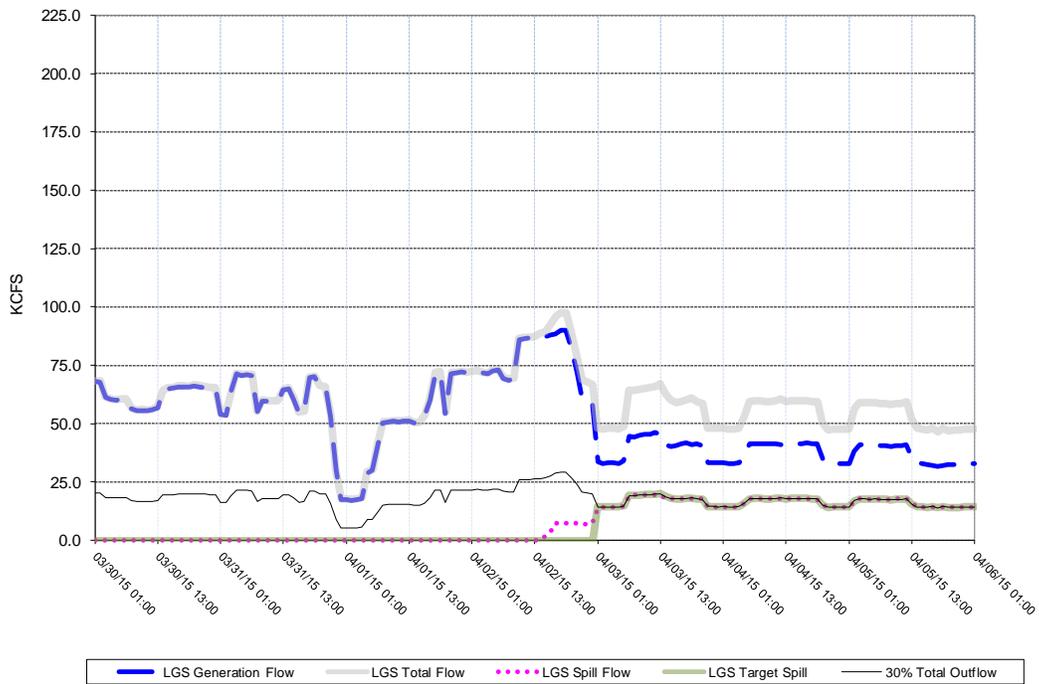


Figure 3

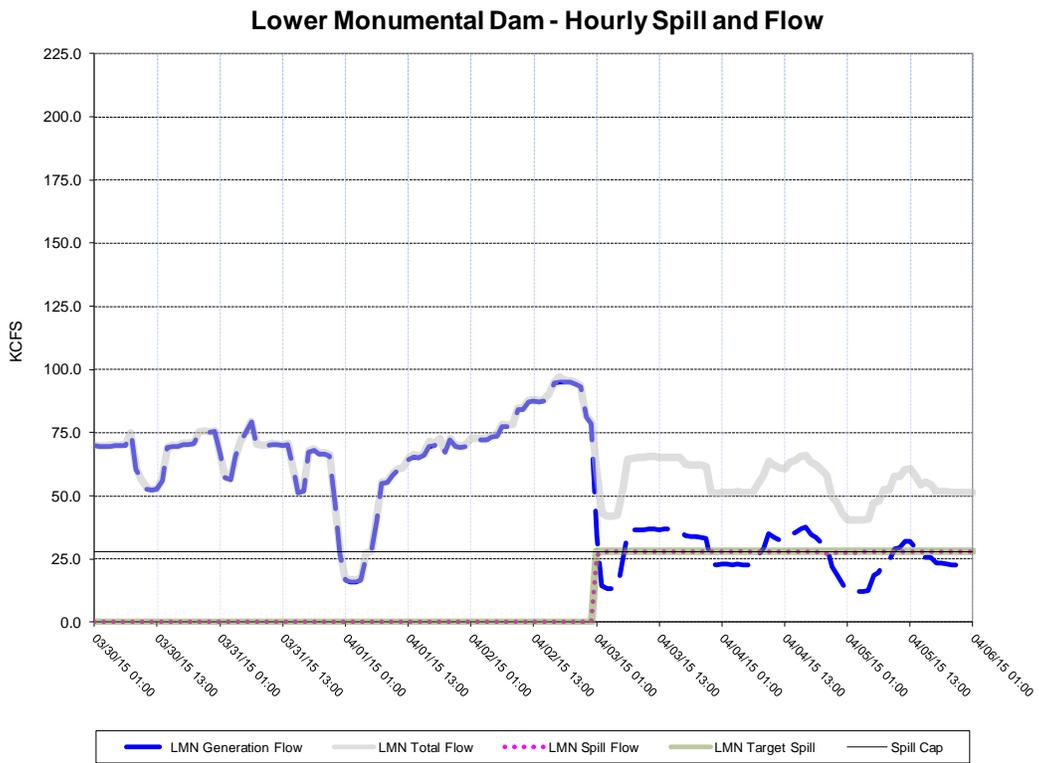
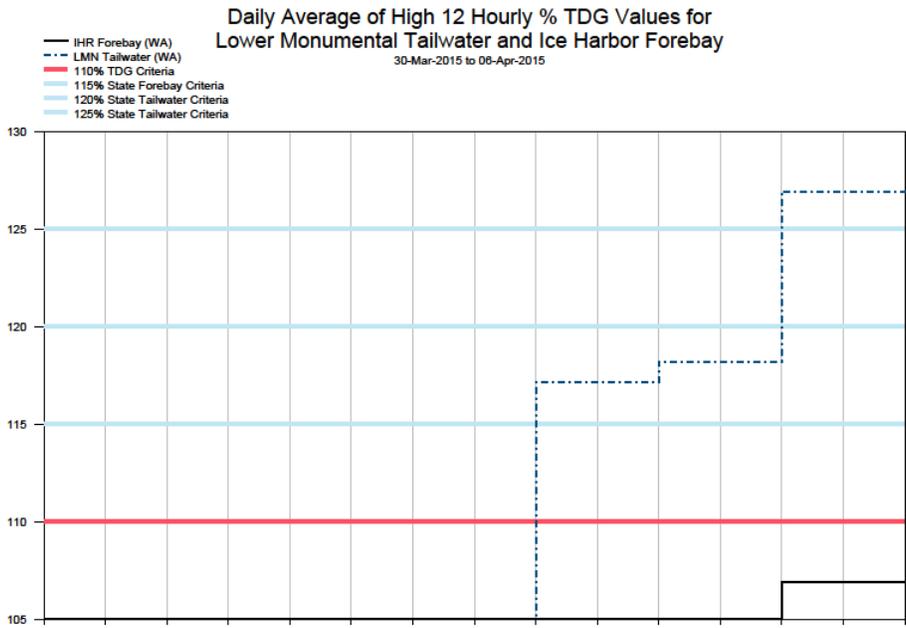


Figure 4

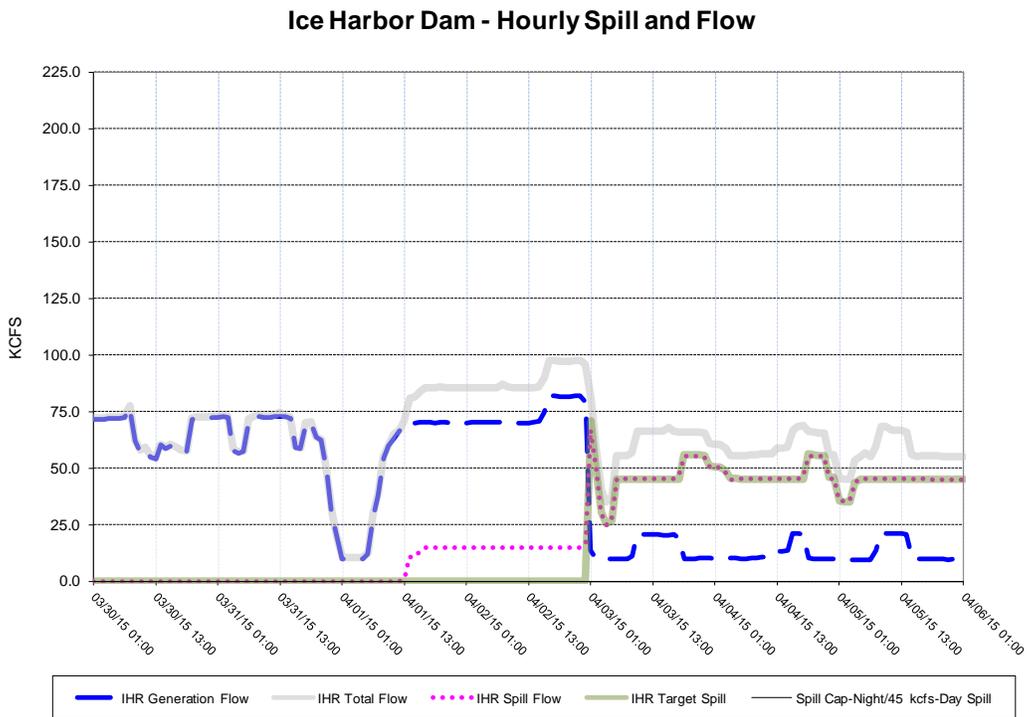
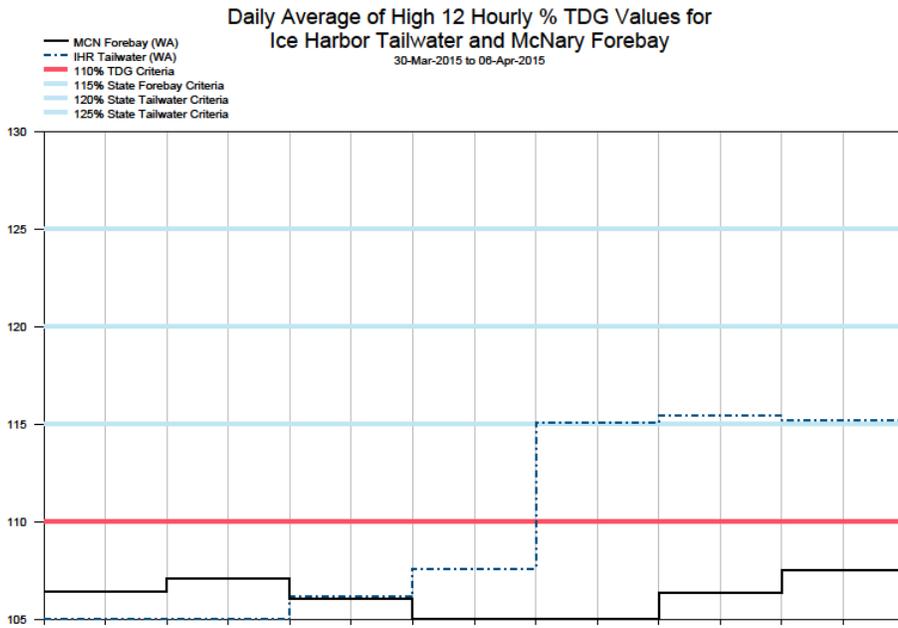


Figure 5

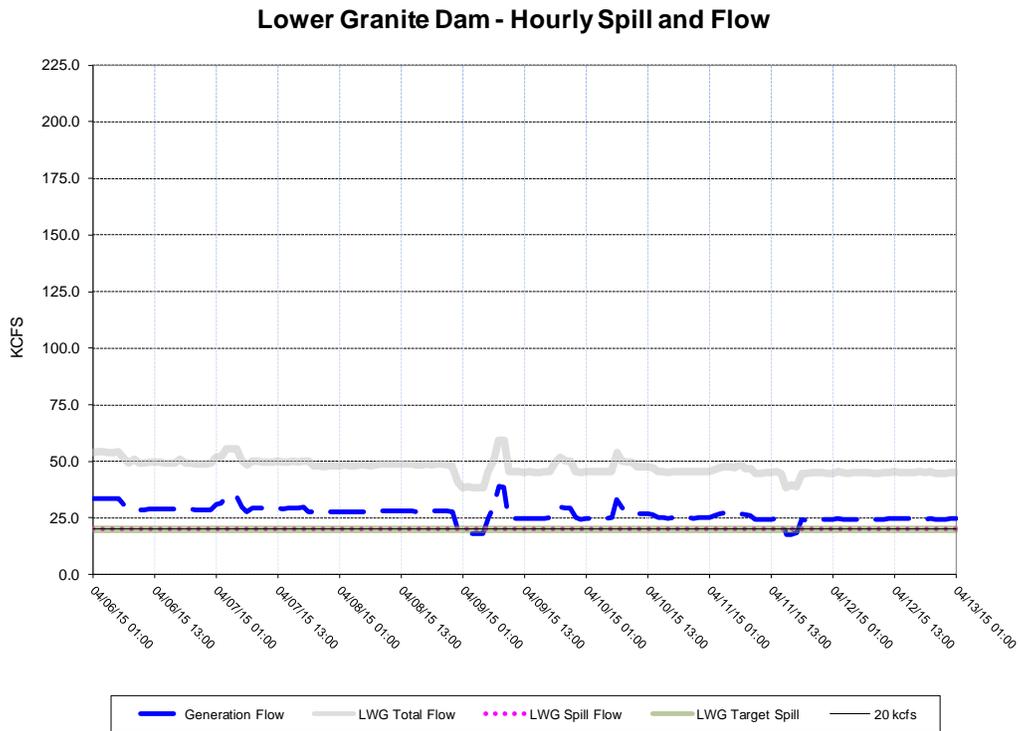
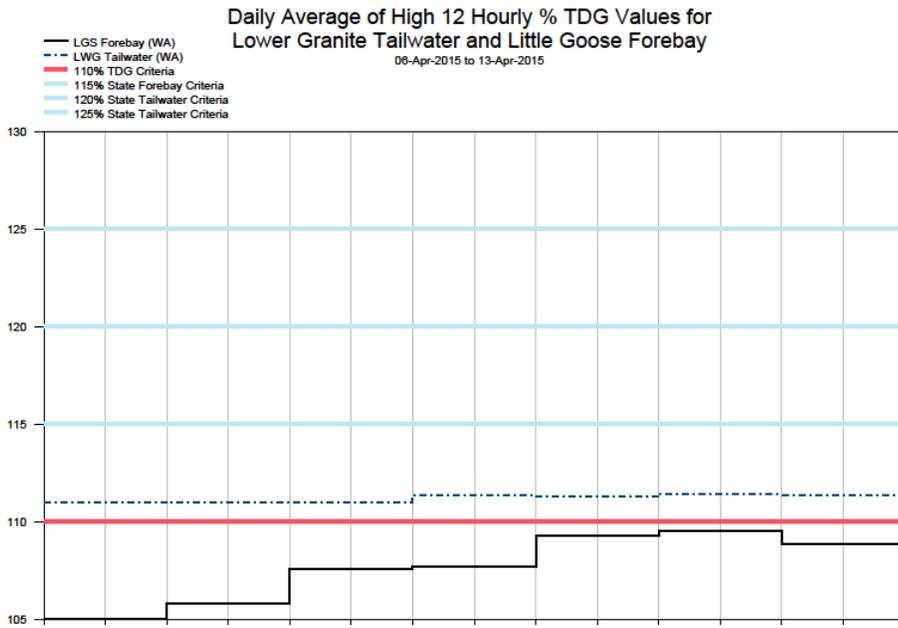
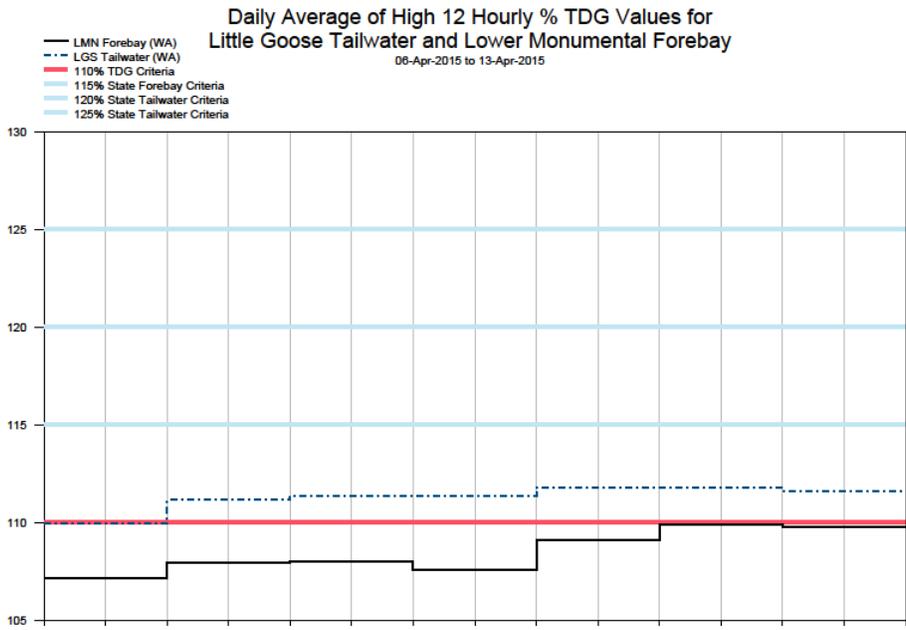


Figure 6



Little Goose Dam - Hourly Spill and Flow

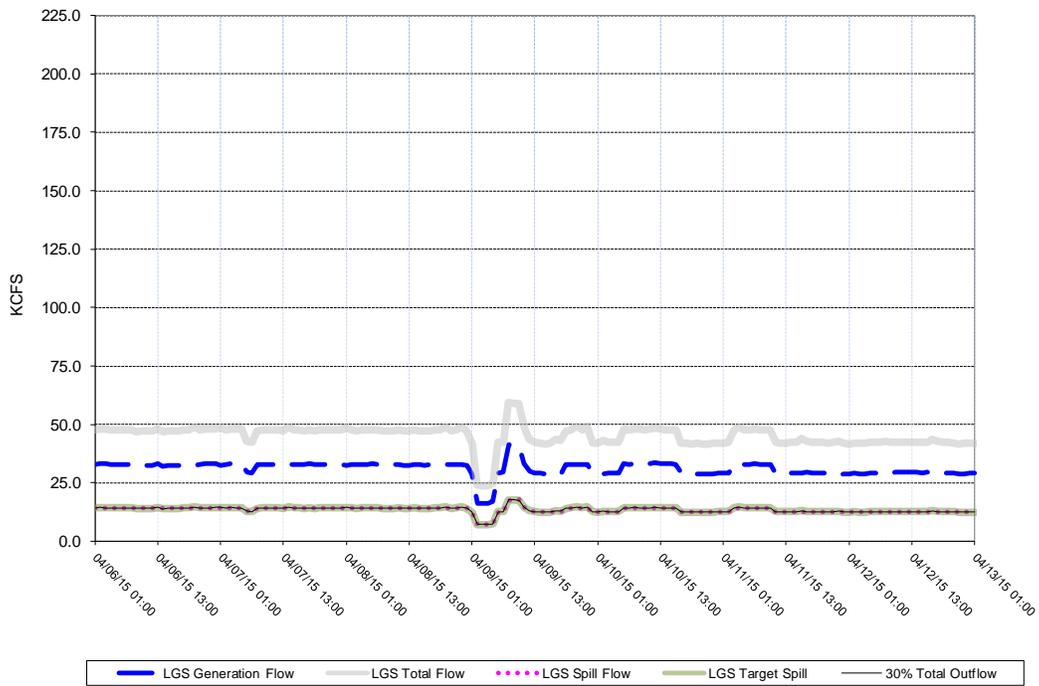


Figure 7

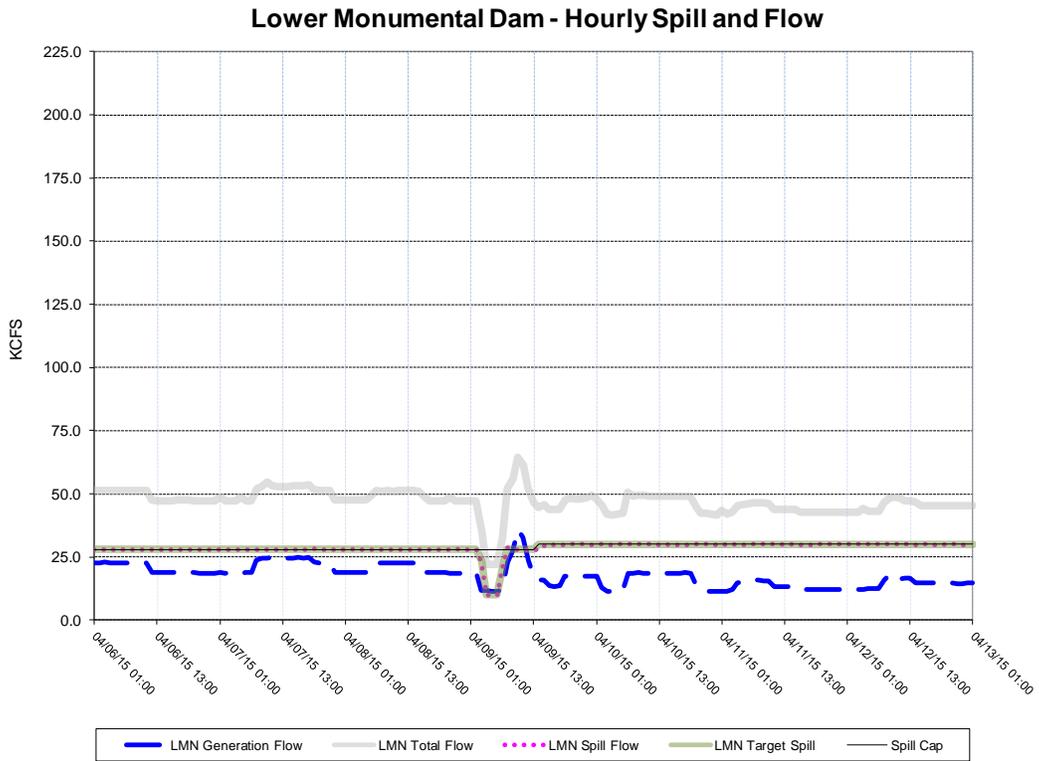
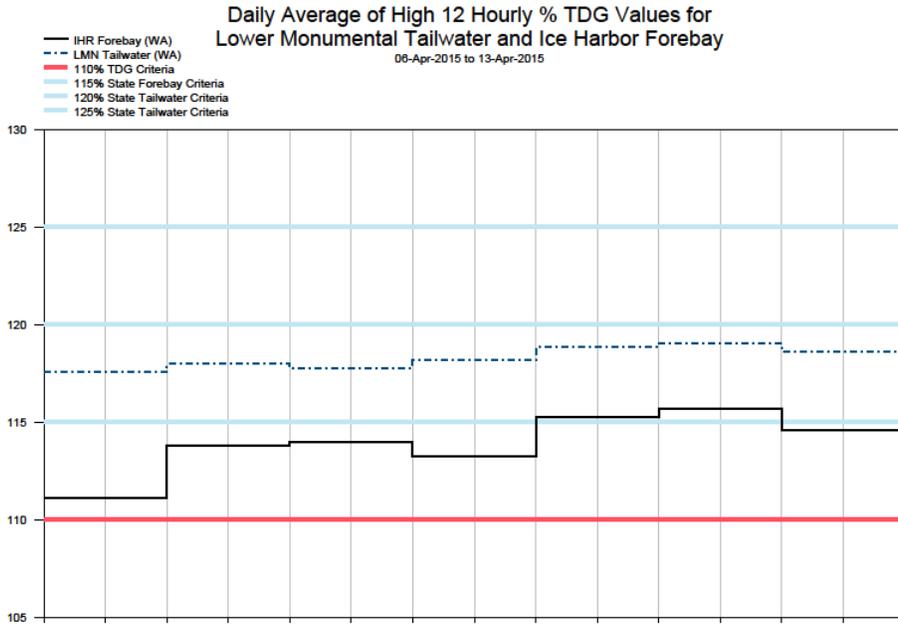


Figure 8

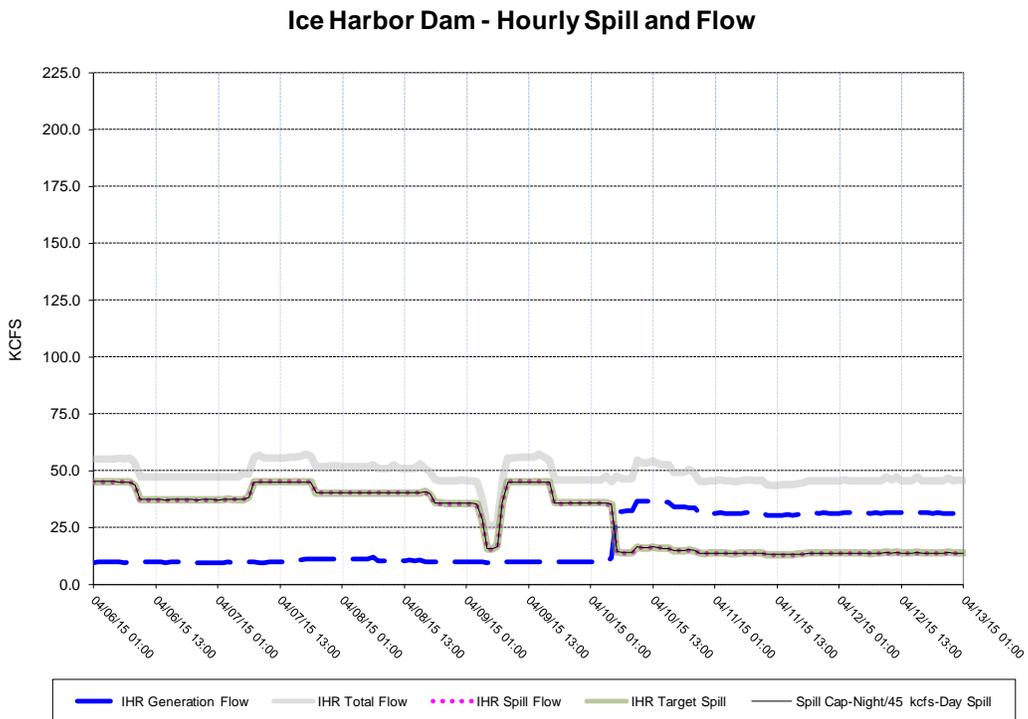
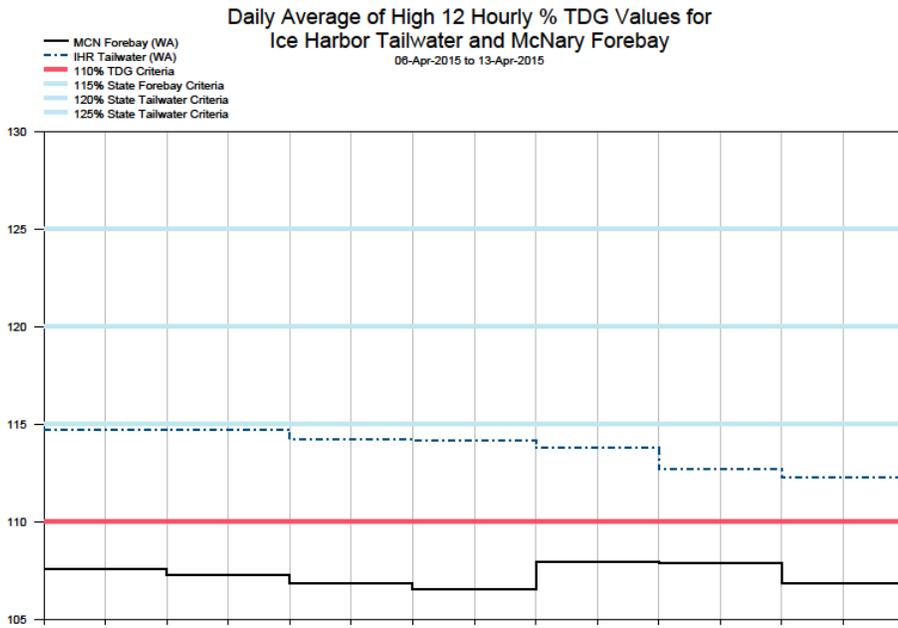
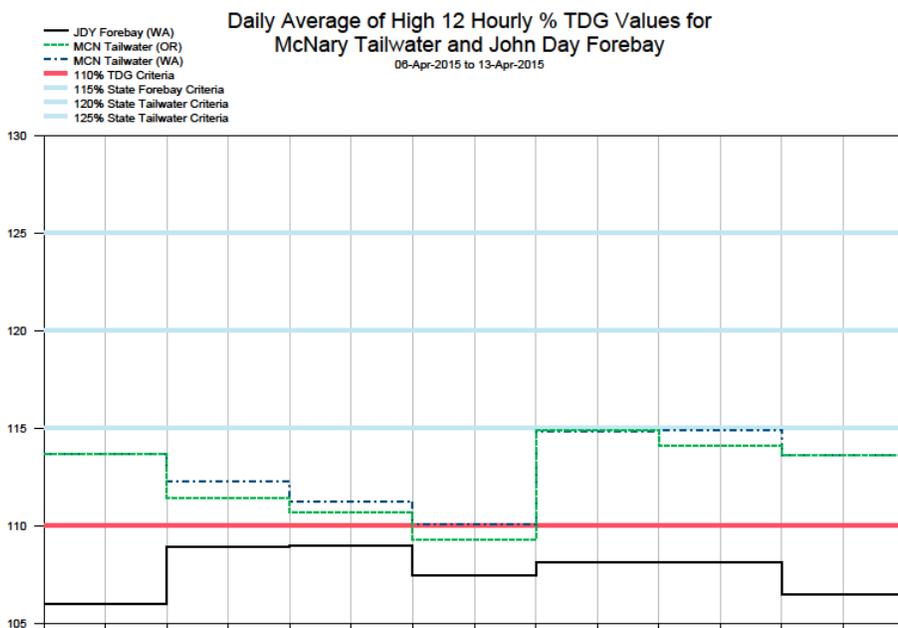


Figure 9



McNary Dam - Hourly Spill and Flow

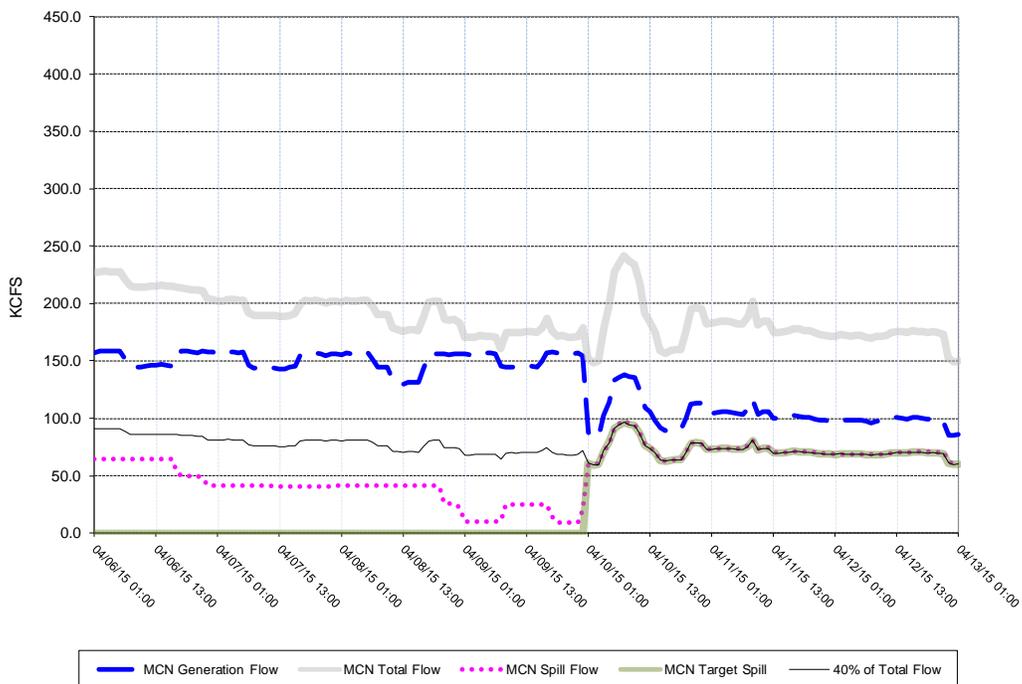
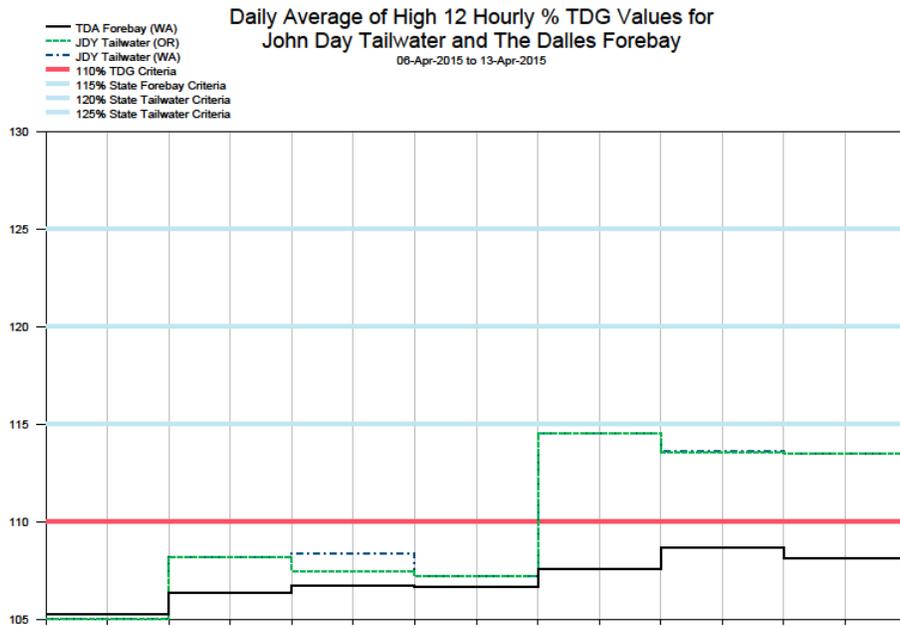


Figure 10



John Day Dam - Hourly Spill and Flow

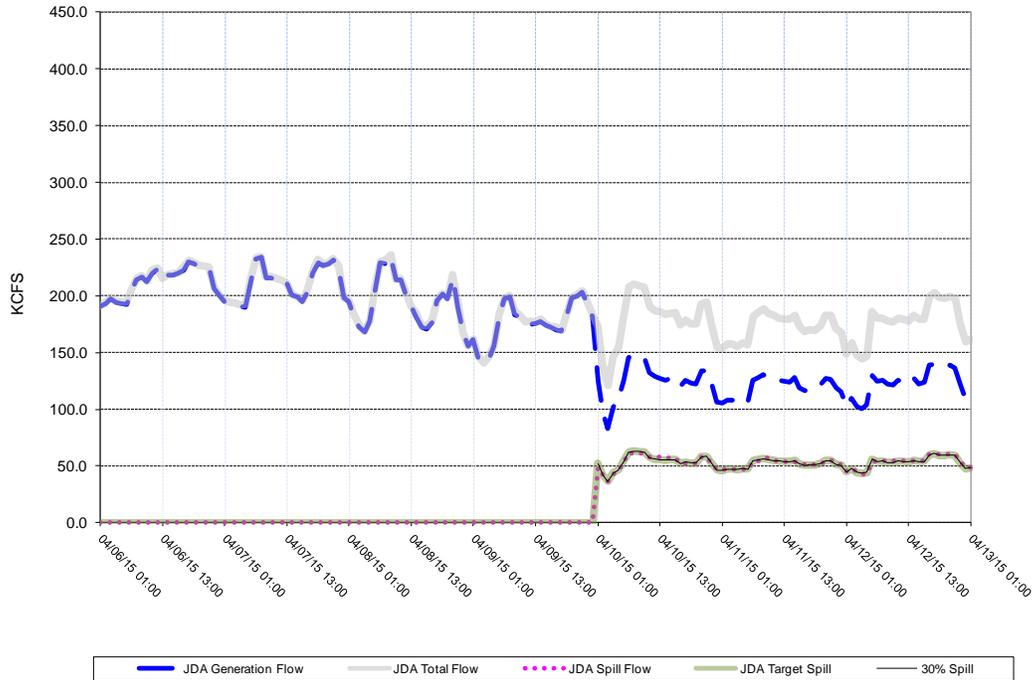
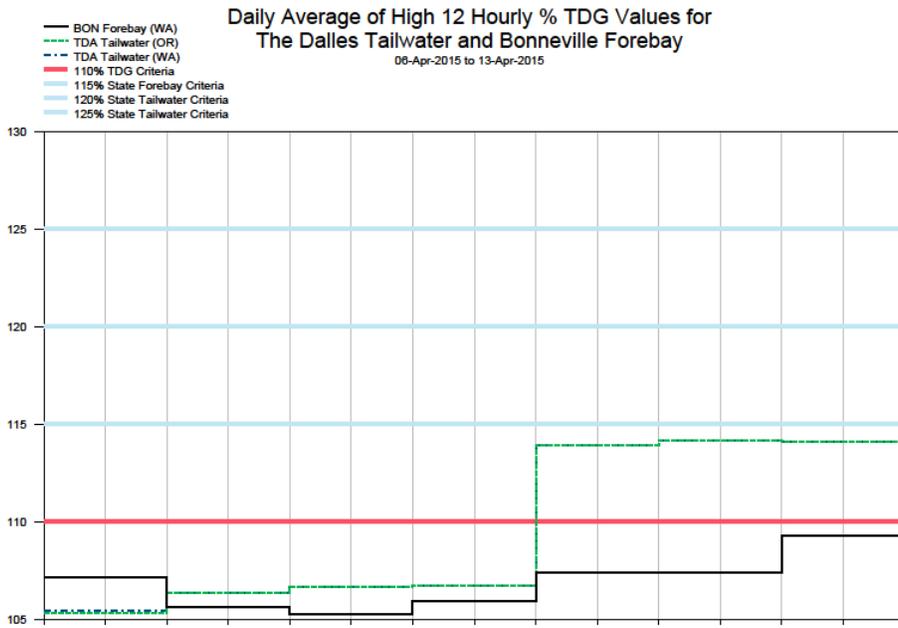


Figure 11



The Dalles Dam - Hourly Spill and Flow

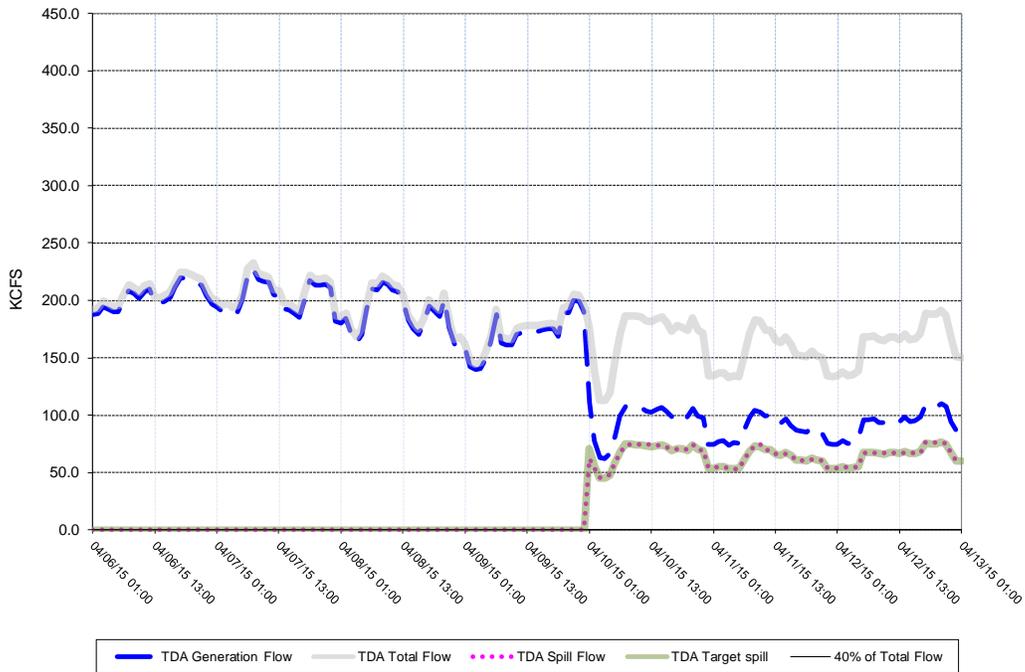


Figure 12

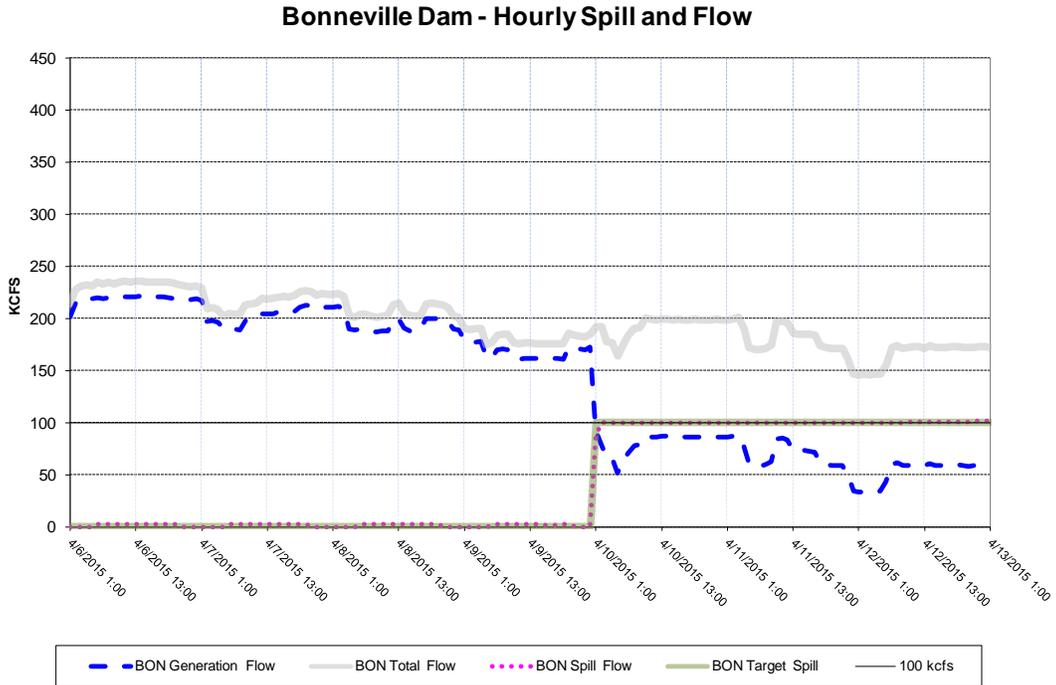
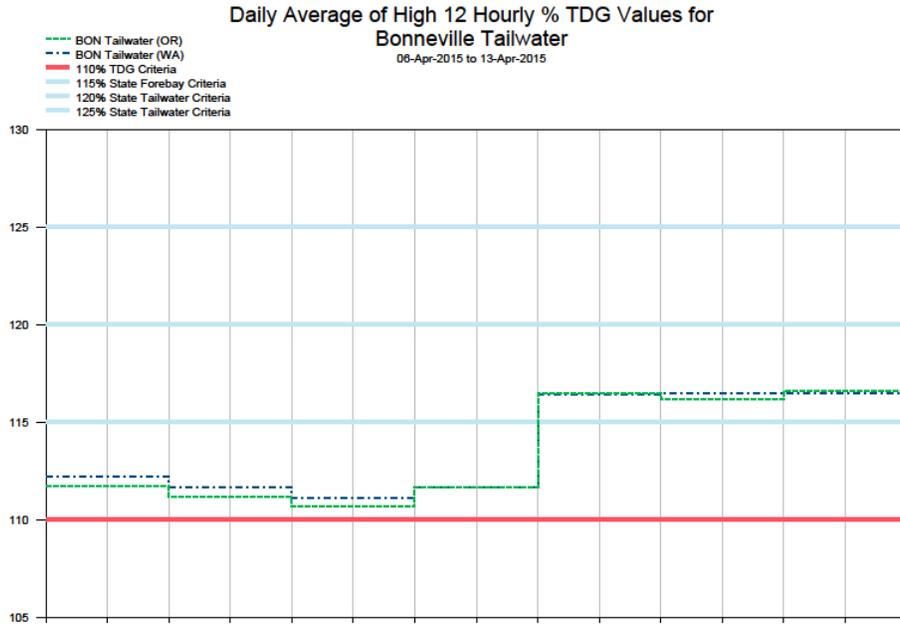
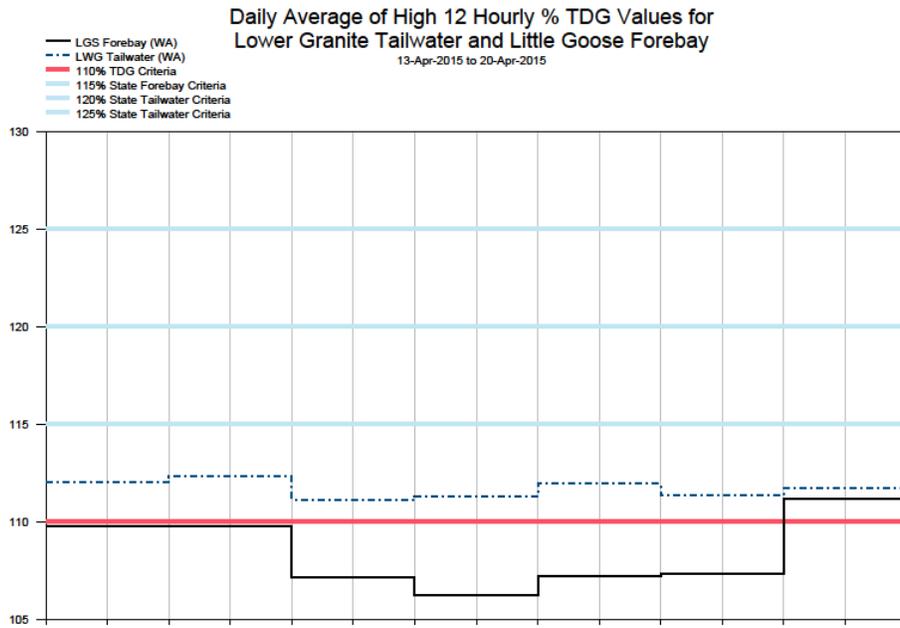


Figure 13



Lower Granite Dam - Hourly Spill and Flow

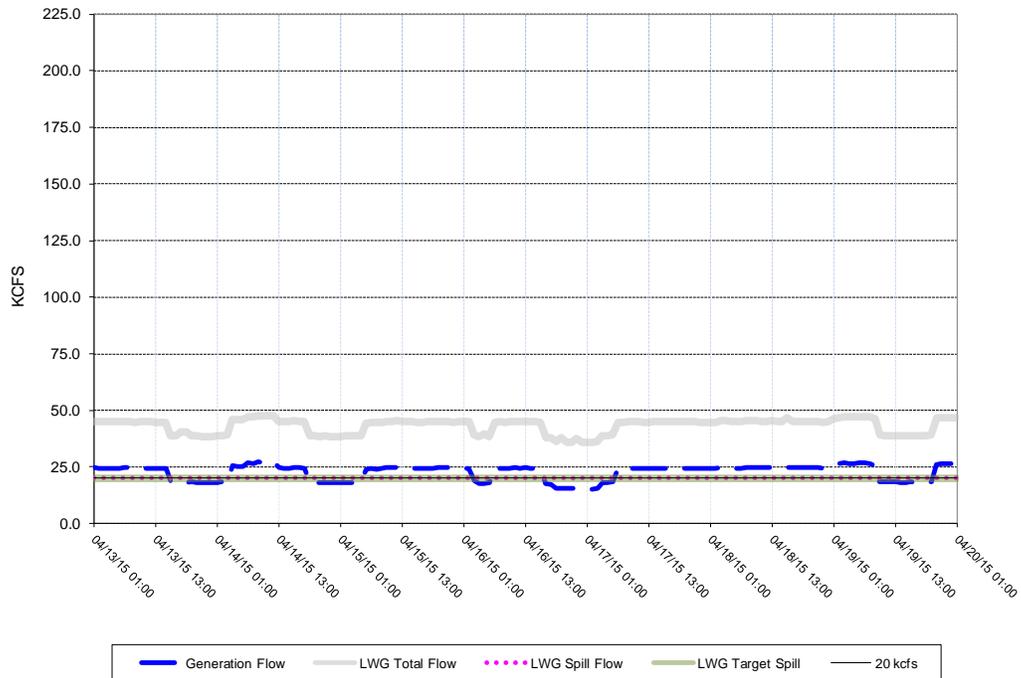
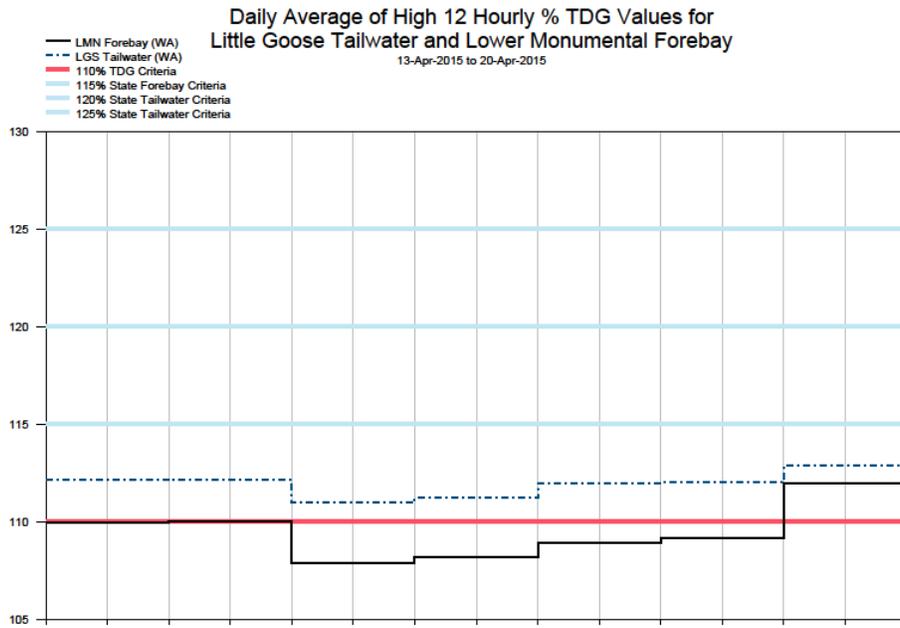


Figure 14



Little Goose Dam - Hourly Spill and Flow

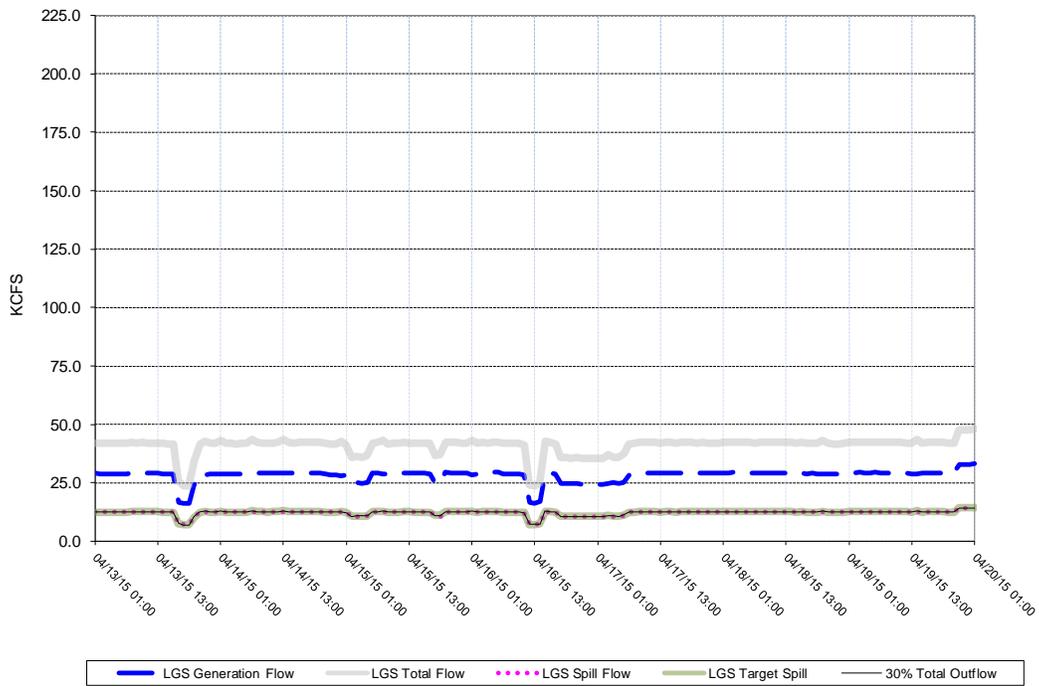


Figure 15

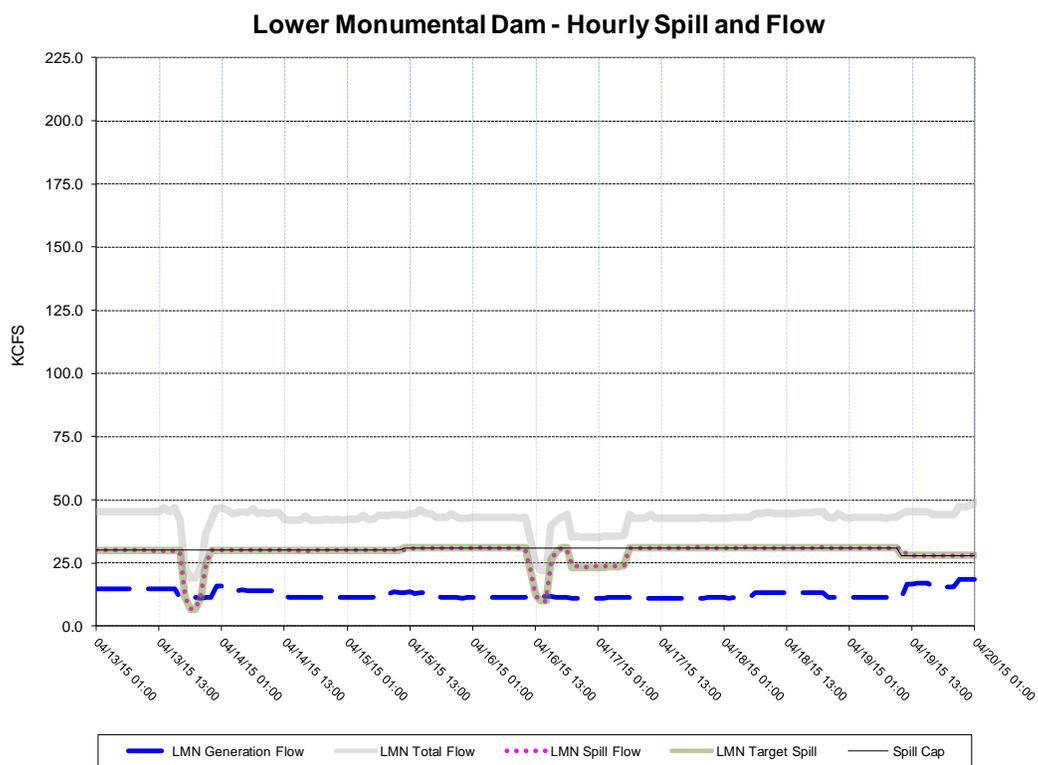
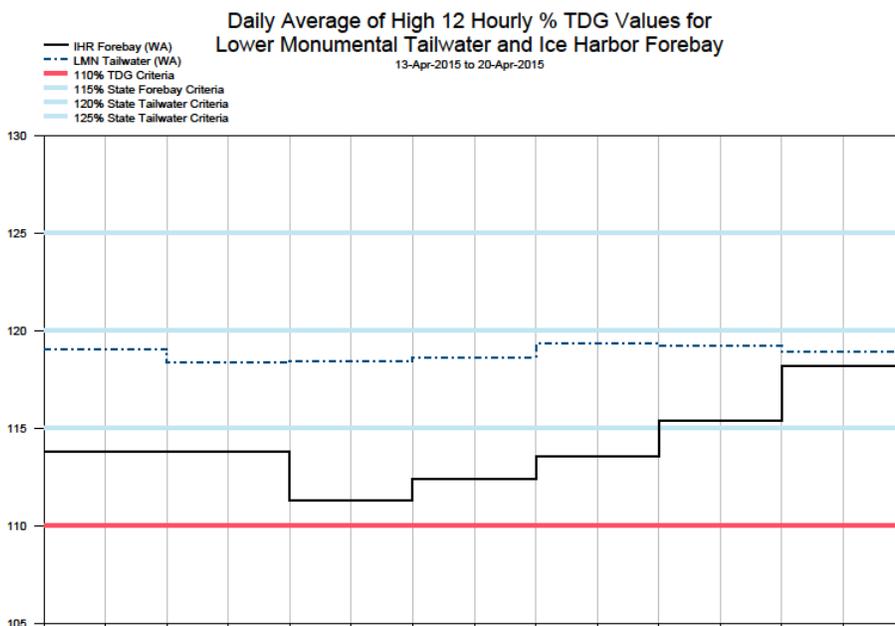
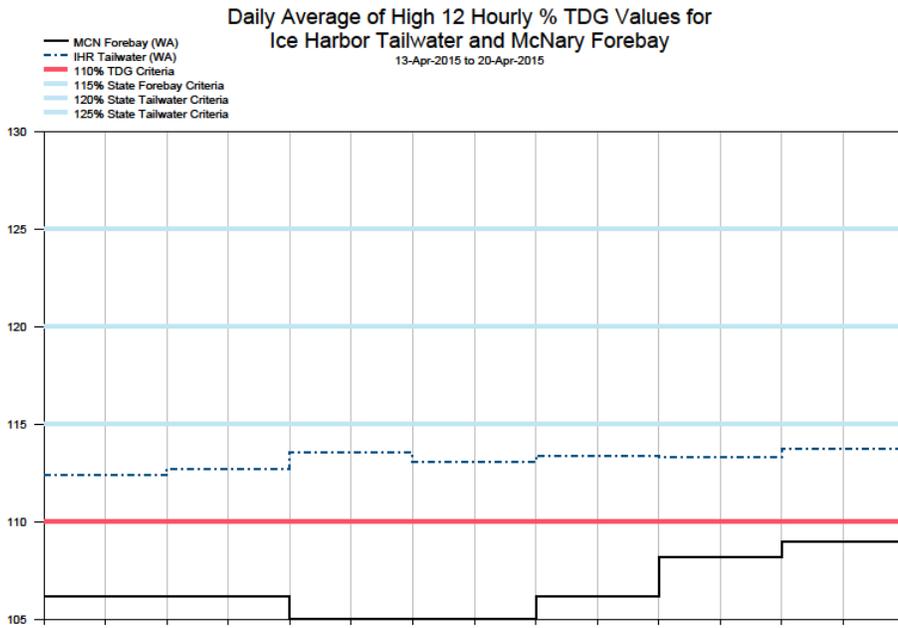


Figure 16



Ice Harbor Dam - Hourly Spill and Flow

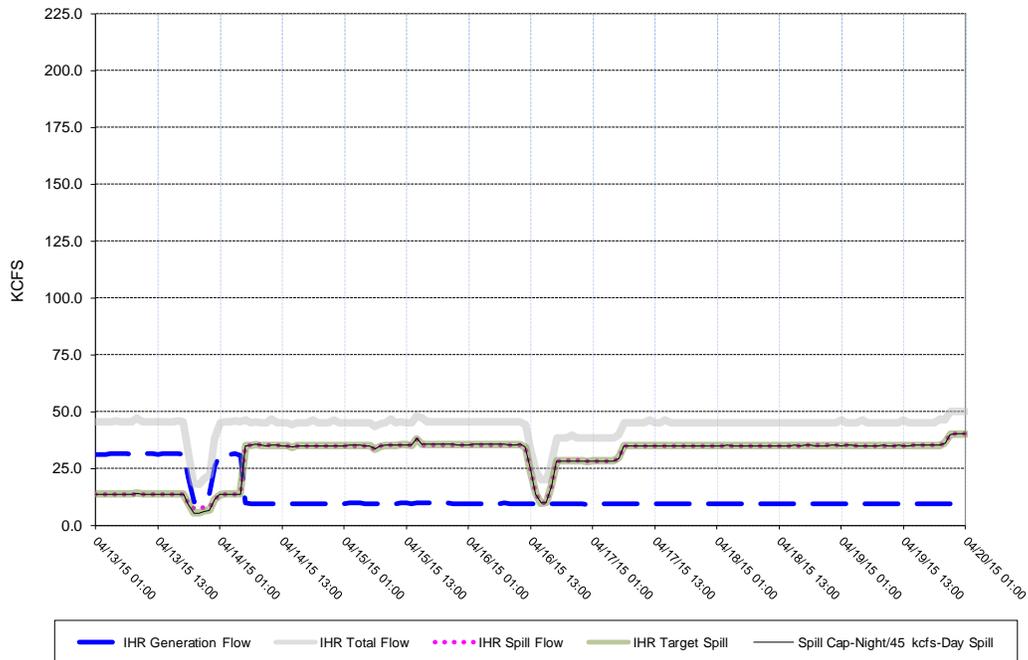
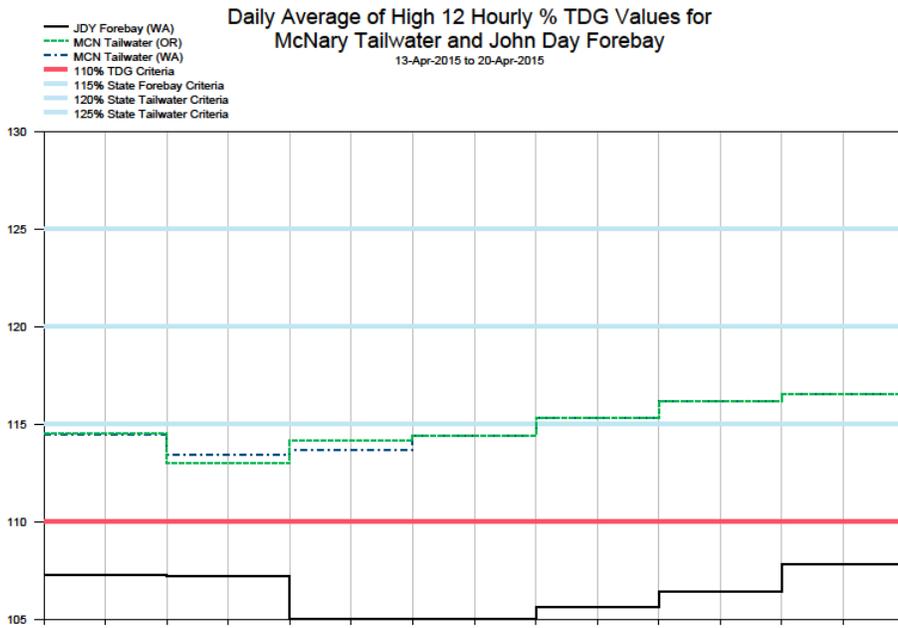


Figure 17



McNary Dam - Hourly Spill and Flow

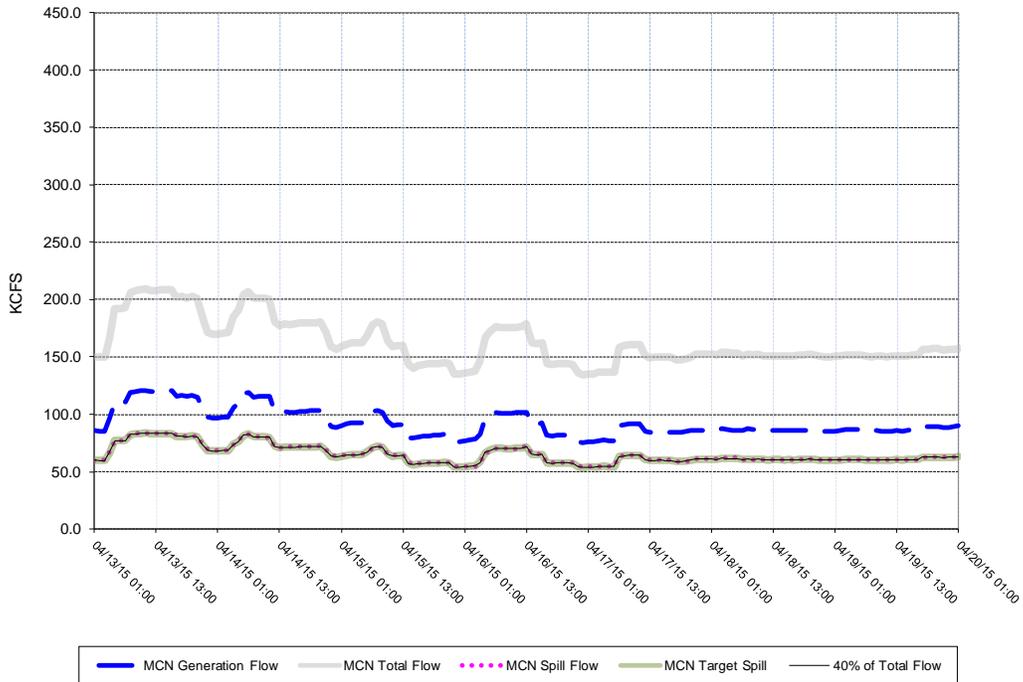
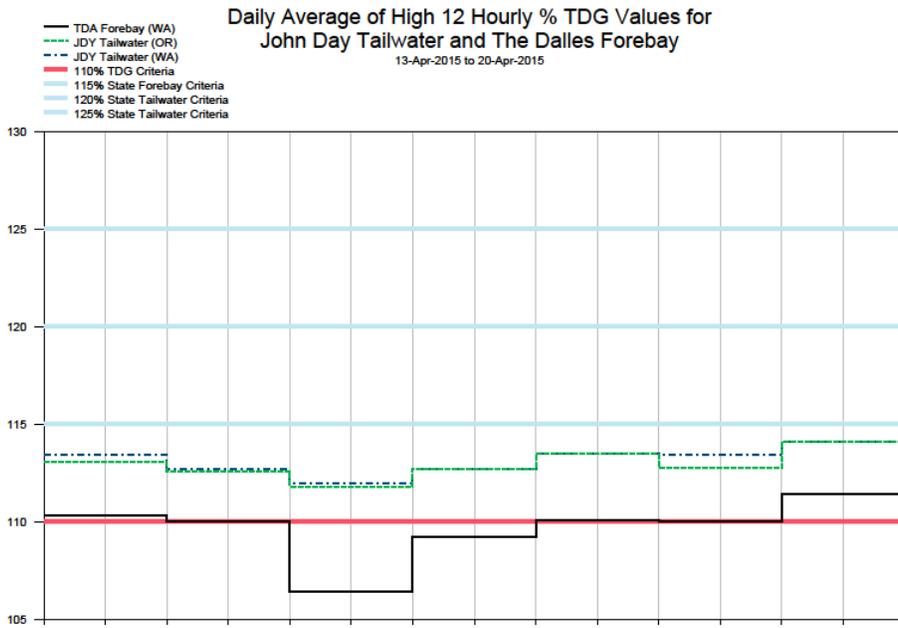


Figure 18



John Day Dam - Hourly Spill and Flow

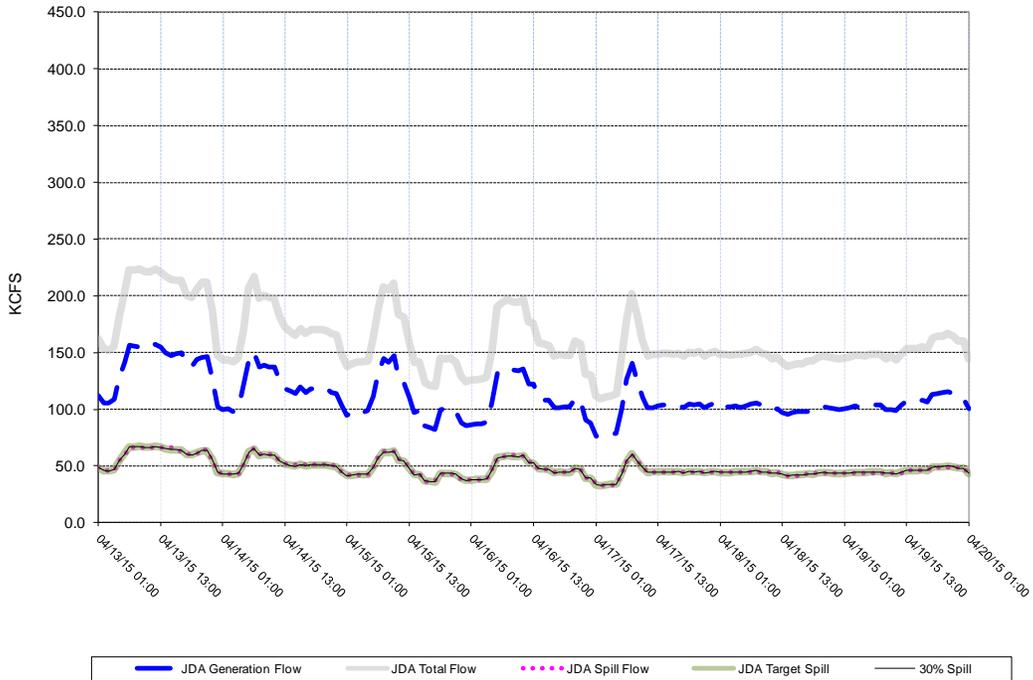
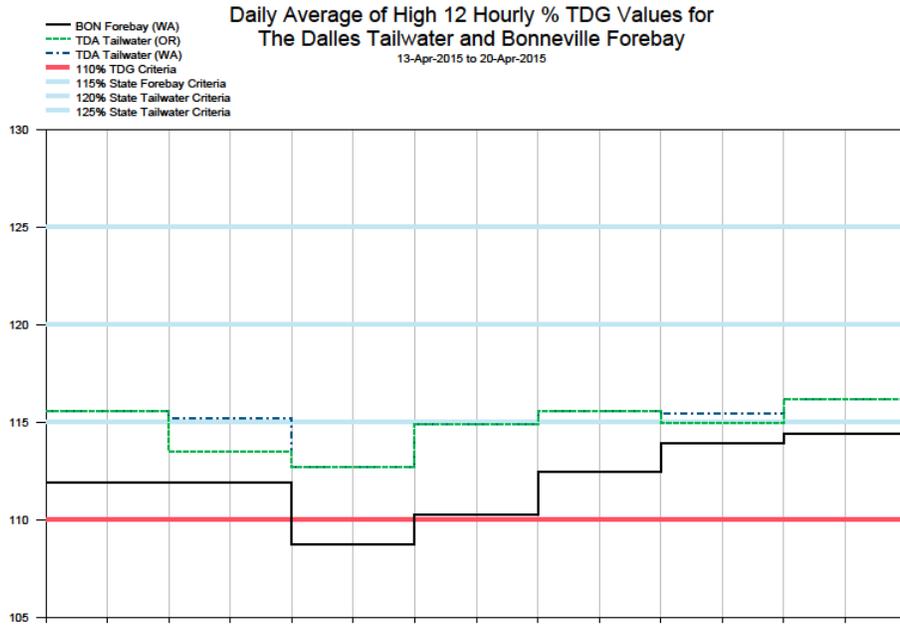


Figure 19



The Dalles Dam - Hourly Spill and Flow

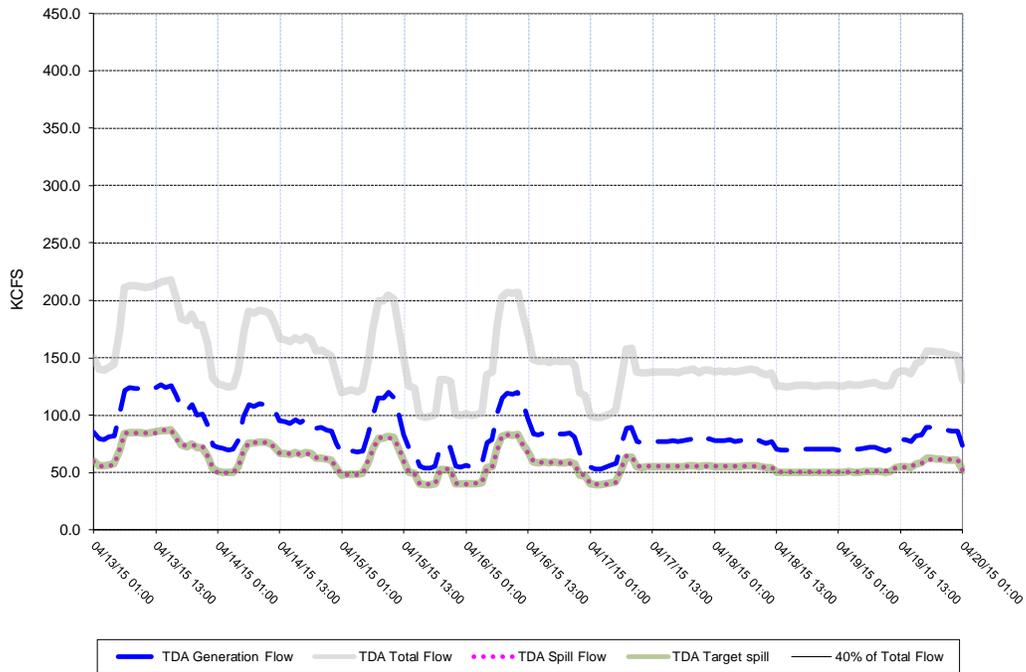


Figure 20

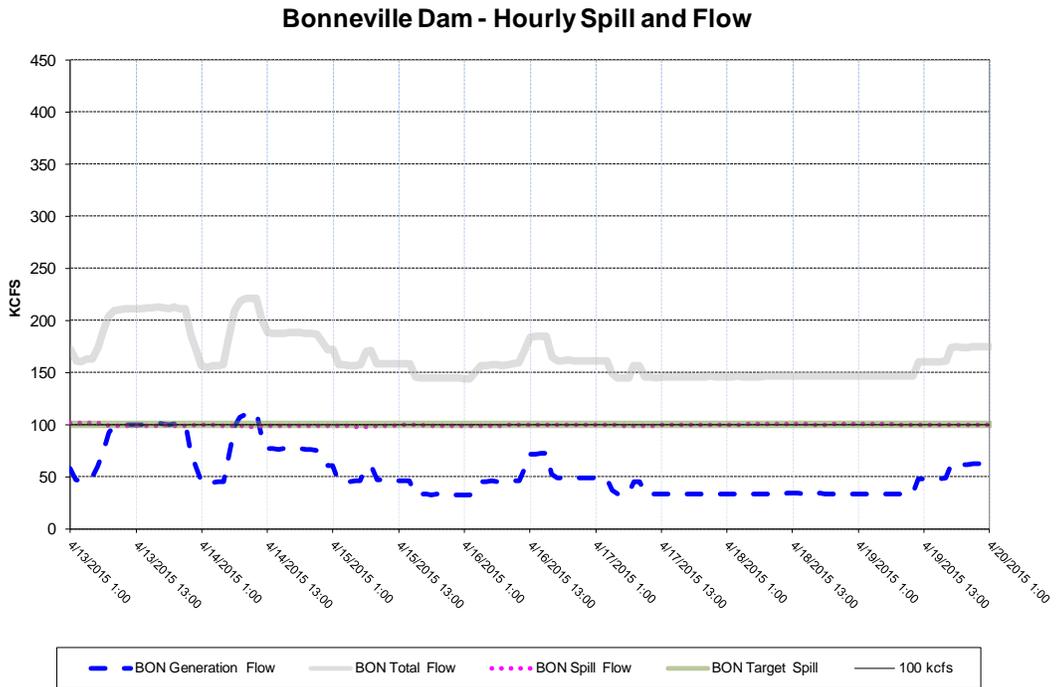
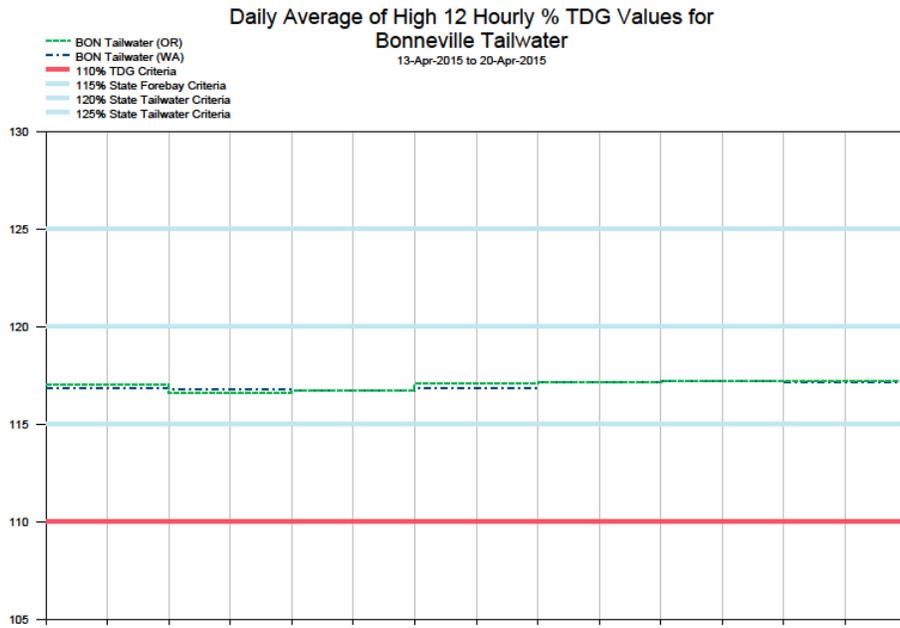
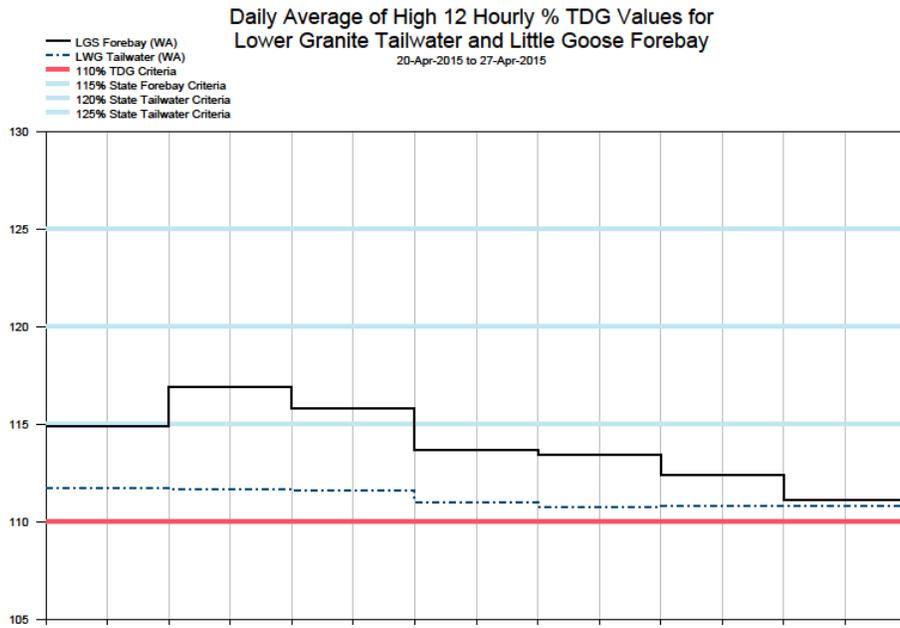


Figure 21



Lower Granite Dam - Hourly Spill and Flow

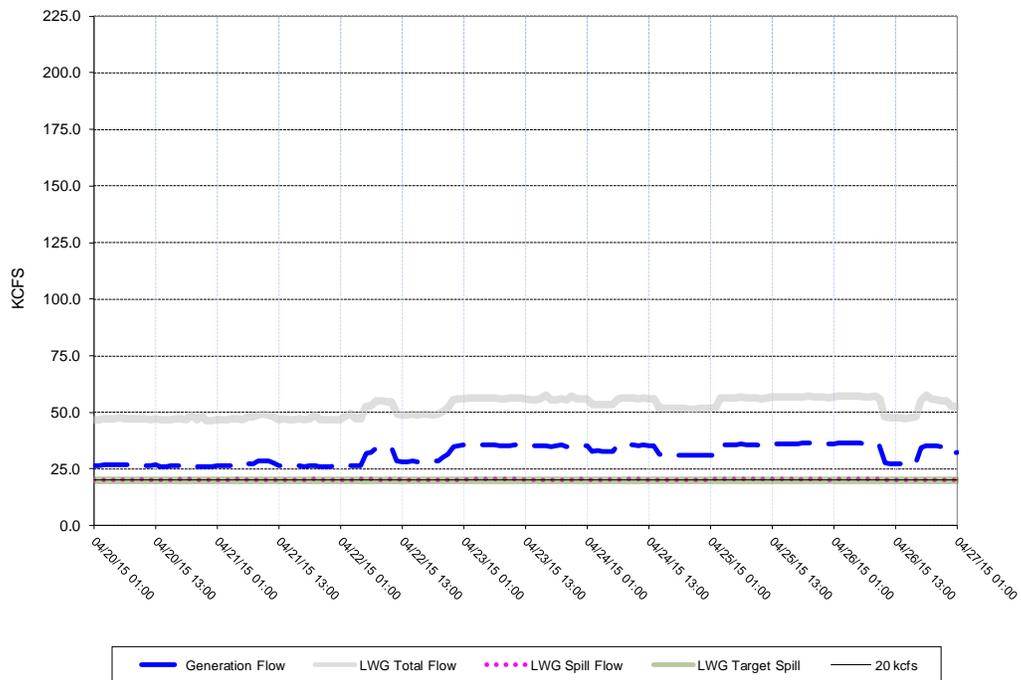
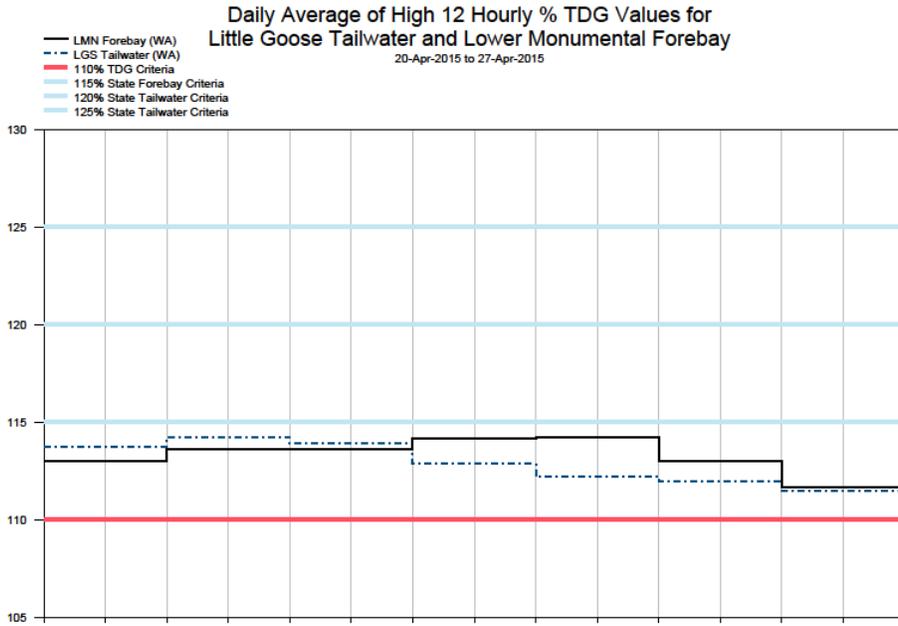


Figure 22



Little Goose Dam - Hourly Spill and Flow

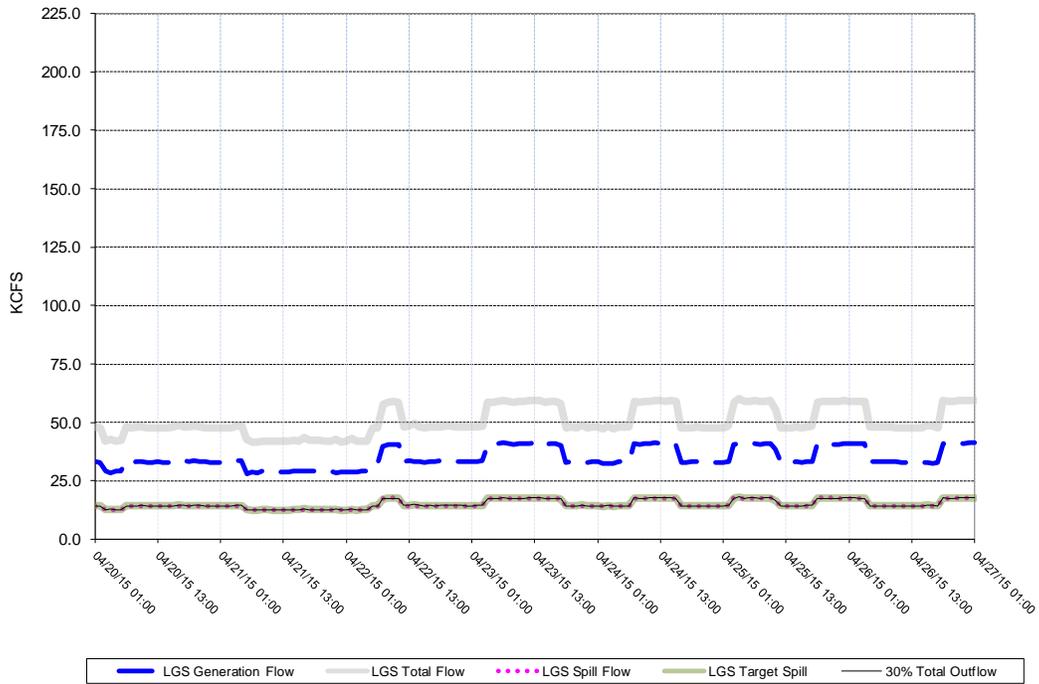


Figure 23

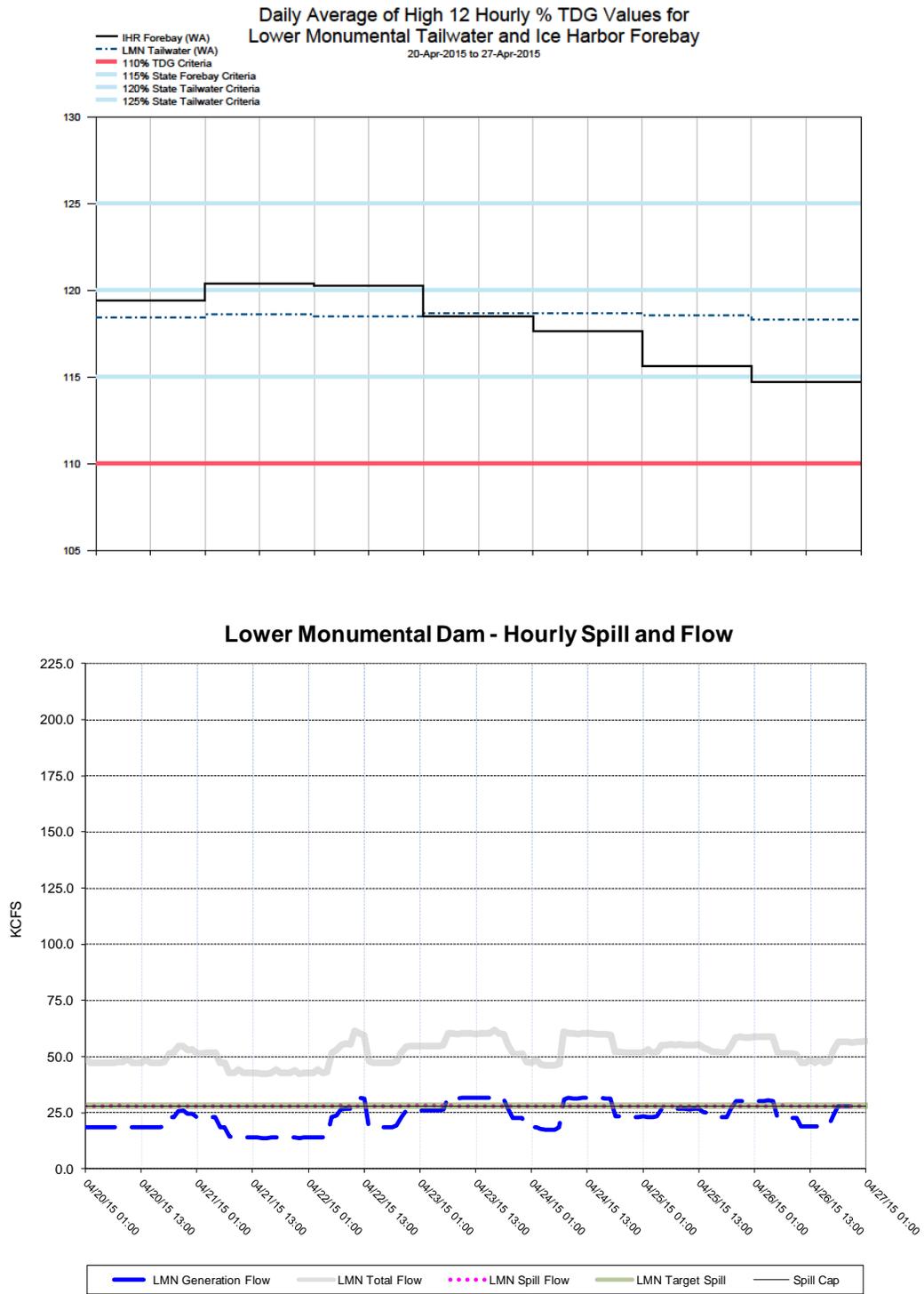


Figure 24

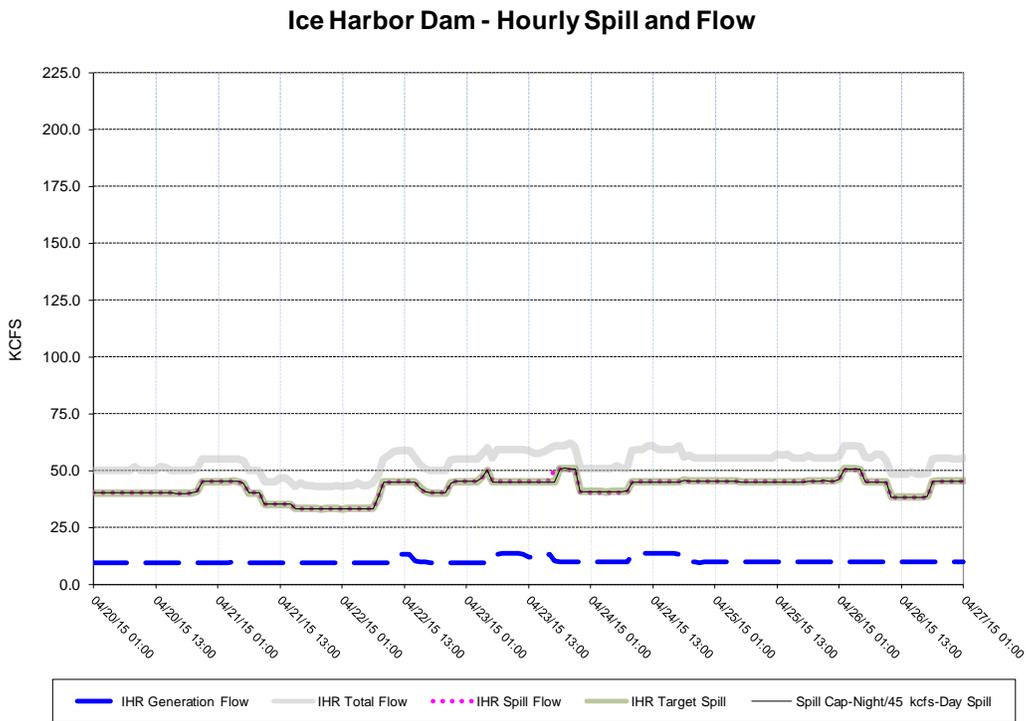
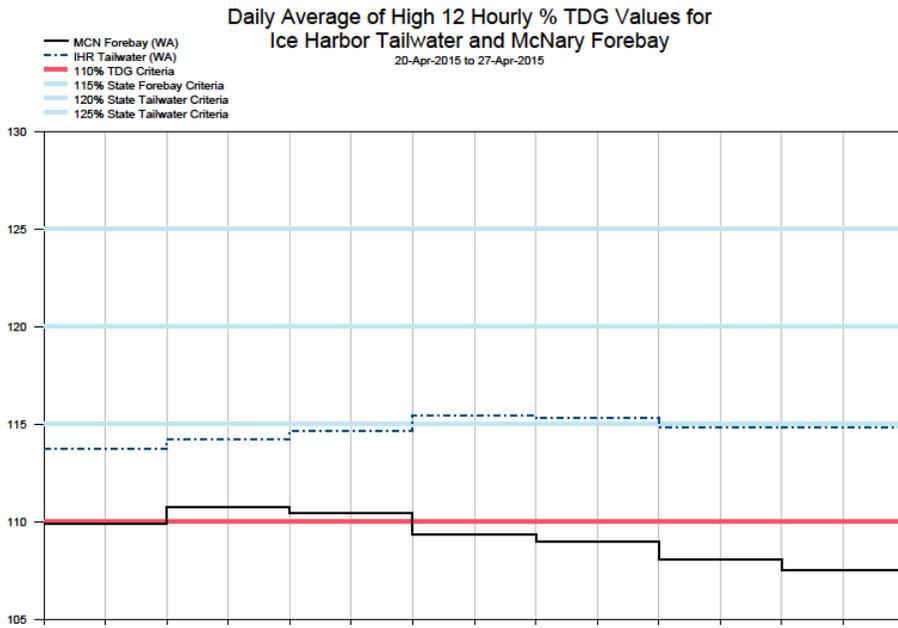
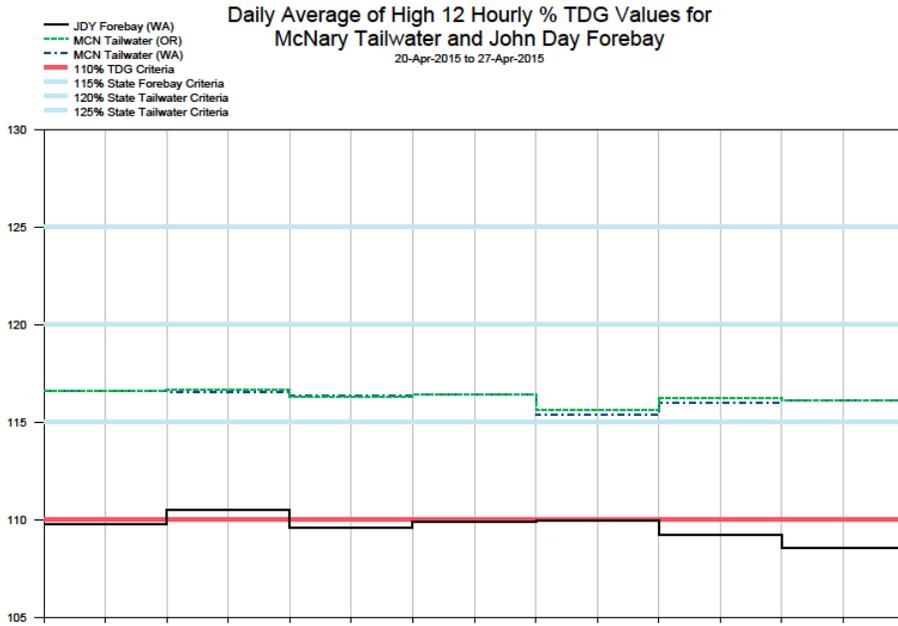


Figure 25



McNary Dam - Hourly Spill and Flow

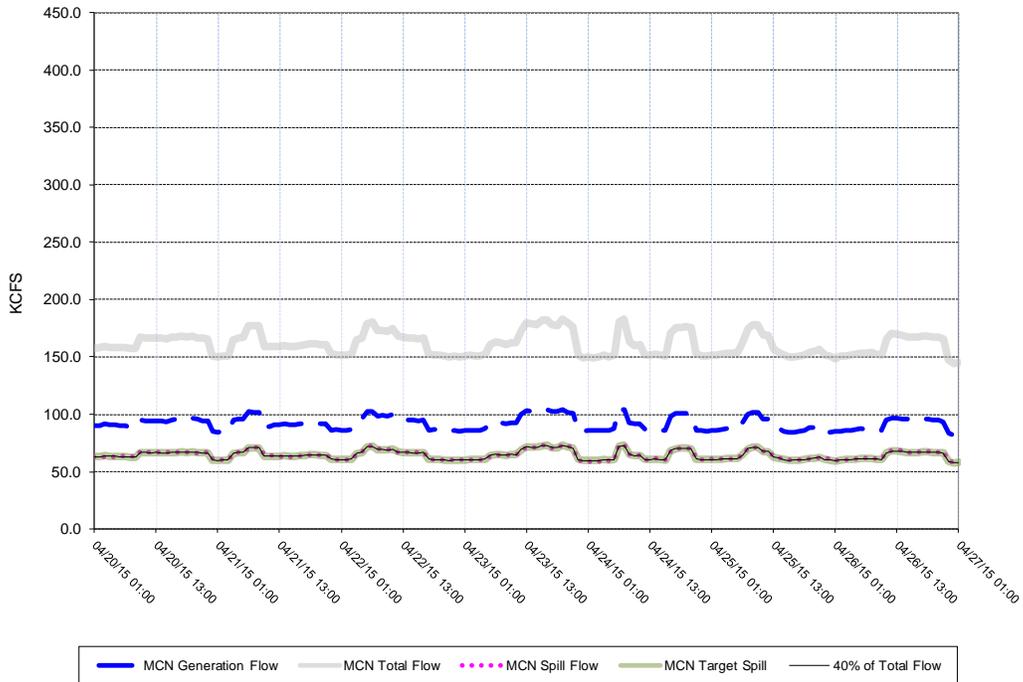
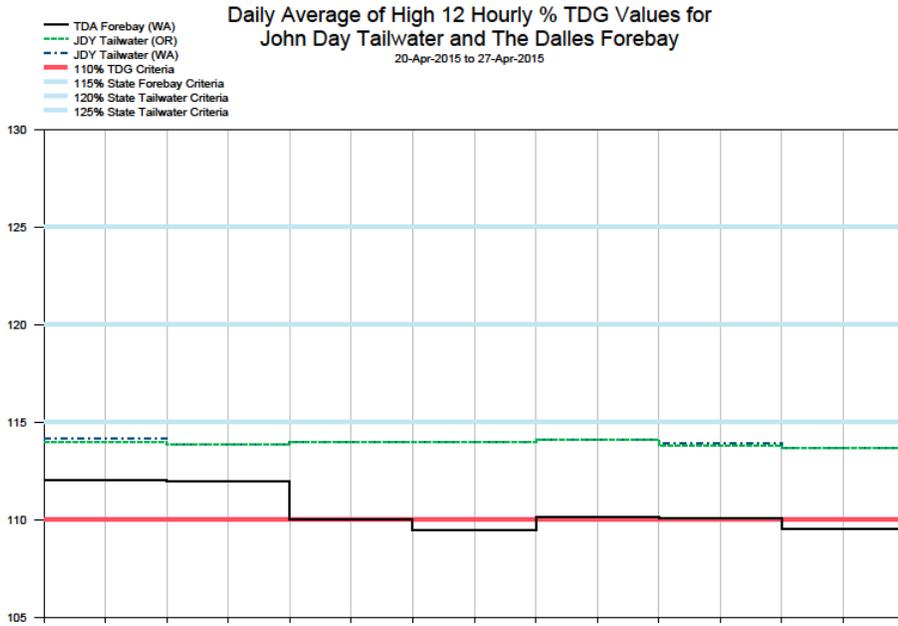


Figure 26



John Day Dam - Hourly Spill and Flow

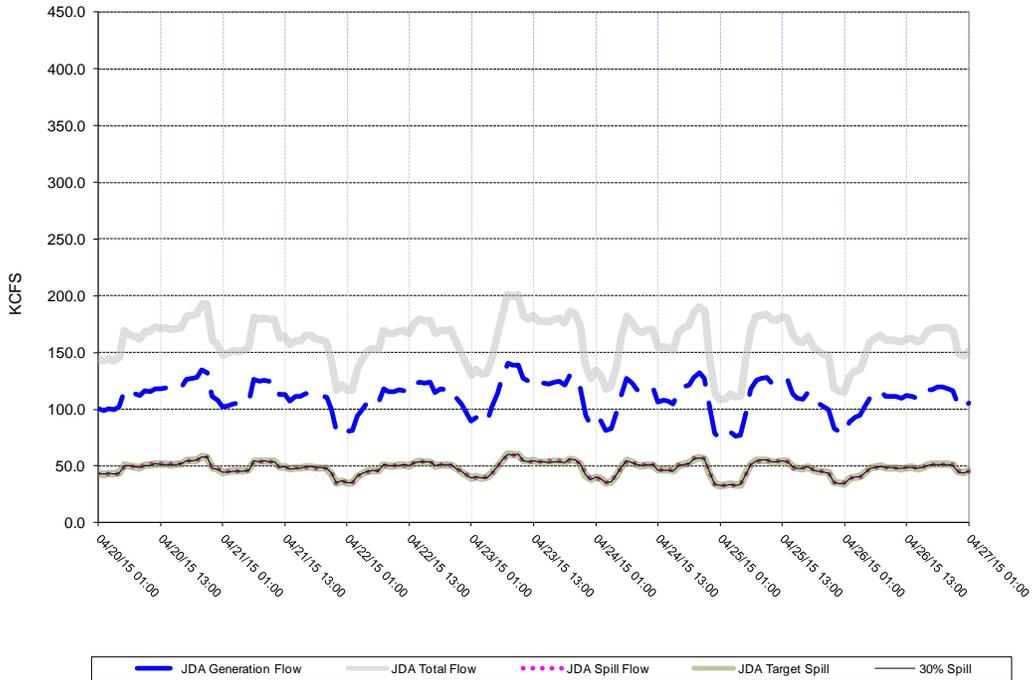
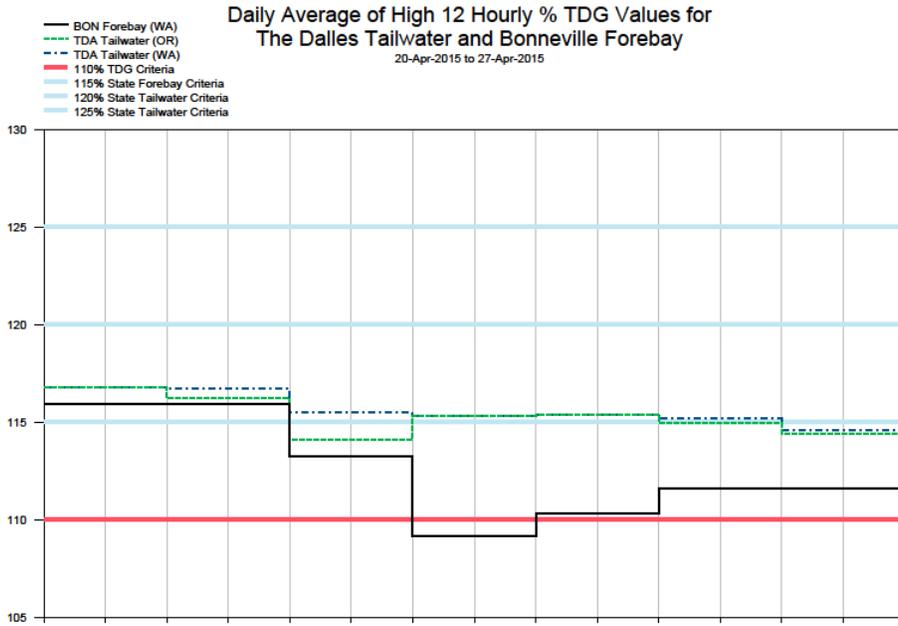


Figure 27



The Dalles Dam - Hourly Spill and Flow

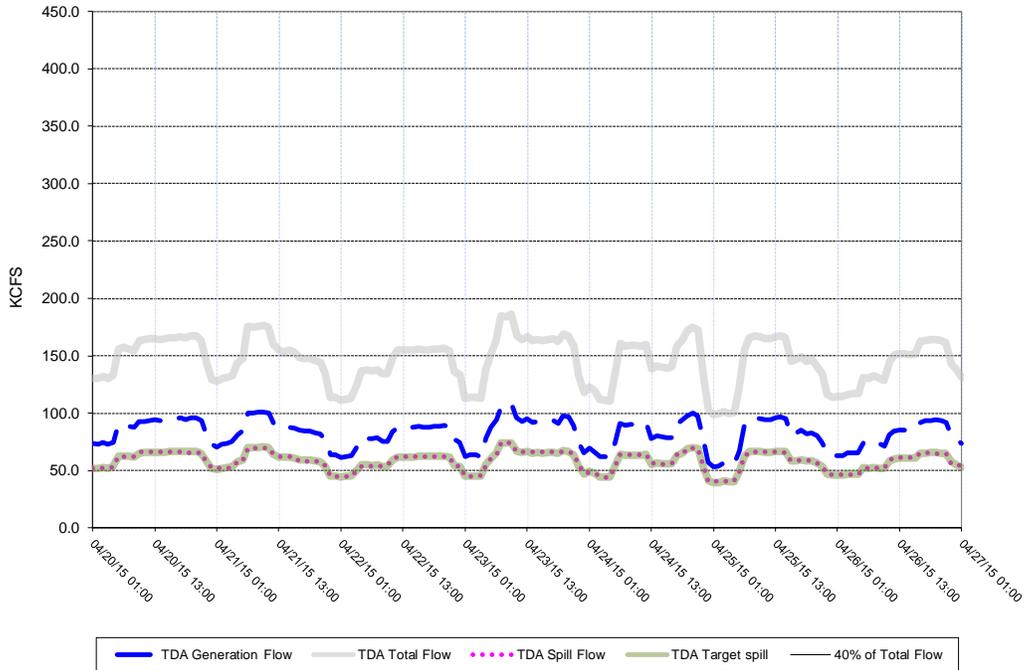


Figure 28

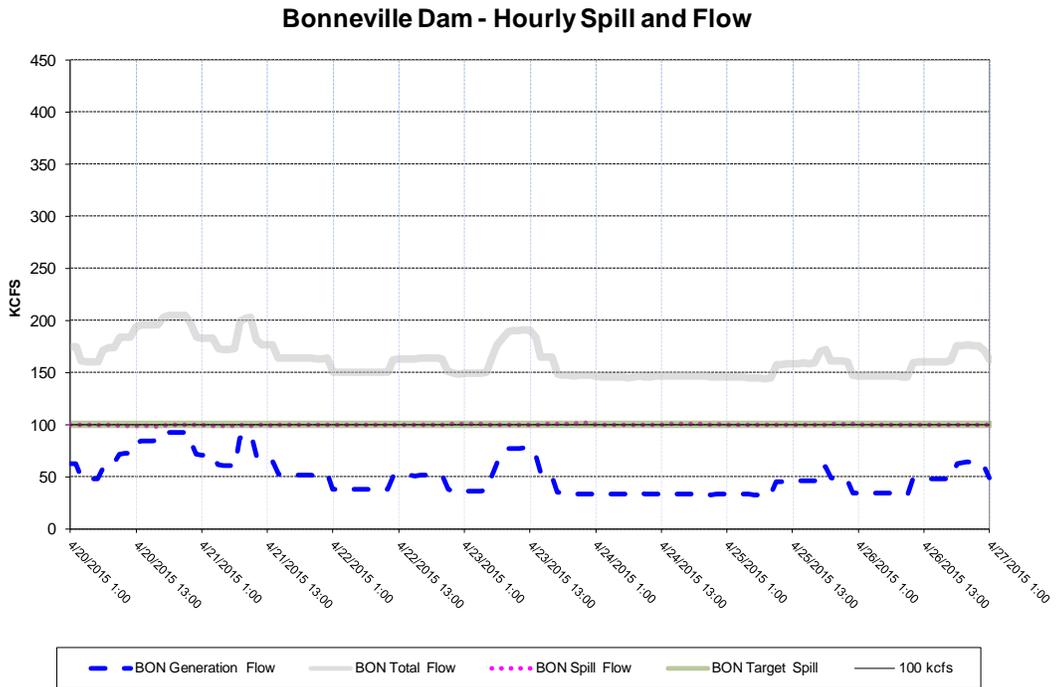
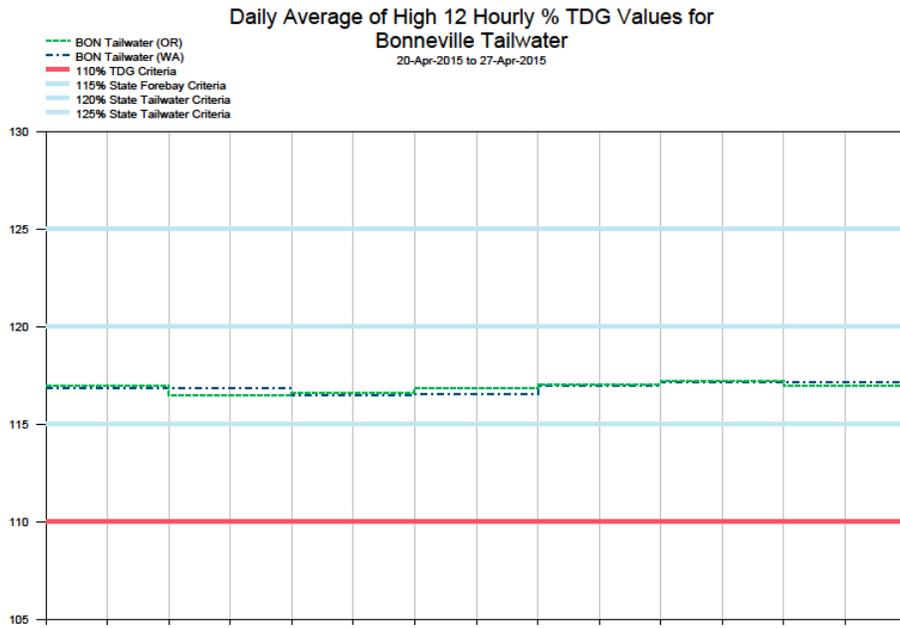


Table 1
Average Percent TDG Values For April 1 – April 26

Date	FIXED MONITORING STATIONS																			
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	IDSW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW	
	WA	WA	WA	WA	WA	WA	WA	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120
4/1/2015	102.5	102.1	102	101.3	101.9	101.5	102	106.6	105.9	111.5	111.5	104.8	108.3	109.5	104.5	105	107.1	104.4	110.3	110.2
4/2/2015	102.1	101.6	101.7	103.1	101.4	101.1	101.5	107.6	104.7	116.5	116.5	104.1	114.3	114.3	103.9	108.1	108.1	105.2	110.6	110.7
4/3/2015	100.9	110.1	102.2	108.8	101.3	117.1	101.4	115.1	104.4	113.2	116.2	104.7	112.6	114.3	106.6	108.4	108.4	105	111	110.8
4/4/2015	101.6	110.4	102.5	109.1	101.8	119.2	101.7	115.4	106.6	113.4	113.4	105	104.1	104.7	106.4	105.9	107.5	108.8	112.7	112.5
4/5/2015	103.2	110.7	103.2	109.9	105.1	126.9	107.2	115.1	107.5	113.7	113.7	106	104.9	104.9	105.3	105.6	105.5	108.8	112.9	112.9
4/6/2015	103.4	111	103.3	110	107.1	117.6	111.3	114.6	107.5	113.7	113.7	106	105.1	105.1	105.2	105.3	105.4	106.9	111.8	112.2
4/7/2015	103.1	111	105.8	111.1	107.9	118	113.9	114.7	107.3	111.4	112.1	108.9	108.2	108.2	106.4	106.4	106.4	105.6	111.4	111.8
4/8/2015	103.2	111	107.6	111.3	108	117.7	114	114	106.8	110.6	111.2	108.9	107.4	108.4	106.7	106.7	106.7	105.3	110.8	111.2
4/9/2015	101.7	111.3	107.8	111.4	107.7	118.1	113.4	114.1	106.6	109.2	109.8	107.5	107.2	107.2	106.7	106.8	106.8	106.1	111.9	111.9
4/10/2015	102.9	111.3	109.3	111.8	109.1	118.8	115.3	113.6	107.9	114.9	114.8	108.1	114.5	114.5	107.7	113.9	113.9	107.4	116.7	116.7
4/11/2015	103	111.4	109.5	111.8	109.9	119	115.7	112.6	107.9	114.1	114.9	108.1	113.5	113.5	108.6	114.2	114.2	107.4	116.4	116.6
4/12/2015	102.3	111.3	108.7	111.6	109.7	118.5	114.5	112.1	106.7	113.7	113.7	106.4	113.5	113.5	108.2	114.1	114.1	109.4	116.7	116.6
4/13/2015	103.1	112.1	109.8	112.2	110	119	113.8	112.4	106.2	114.4	114.5	107.3	113	113.4	110.3	115.6	115.6	111.9	117.2	117
4/14/2015	103.1	112.3	109.8	112.1	110	118.3	113.8	112.7	106.1	113	113.3	107.1	112.6	112.6	109.8	113.4	115	111.9	116.8	117
4/15/2015	101.2	111.1	107	110.9	107.8	118.5	111.2	113.5	103.7	114.2	113.9	104.4	111.8	111.9	106.5	112.7	112.7	108.6	117	117
4/16/2015	101	111.4	106.3	111.2	108.2	118.6	112.4	113	105	114.4	114.4	104.7	112.7	112.7	109.3	114.9	114.9	110.3	117.2	117
4/17/2015	102.5	111.9	107.2	111.9	108.9	119.3	113.6	113.4	106.3	115.3	115.3	105.6	113.5	113.5	110.1	115.6	115.6	112.5	117.4	117.3
4/18/2015	102.5	111.3	107.3	112	109.2	119.2	115.5	113.3	108.3	116.2	116.2	106.6	112.7	113.4	109.9	114.9	115.3	113.9	117.4	117.4
4/19/2015	103.2	111.7	111.3	112.8	112	118.9	118.3	113.7	109.1	116.5	116.5	107.9	114.1	114.1	111.4	116.2	116.2	114.5	117.3	117.3
4/20/2015	106.2	111.7	114.9	113.7	113	118.4	119.4	113.7	110	116.6	116.6	109.9	113.9	114.1	112	116.8	116.8	115.9	117.2	117
4/21/2015	106.1	111.6	116.9	114.2	113.6	118.6	120.4	114.2	110.7	116.7	116.5	110.5	113.9	113.8	111.9	116.2	116.6	115.9	116.7	117
4/22/2015	105.3	111.5	115.4	113.7	113.6	118.4	120.2	114.6	110.4	116.3	116.3	109.5	114	114	109.7	114.1	115.2	112.9	116.9	116.7
4/23/2015	103.7	110.9	113.6	112.8	114.2	118.7	118.4	115.4	109.3	116.4	116.4	109.9	114	113.9	109.5	115.3	115.3	109.1	117.1	116.8
4/24/2015	103.6	110.8	113.4	112.2	114.2	118.7	117.5	115.1	108.9	115.7	115.4	109.9	114.1	114.1	110.1	115.4	115.4	110.4	117.2	117.2
4/25/2015	102.6	110.8	112.4	111.9	112.9	118.5	115.6	114.8	108	116.2	116	109.2	113.8	113.8	110	114.9	115.1	111.6	117.5	117.4
4/26/2015	101.7	110.8	111.1	111.4	111.6	118.2	114.6	114.8	107.5	116.1	116.1	108.4	113.6	113.6	109.5	114.4	114.4	111.6	117.1	117.3

Total Dissolved Gas Monitoring Stations

Code	Station Name
LWG	Lower Granite Forebay
LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay
LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay
LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay
IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay
MCPW	McNary Tailwater
JDY	John Day Forebay
JHAW	John Day Tailwater
TDA	The Dalles Forebay
TDDO	The Dalles Tailwater
BON	Bonneville Forebay
CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal