

Appendix D

2015 FOP Implementation Reports

**With Hourly Spill, Flow
and TDG Graphs**

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FISH OPERATIONS PLAN IMPLEMENTATION REPORT

April 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' April 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in April 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in April displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

¹ Averages reported are consistent with the current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and the Washington TDG criteria adjustments have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented from Monday through Sunday.

The weekly figures begin on March 30 and end on April 26 for the following lower Snake River and lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on March 30 for the lower Snake River and the lower Columbia River projects.

March 30 – April 5	Figures 1 – 4
April 6 – April 12	Figures 5 – 12
April 13 – April 19	Figures 13 – 20
April 20 – April 26	Figures 21 – 28

A. Upper Figure: Displays the average daily %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the Oregon 120%TDG standard modification limit for the tailwater of the dam.
2. The blue dot-dash line represents the Washington 120%TDG criteria adjustment for the tailwater of the dam.
3. The black solid line represents the Washington 115%TDG criteria adjustment for the forebay of the next dam downstream.

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

II. A table is included at the end of the figures that lists the average daily %TDG for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects,

tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the April 2015 Spill Variance Table.³ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour (except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams⁴, which may

³ Involuntary spill conditions appear in the figures, but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

⁴ As specified in the 2015 FOP (p. 14), this applies when the spill level is below 40% of total flow at The Dalles Dam.

range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

April 2015 Operations

The month of April was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the April 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 2.9 MAF (Million Acre Feet) or 64% of average as measured at Lower Granite Dam. For the lower Columbia, the Runoff Processor indicated the April 2015 adjusted volume runoff was below the 30 year average (1981-2010): 11.5 MAF or 83% of average as measured at The Dalles. The monthly precipitation summary for April was well below average at 53% on the Snake River above Ice Harbor Dam and also well below average on the Columbia River above The Dalles Dam at 51%.

During the April 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 20 kcfs, 24 hours/day.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day.

- Lower Monumental Dam - The hourly target spill level was the %TDG cap, 24 hours/day.
- Ice Harbor Dam - The hourly target spill level was 45 kcfs during the daytime and the %TDG cap during the nighttime. From April 10 – 14, the hourly target spill level was 30% of total project outflow, 24 hours/day⁵. Nighttime spill hours are 1800-0500.
- McNary Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- John Day Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level was 100 kcfs, 24 hours/day.

Operational Adjustments

No Operational Adjustments to report.

⁵ Spill operation treatments were rearranged as discussed on page 12 of the 2015 FOP to accommodate a post-construction evaluation of modifications made to Ice Harbor spillbay 2 to improve juvenile fish passage survival. This evaluation is described in FPP Appendix A, and the rearrangement of spill operation treatments was further coordinated through the FPOM on April 9.

April 2015 Spill Variance Table

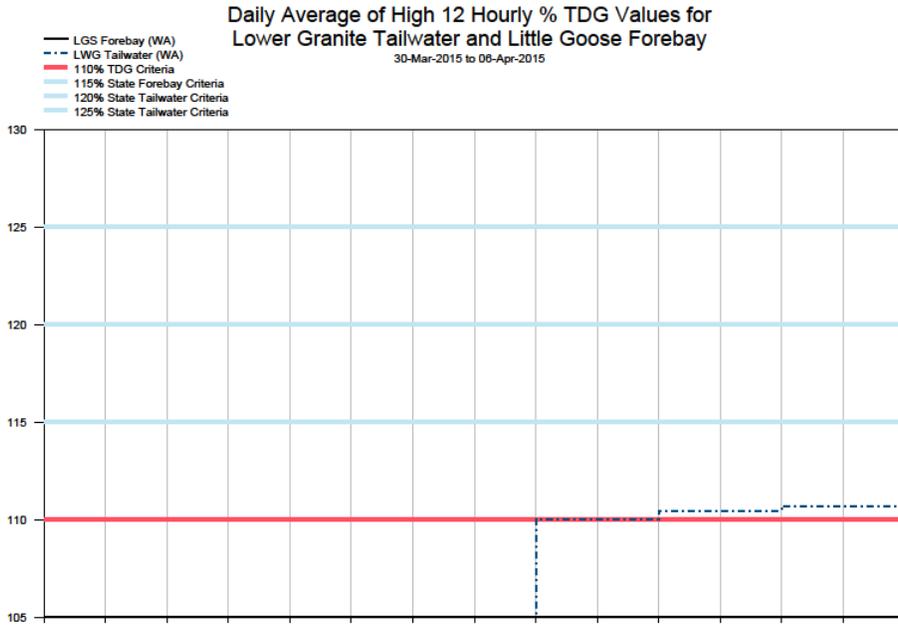
Table 1: April 2015 (4/1 – 4/26) – FOP Implementation Report Table

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Little Goose	Reduced Spill	4/9/15	1700	1	Maintenance	Hourly spill decreased to 28.6% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock for a dam safety inspection. 24-hr avg spill was 29.8%.
Little Goose	Reduced Spill	4/11/15	1600	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range). Reduced spill for safe passage of barge. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/13/15	1700	1	Navigation	Hourly spill decreased to 28.0% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 30.0%.
Little Goose	Reduced Spill	4/15/15	1900	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range). Reduced spill for safe passage of fish barge. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/17/15	0300	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/21/15	1700	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Little Goose	Reduced Spill	4/26/15	1600	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill was 29.9%.
Ice Harbor	Additional Spill	4/13/15	2000 – 2300	4	Operational Limitations	Hourly spill ranged from 35.7% to 42.0% (above 30.0% \pm 1%). Hourly total project outflow ranged from 18.1 to 22.1 kcfs. Due to RSW, minimum spill is fixed at approx 7.5-8.4 kcfs, which results in spill >FOP target when total outflow is approx 17-26 kcfs. 24-hr avg spill was 31.6%.

⁶ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Ice Harbor	Additional Spill	4/23/15	1800	1	Human/Program Error	Hourly spill increased to 50.5 kcfs (above 45 kcfs \pm 2 kcfs range) due to a miscalculation above minimum generation range (8.2-10.0 kcfs).
McNary	Additional Spill	4/12/15	2300	1	Human/Program Error	Hourly spill increased to 41.3% (above 40.0% \pm 1% range) due to a miscalculation. 24-hr avg spill was 40.3%.
John Day	Additional Spill	4/10/15	1400	1	Transmission Stability	Hourly spill increased to 31.1% (above 30.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 29.9%.
John Day	Additional Spill	4/23/15	2300	1	Transmission Stability	Hourly spill increased to 31.3% (above 30.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 30.0%.
The Dalles	Additional Spill	4/13/15	2100	1	Transmission Stability	Hourly spill increased to 41.3% (above 40.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill was 39.9%.

Figure 1



Lower Granite Dam - Hourly Spill and Flow

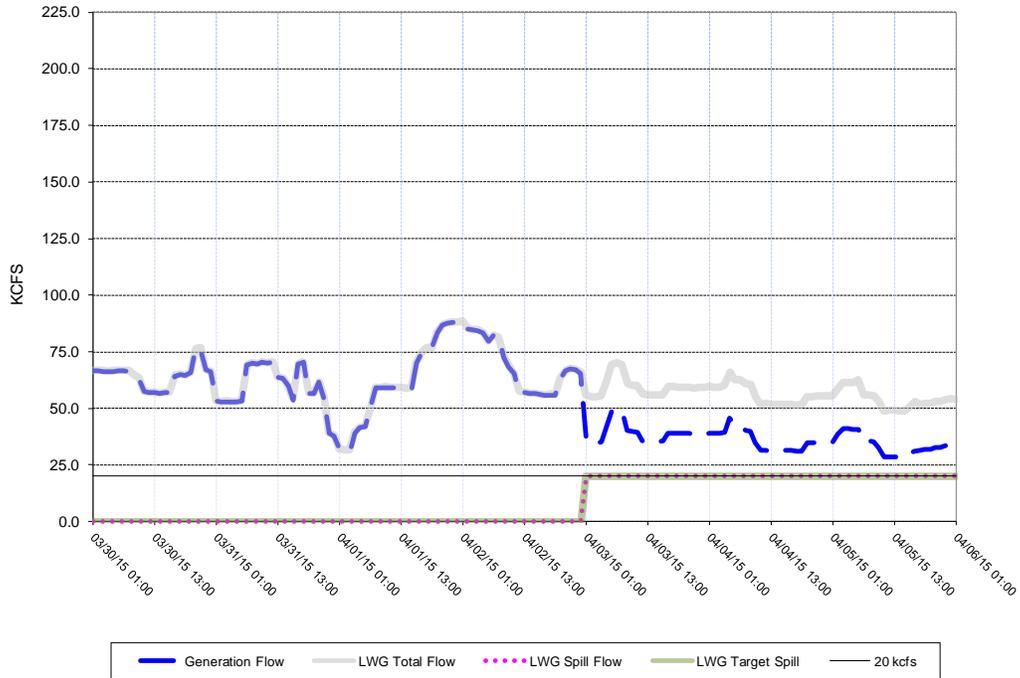
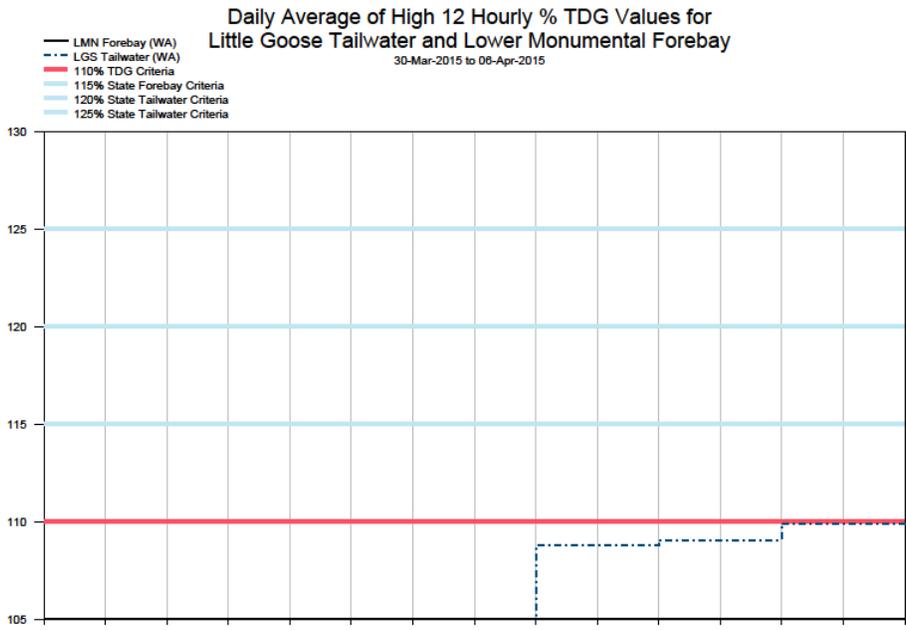


Figure 2



Little Goose Dam - Hourly Spill and Flow

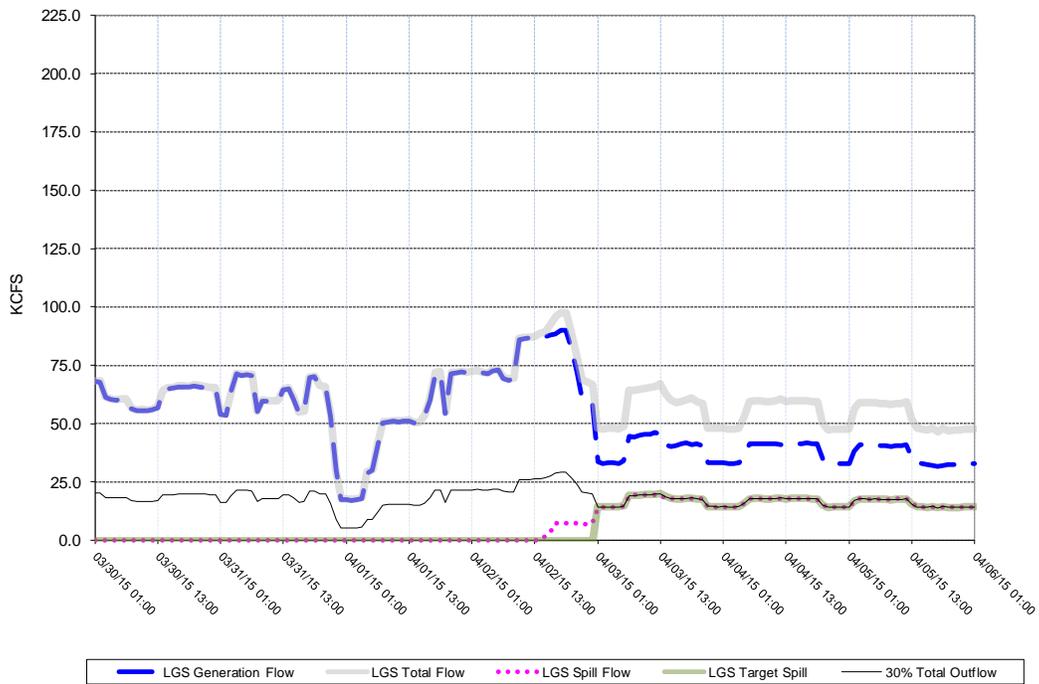


Figure 3

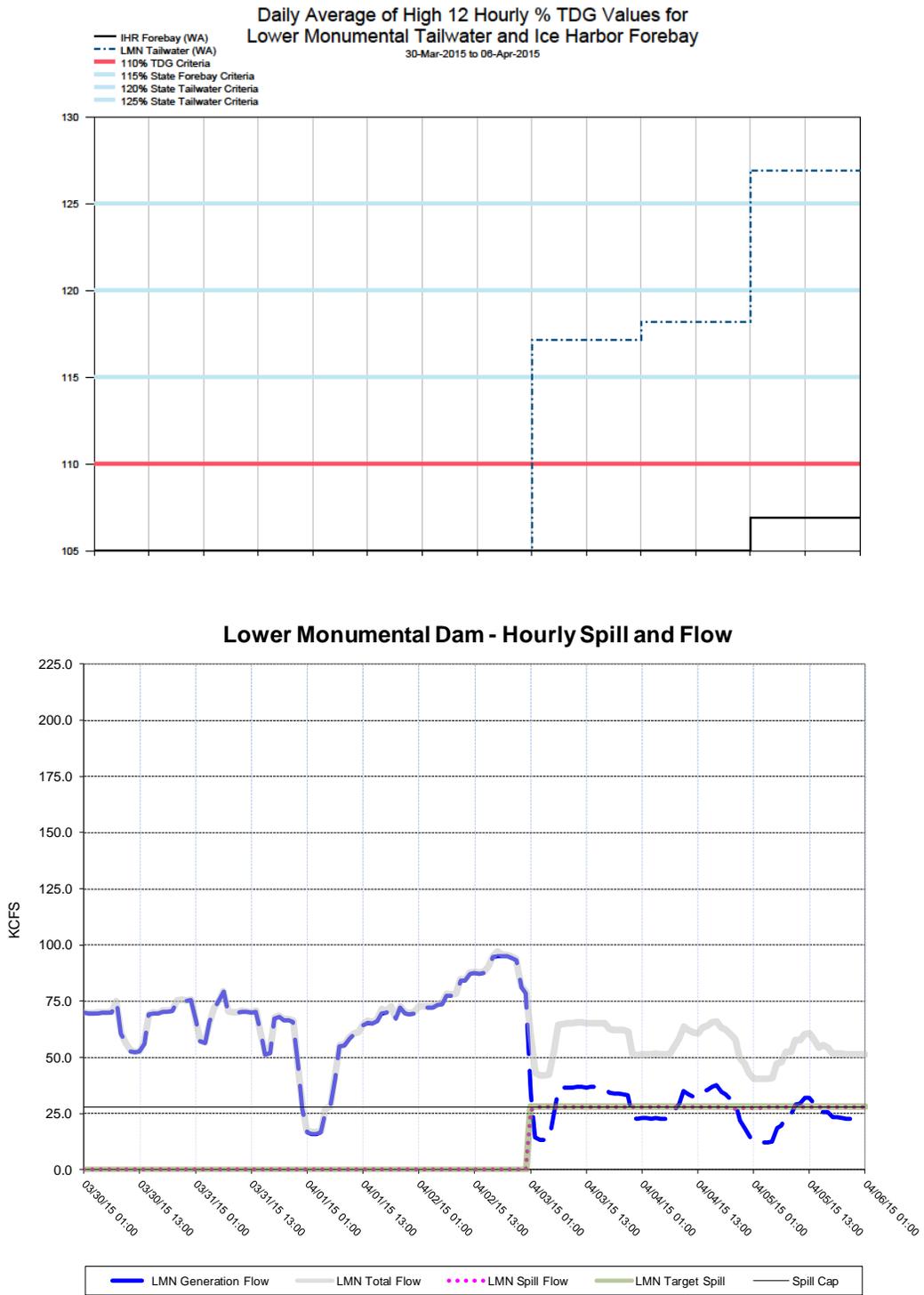


Figure 4

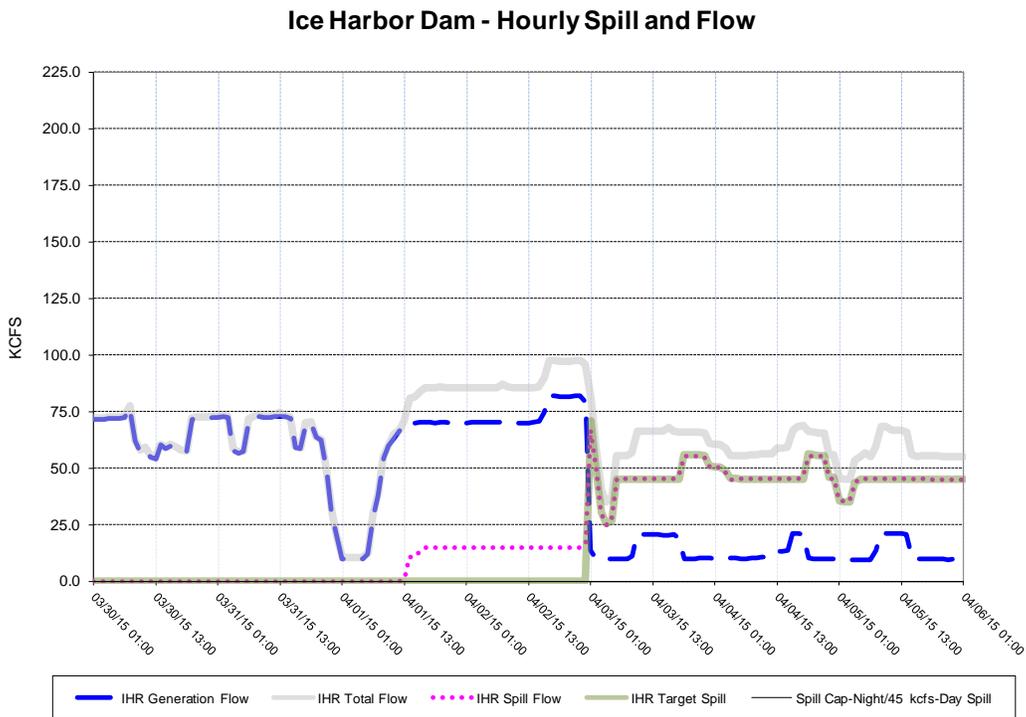
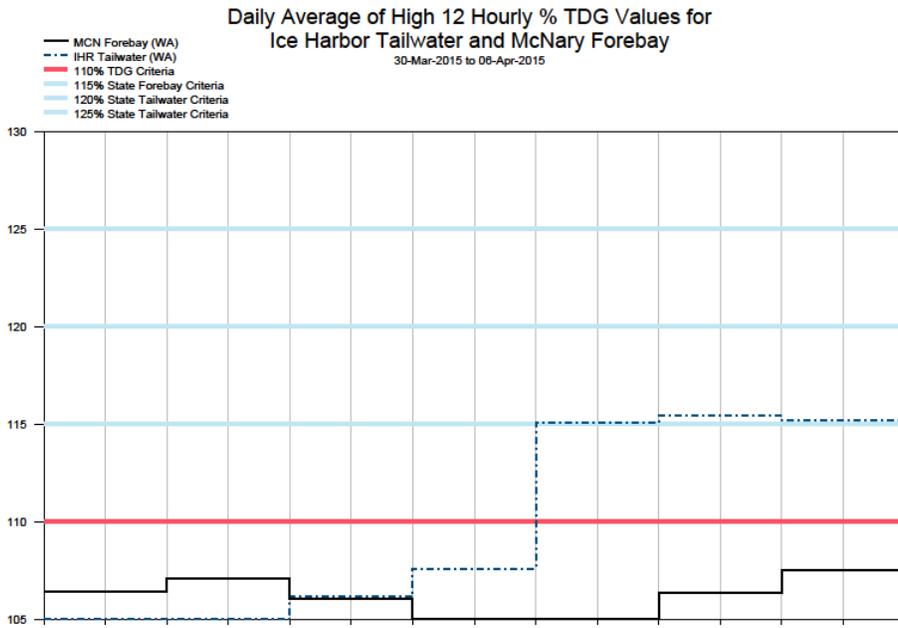


Figure 5

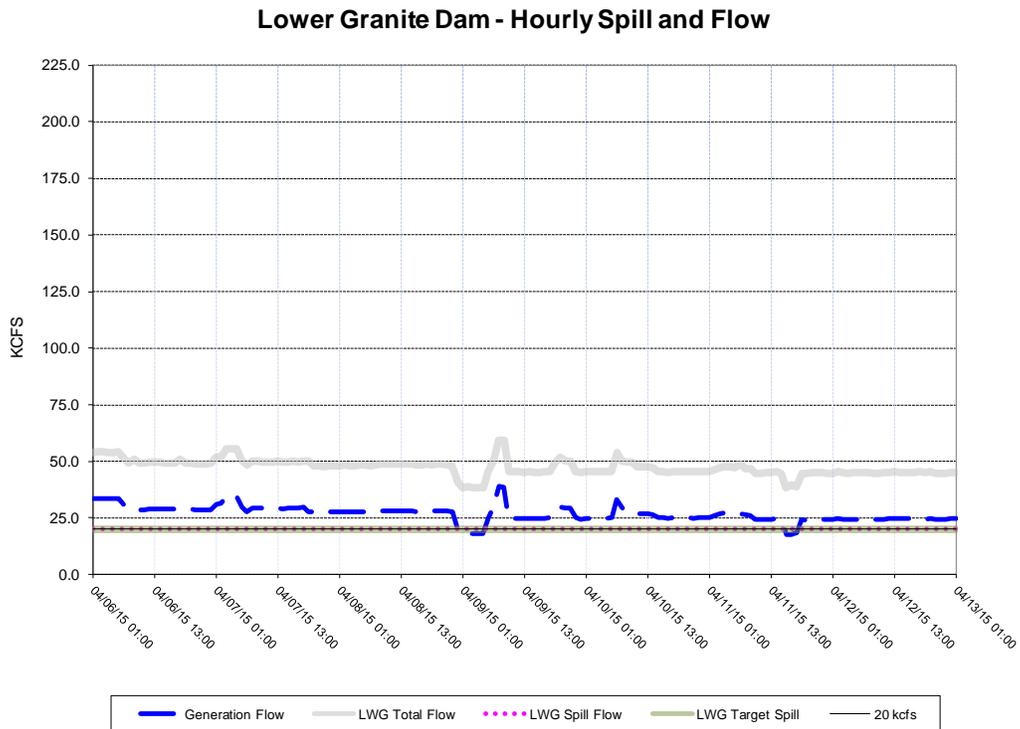
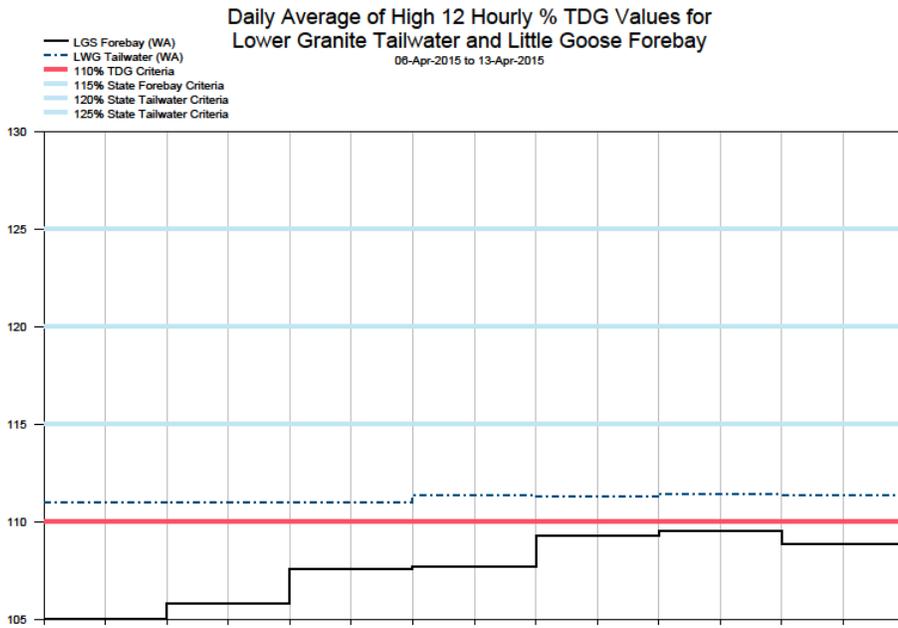
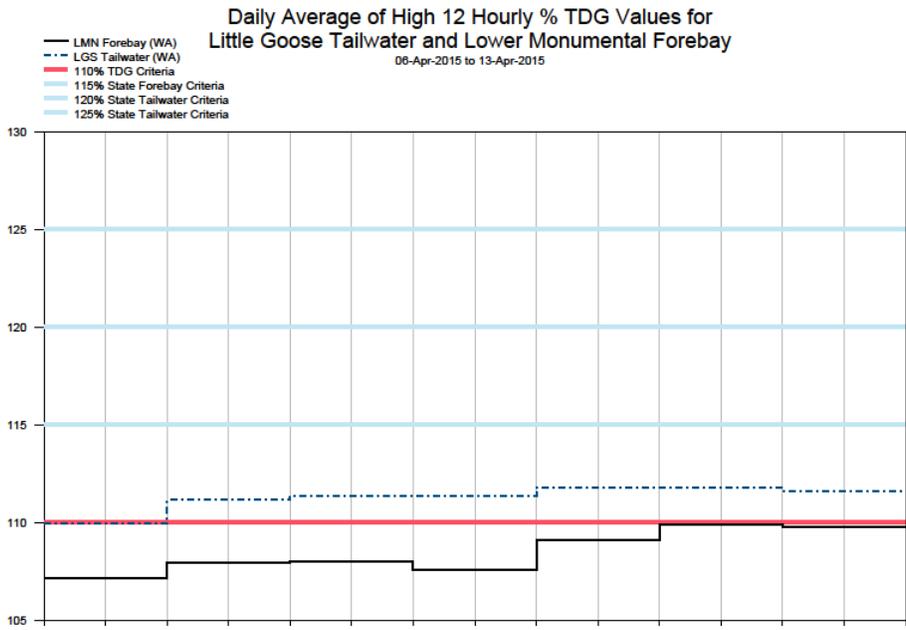


Figure 6



Little Goose Dam - Hourly Spill and Flow

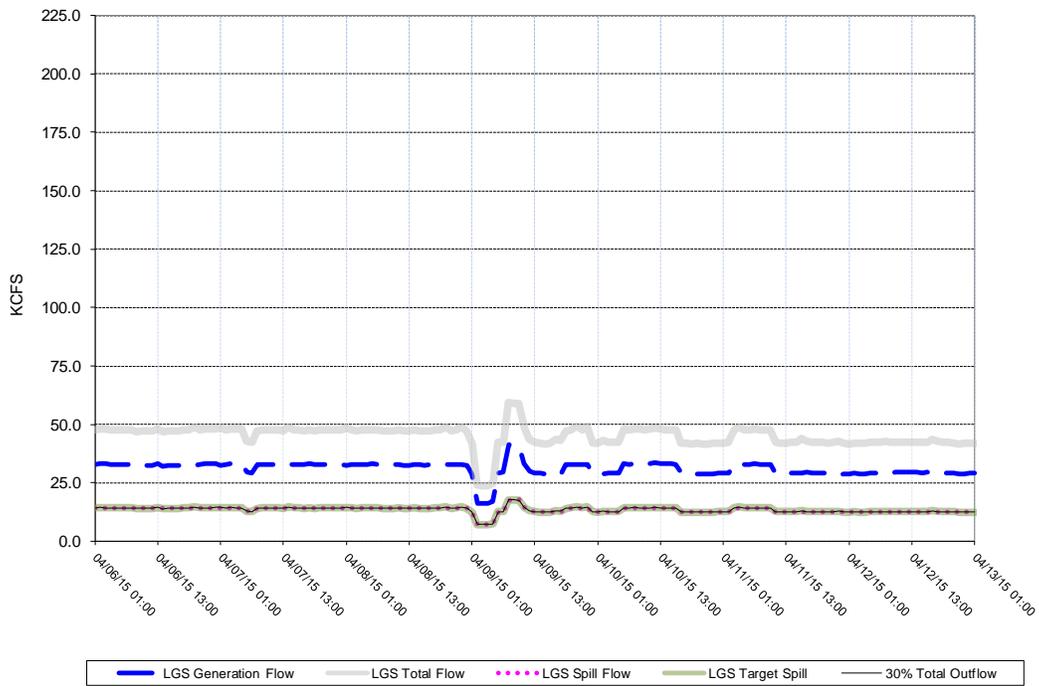


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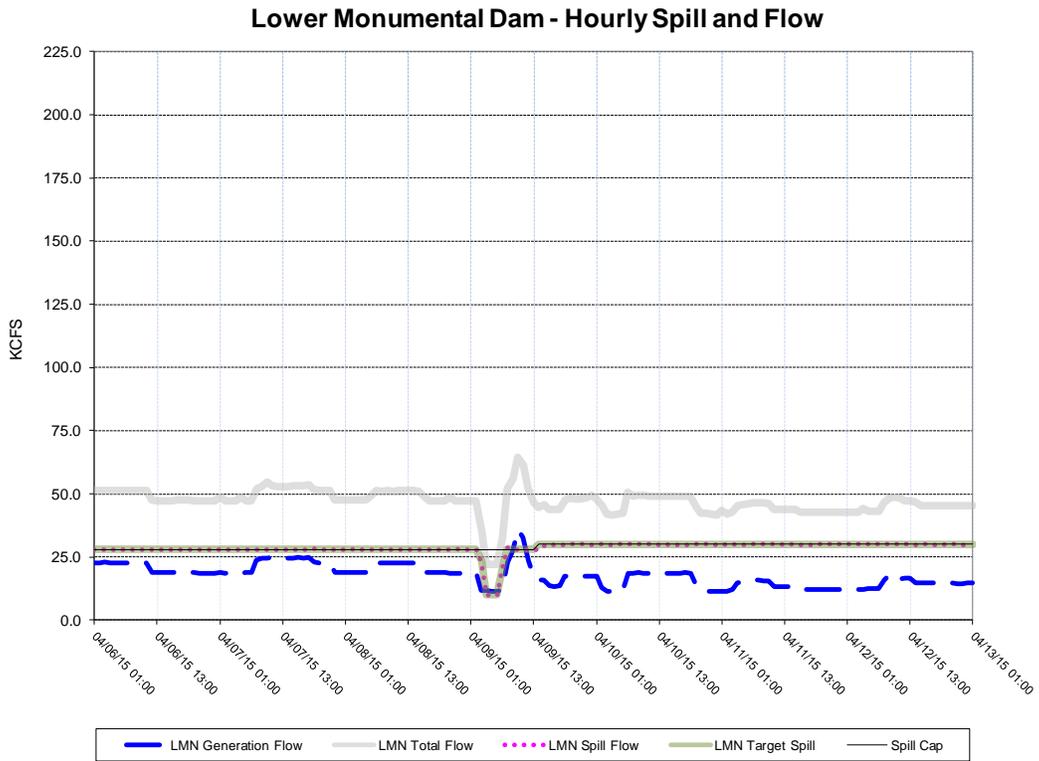
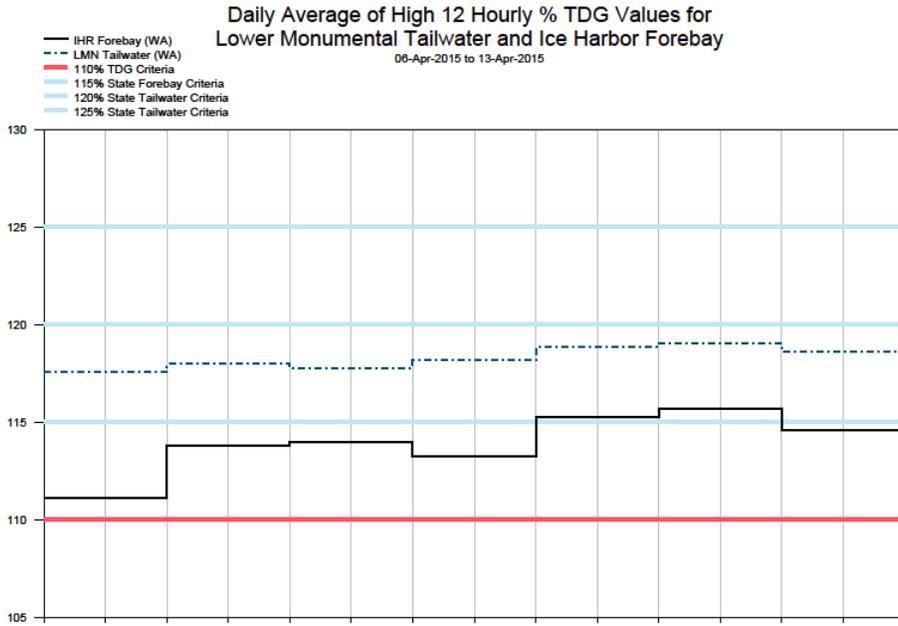


Figure 8

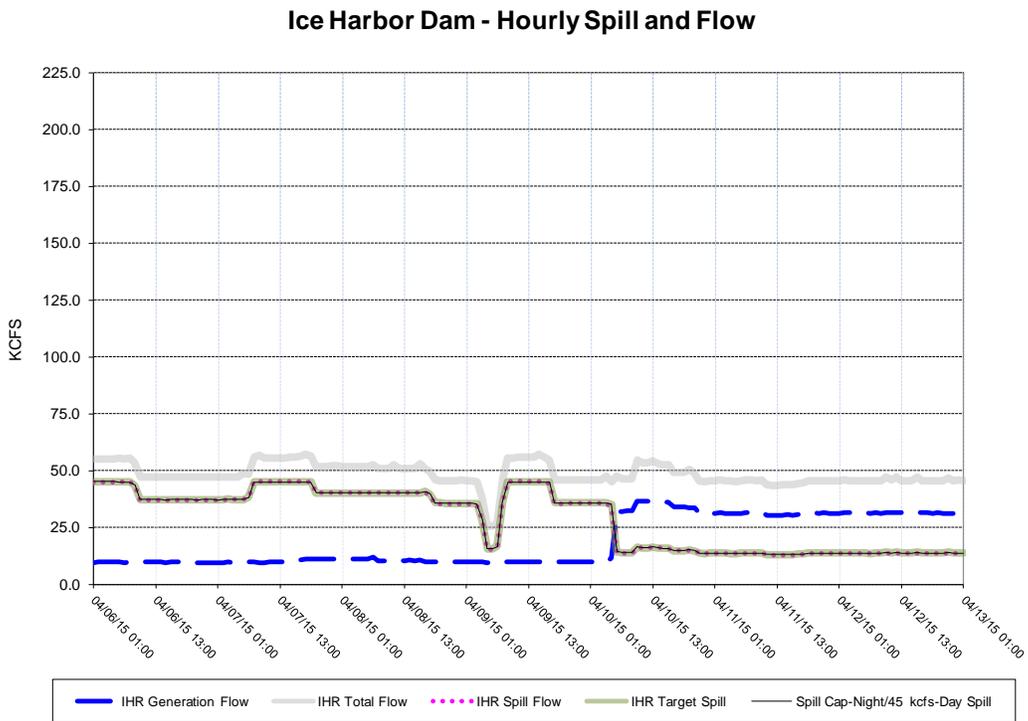
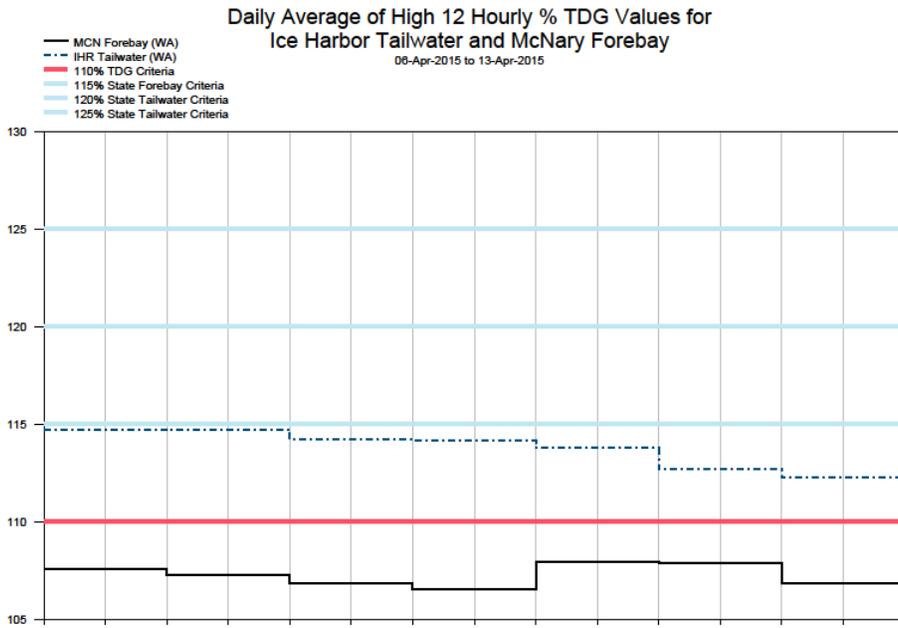
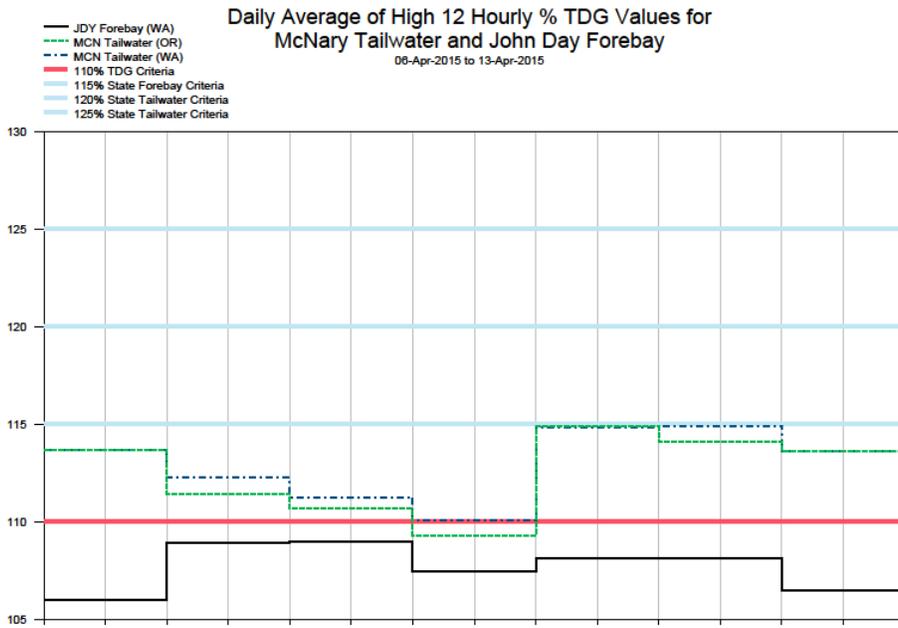


Figure 9



McNary Dam - Hourly Spill and Flow

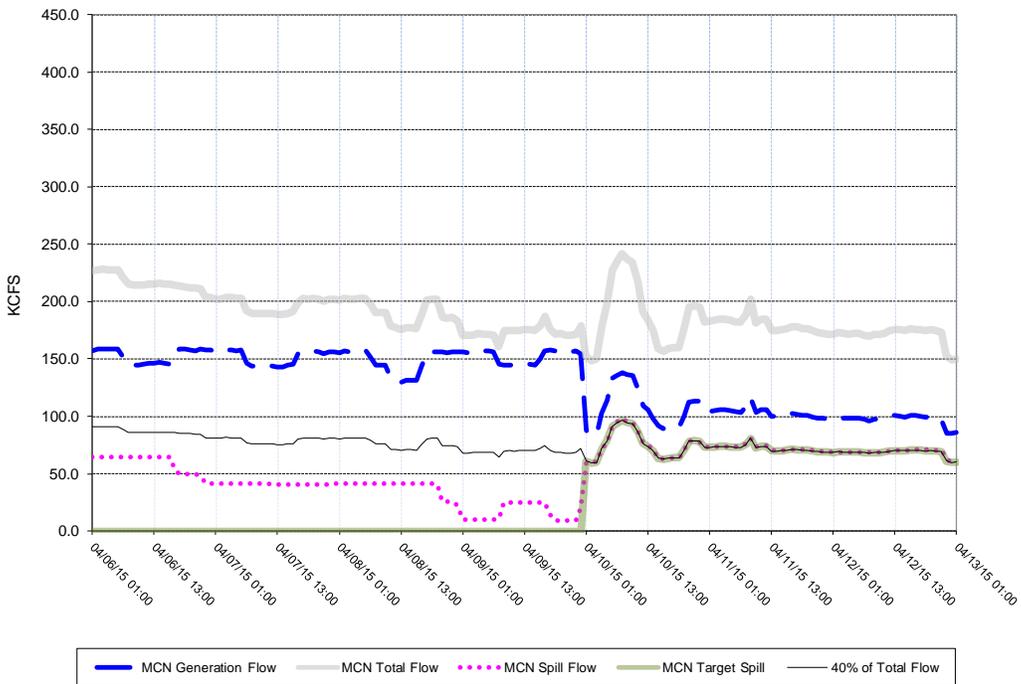
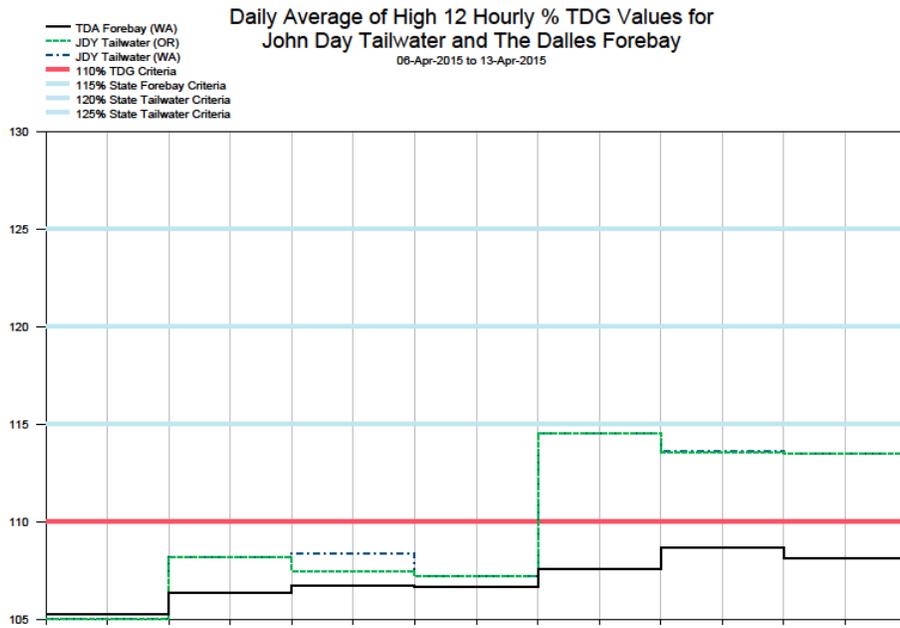


Figure 10



John Day Dam - Hourly Spill and Flow

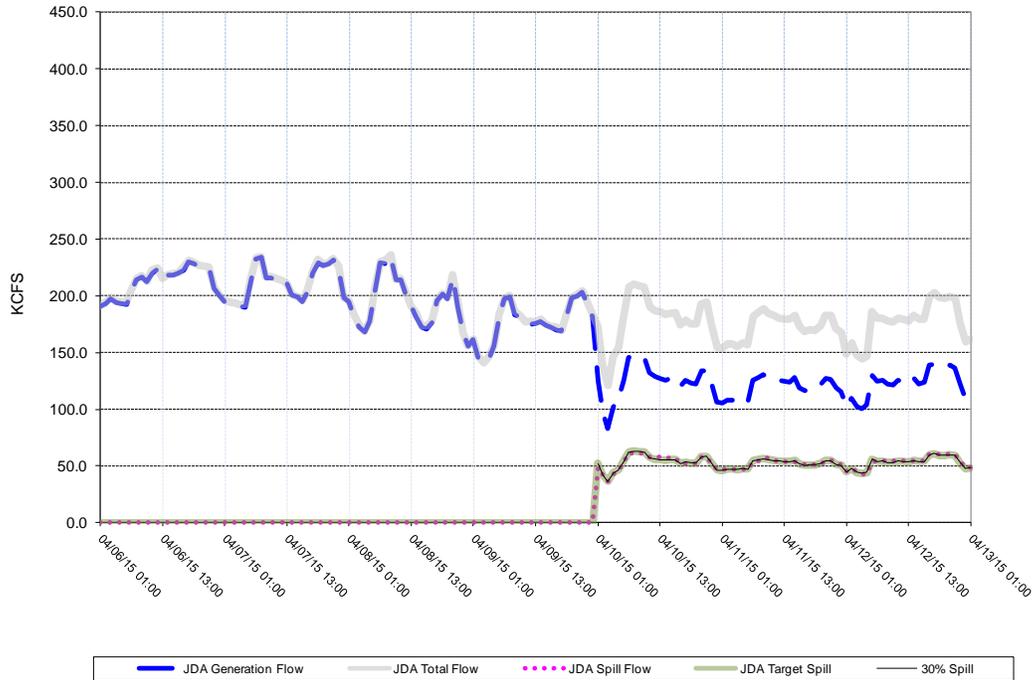
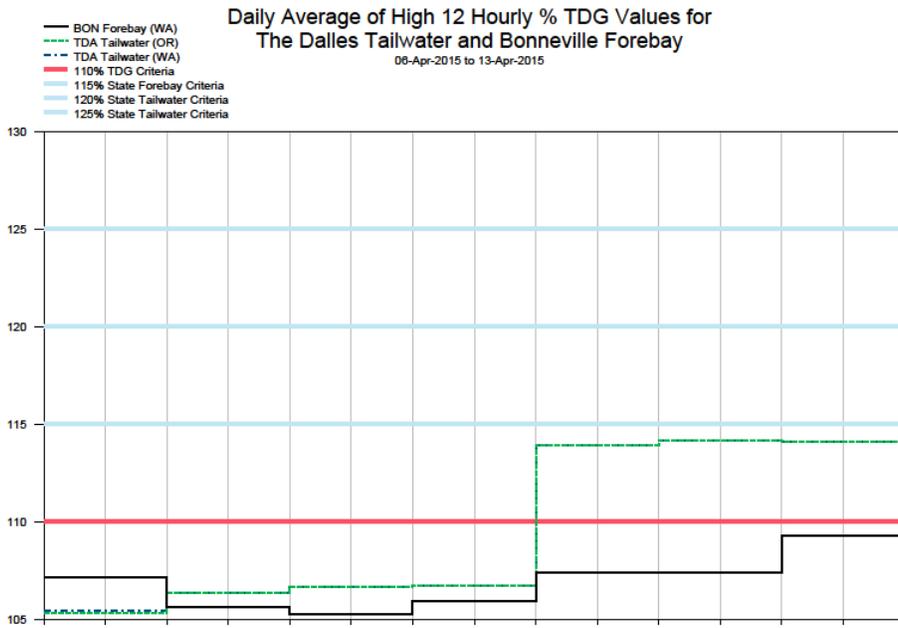


Figure 11



The Dalles Dam - Hourly Spill and Flow

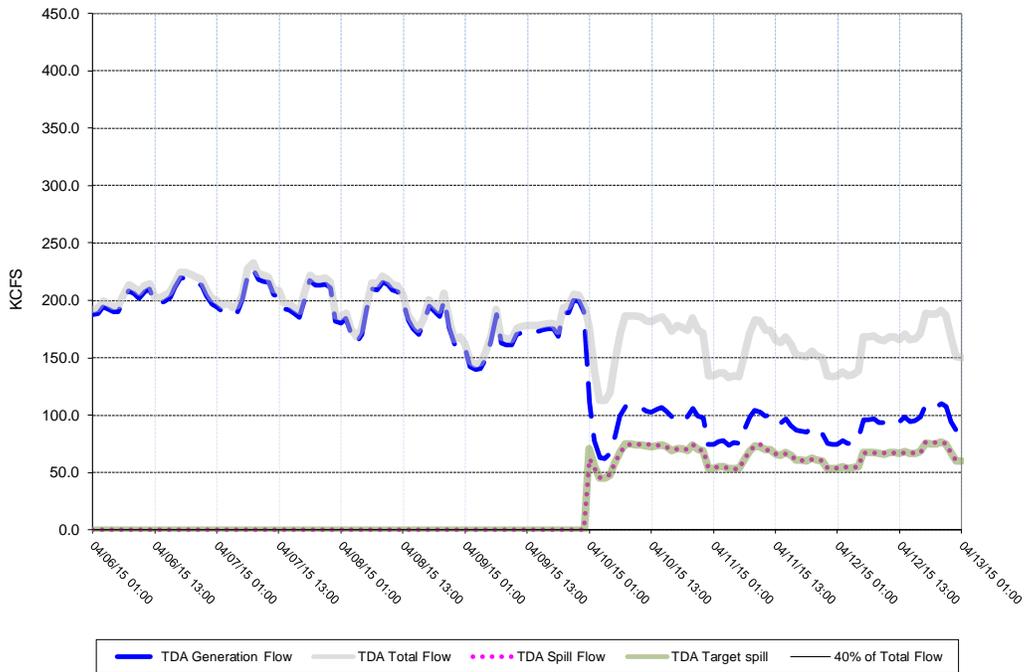


Figure 12

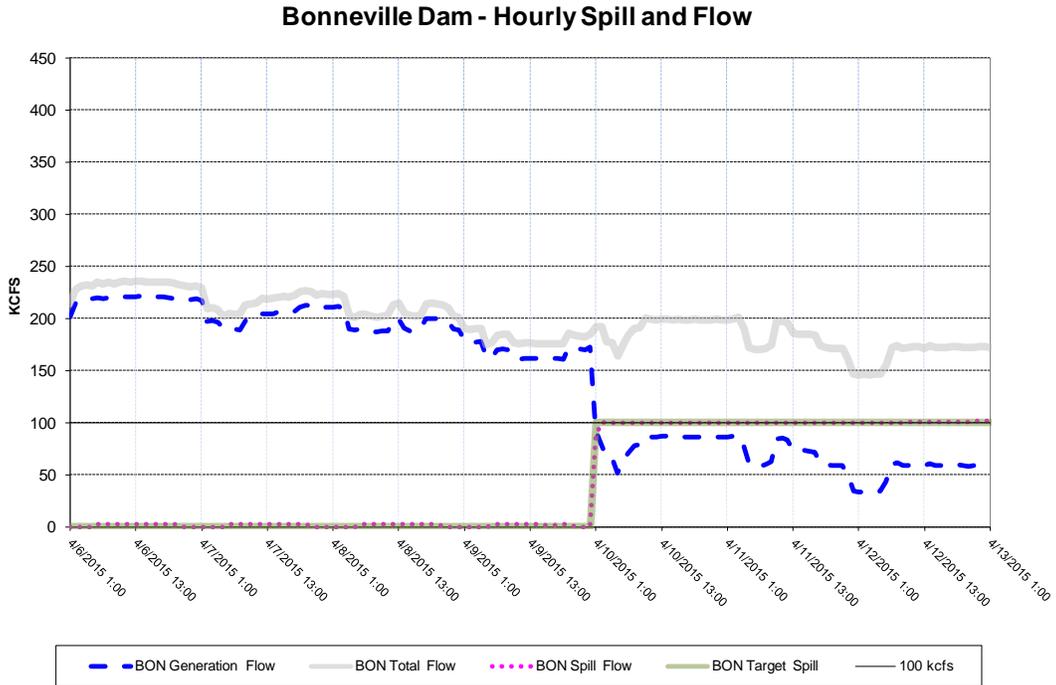
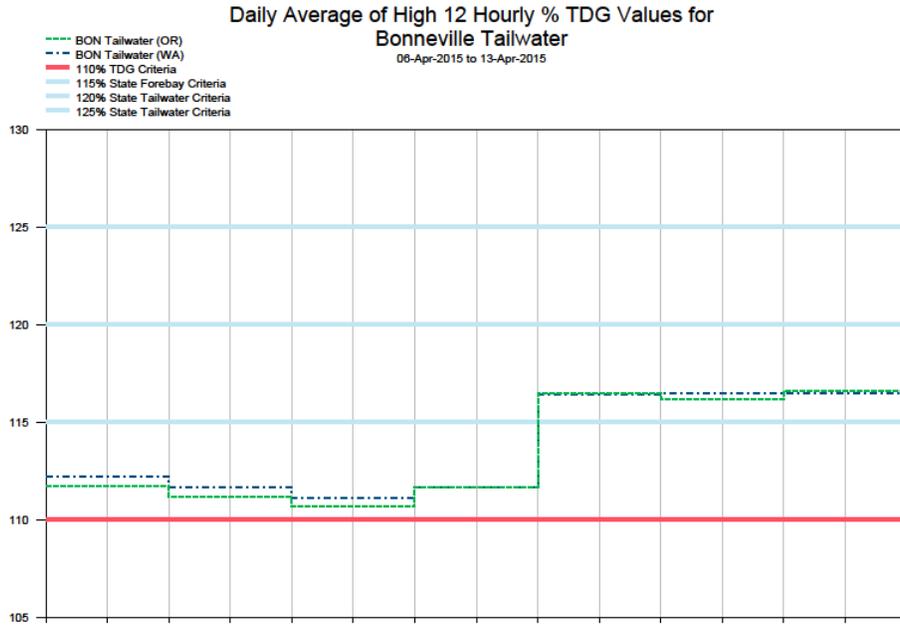


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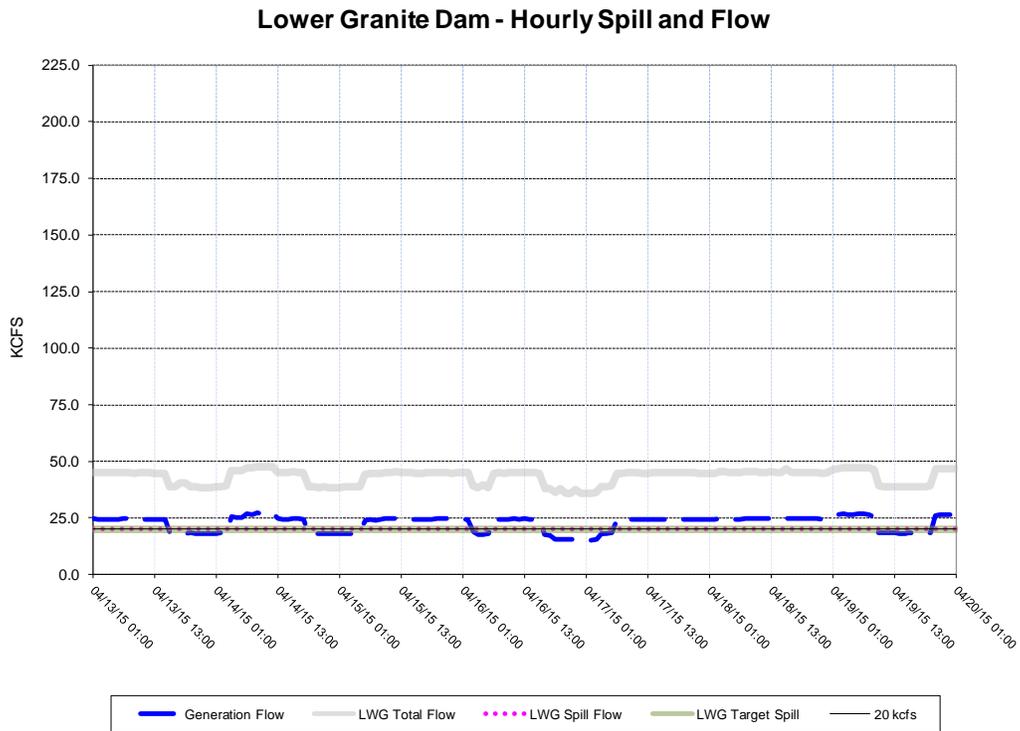
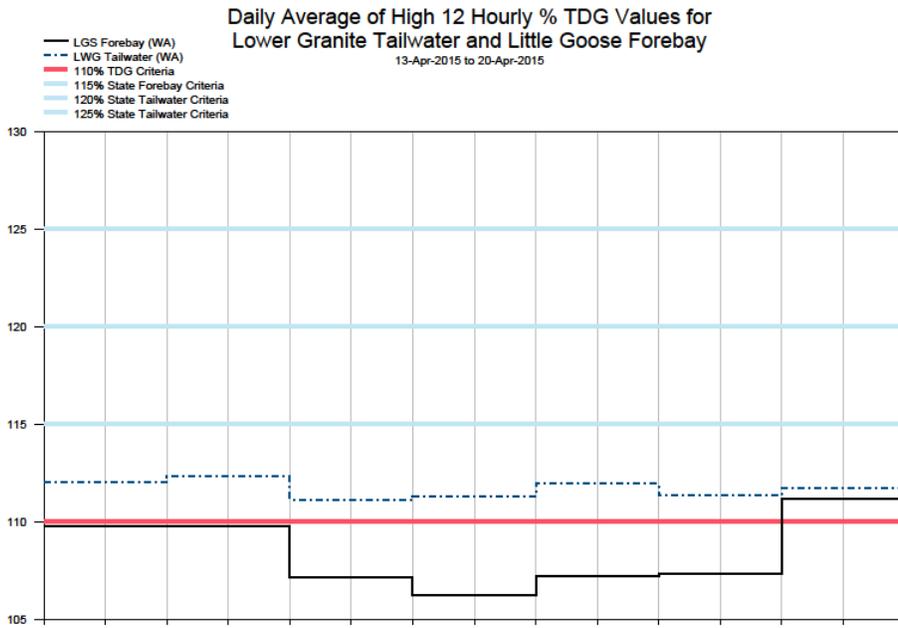
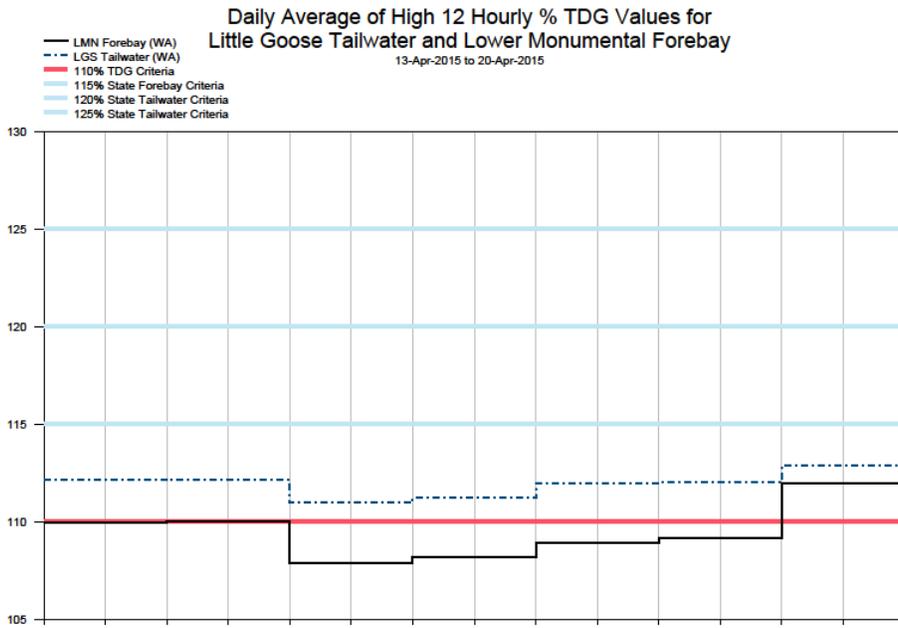


Figure 14



Little Goose Dam - Hourly Spill and Flow

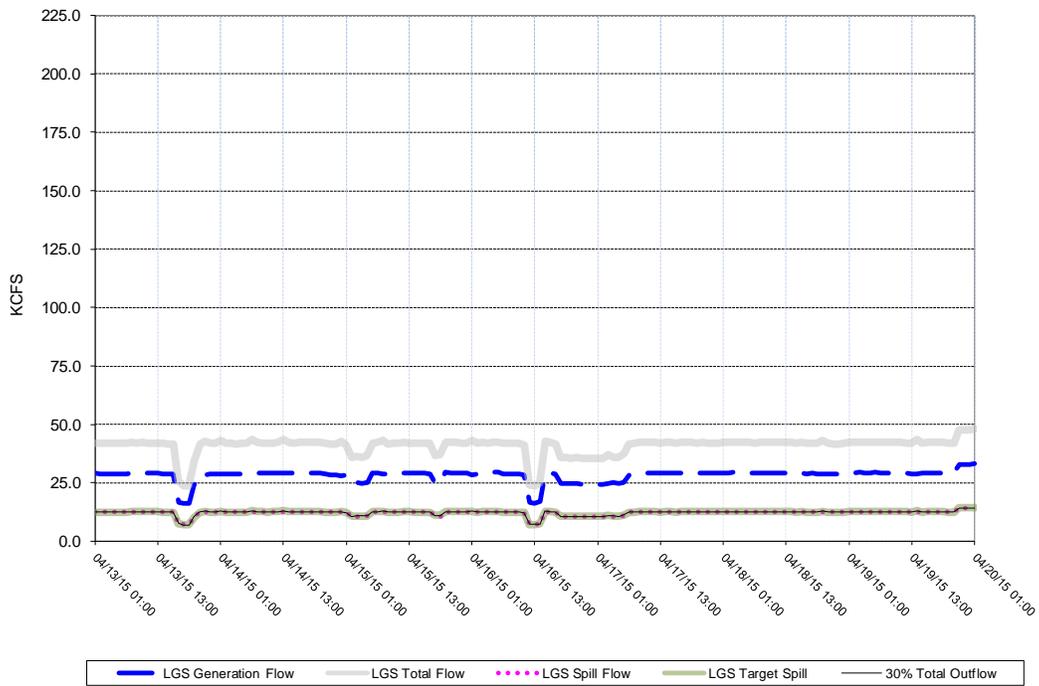


Figure 15

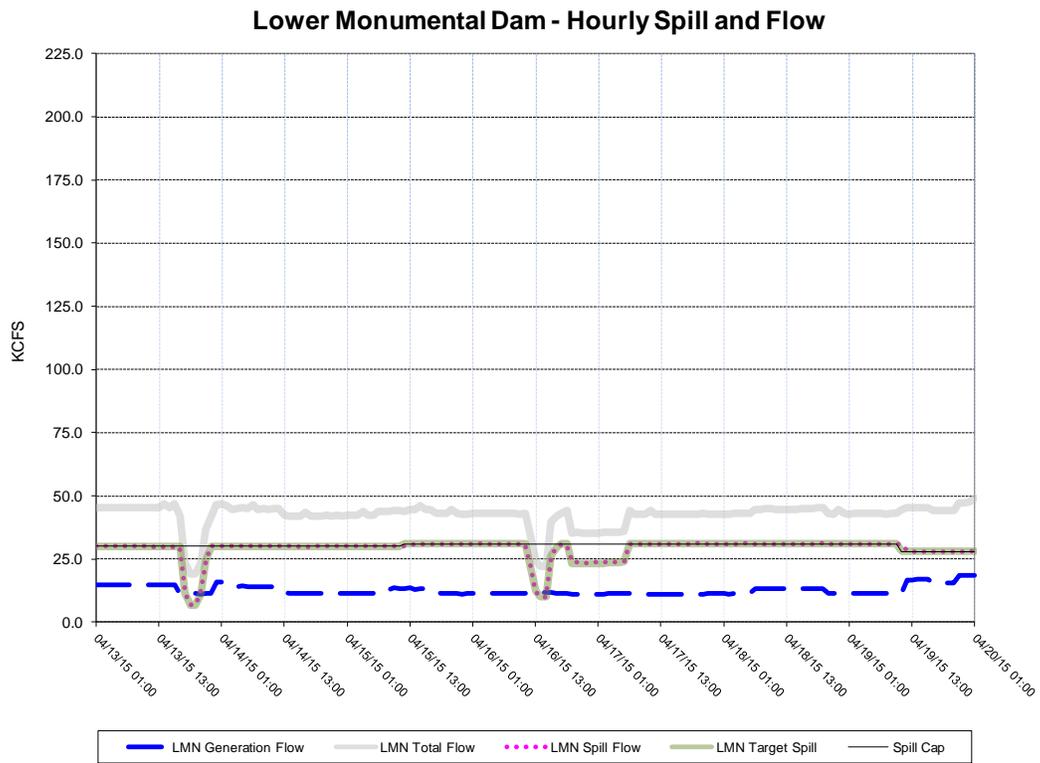
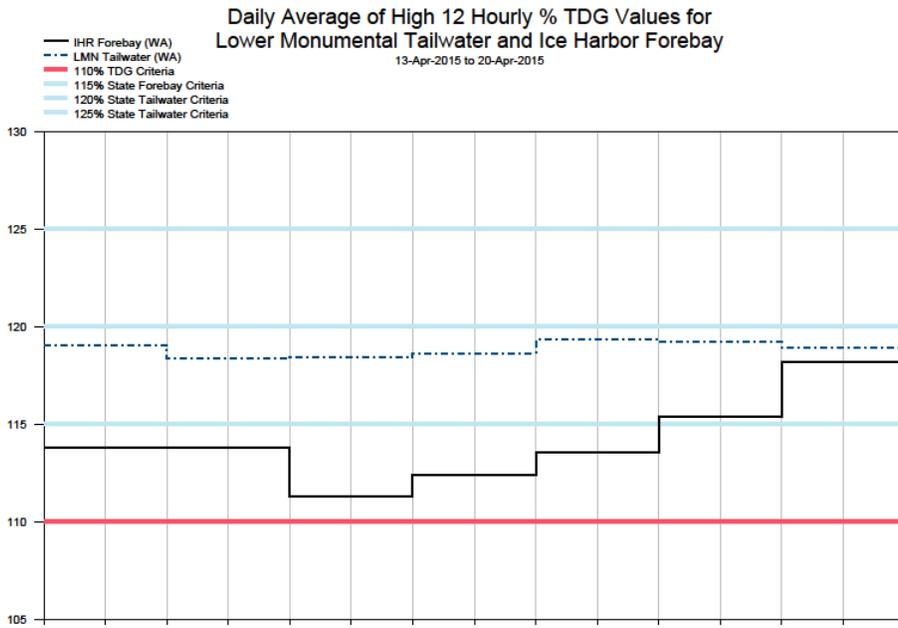


Figure 16

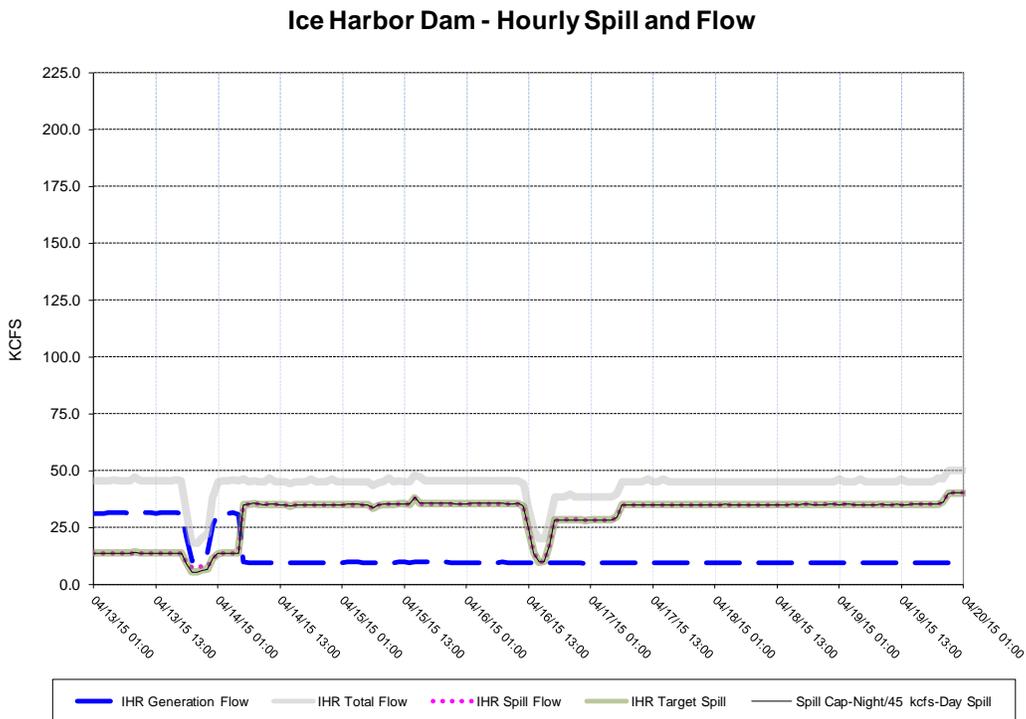
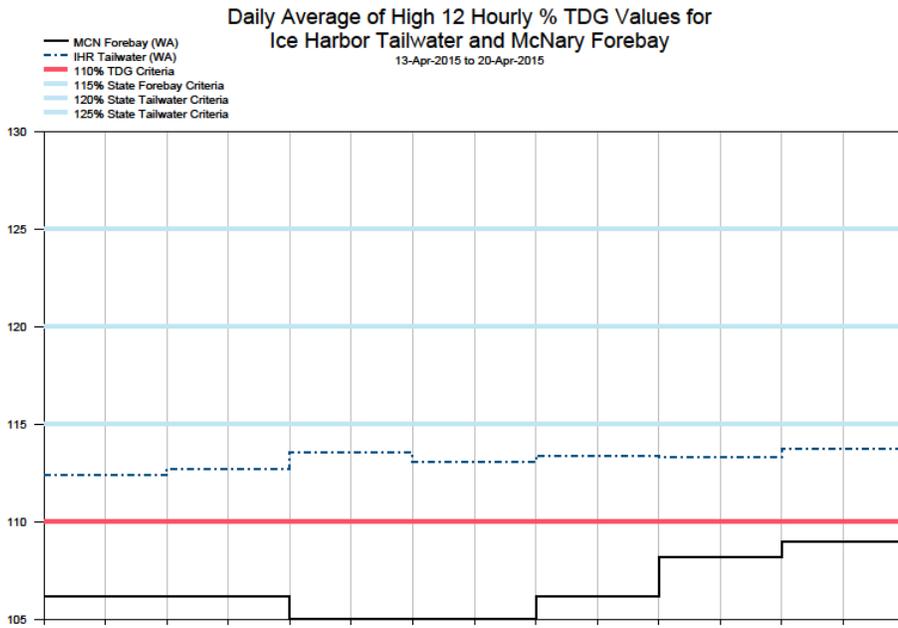
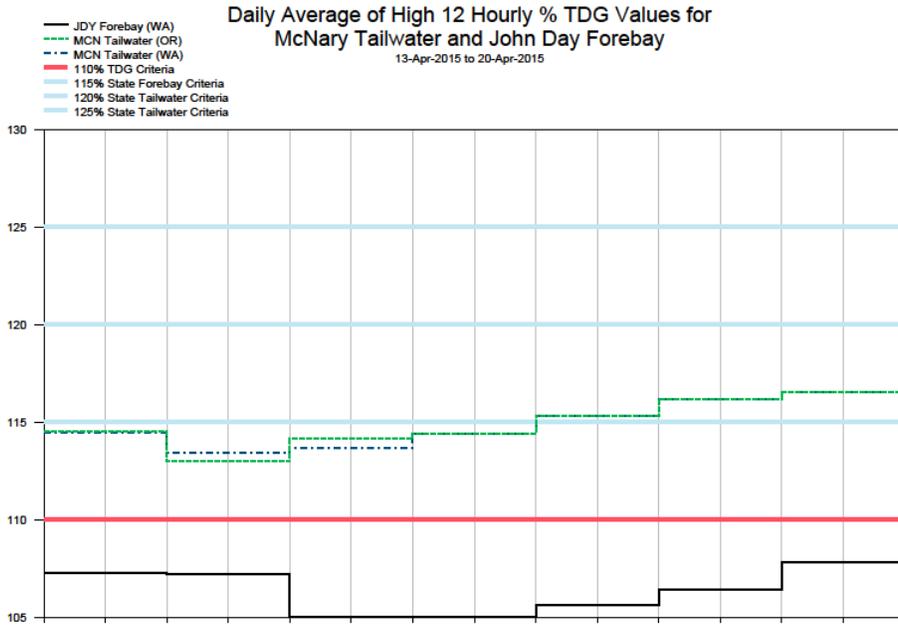


Figure 17



McNary Dam - Hourly Spill and Flow

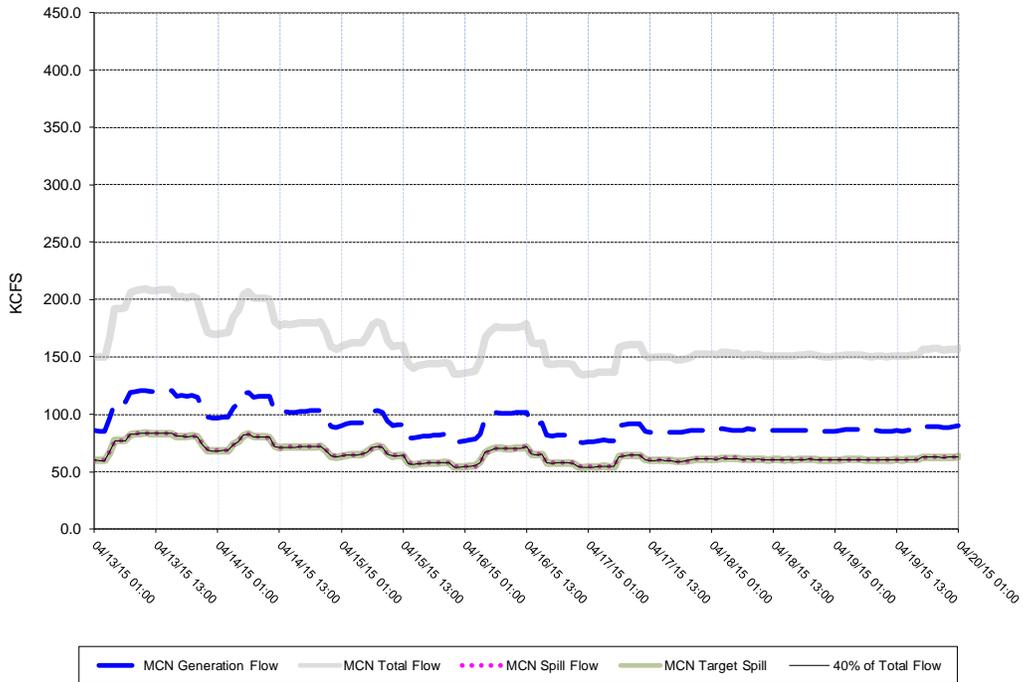
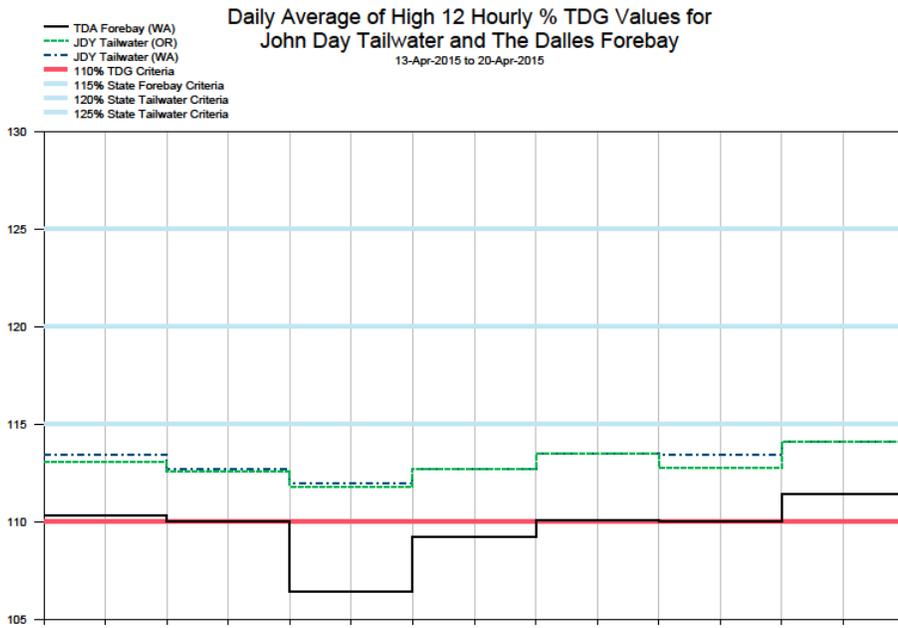


Figure 18



John Day Dam - Hourly Spill and Flow

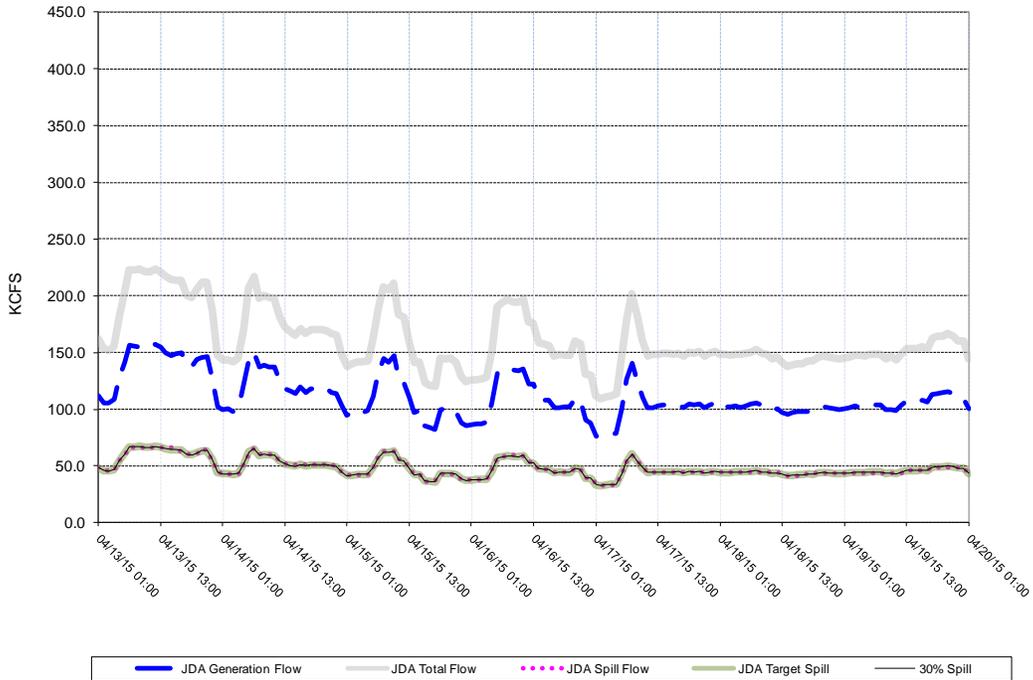
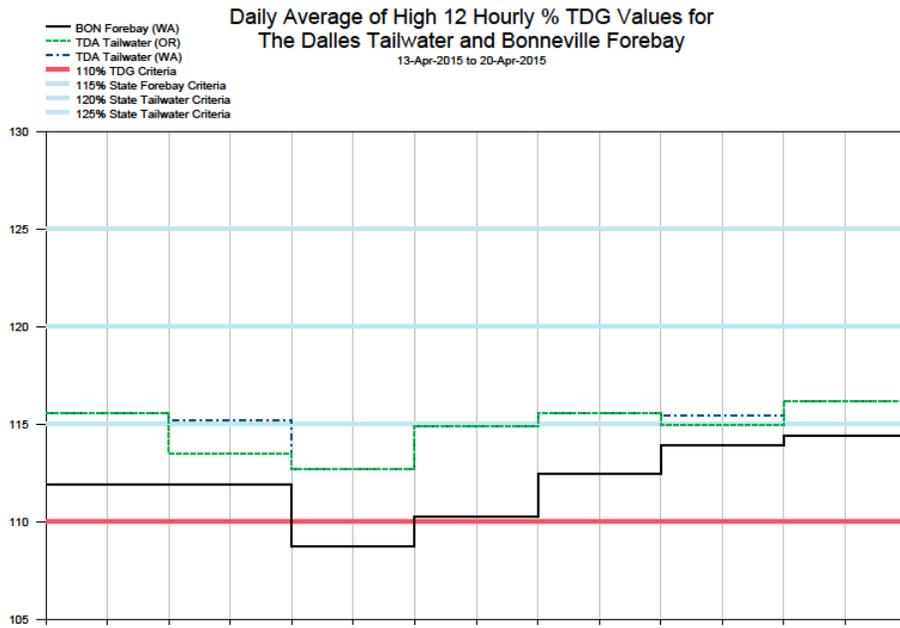


Figure 19



The Dalles Dam - Hourly Spill and Flow

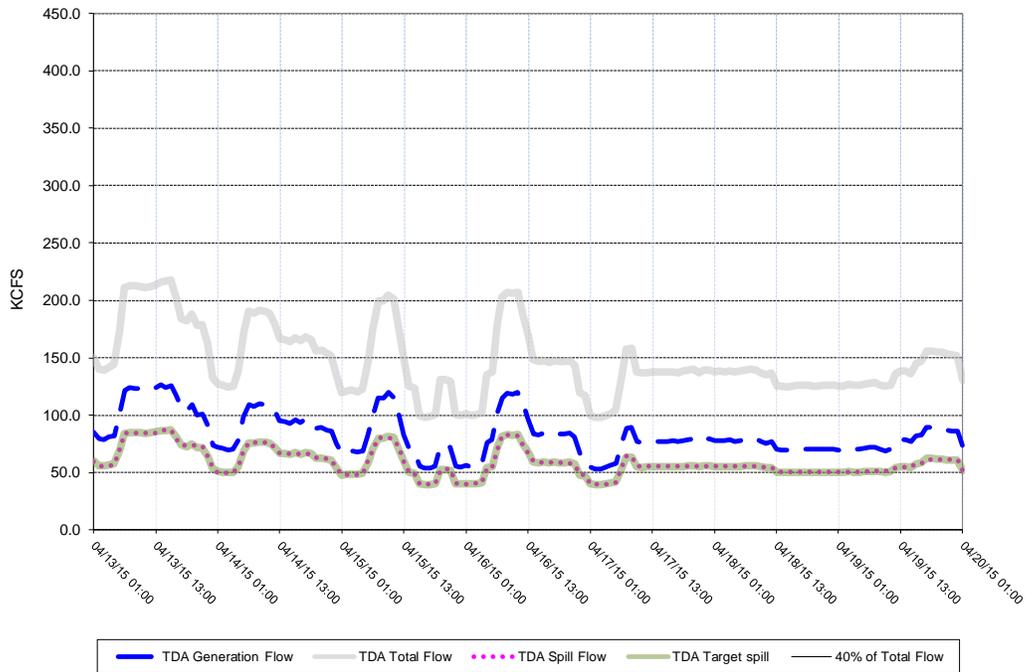


Figure 20

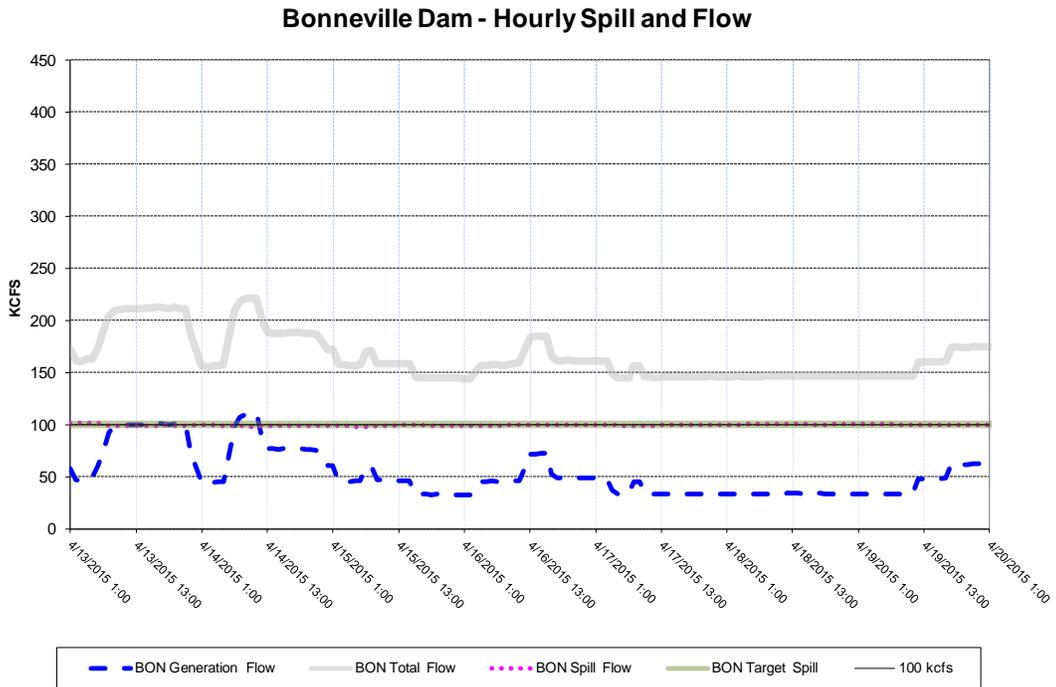
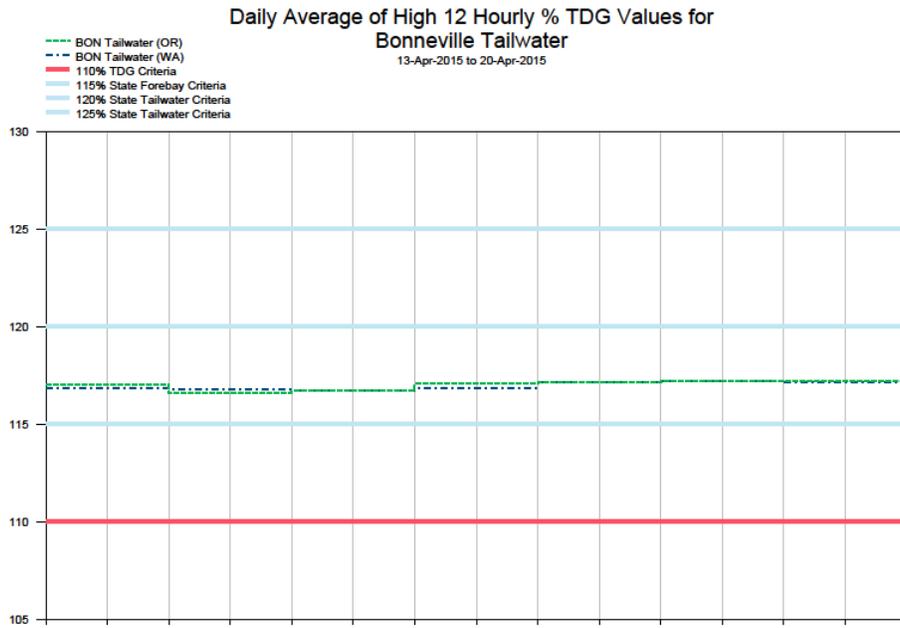
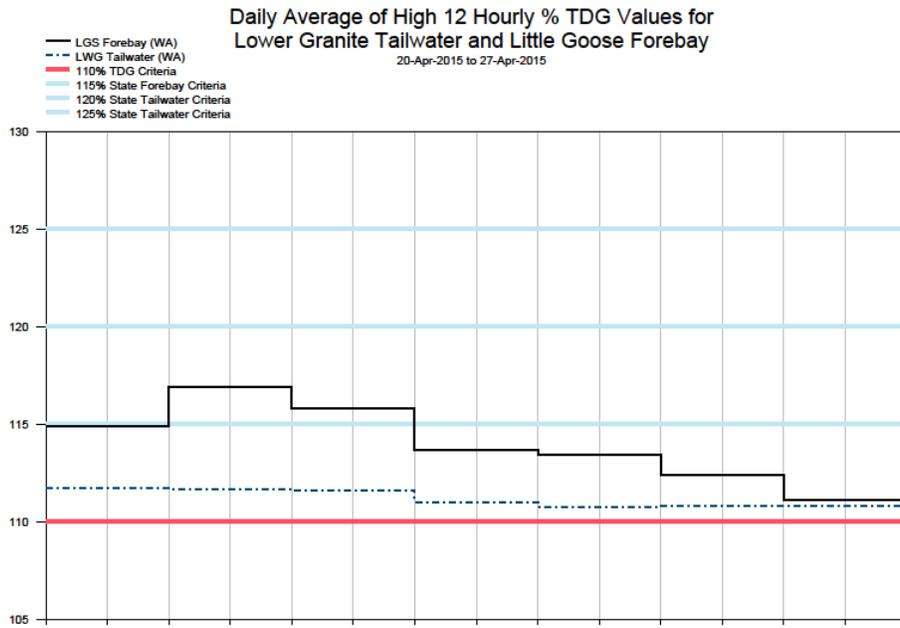


Figure 21



Lower Granite Dam - Hourly Spill and Flow

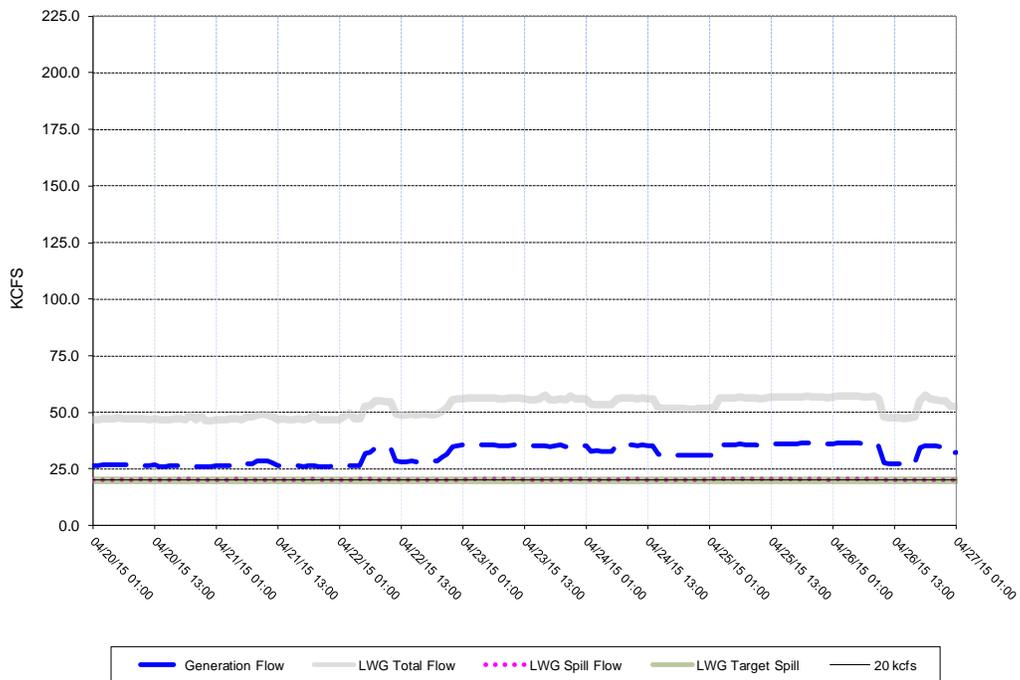
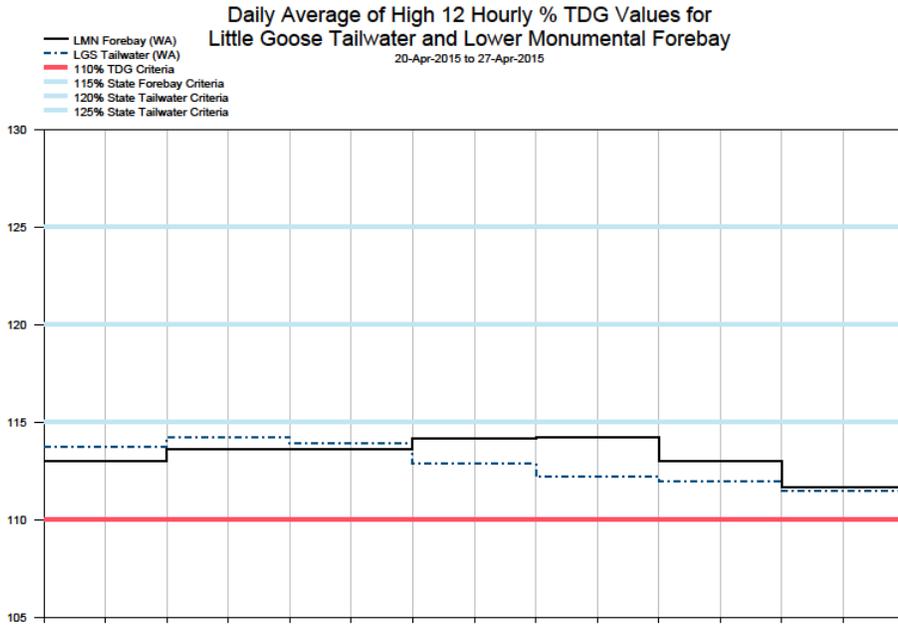


Figure 22



Little Goose Dam - Hourly Spill and Flow

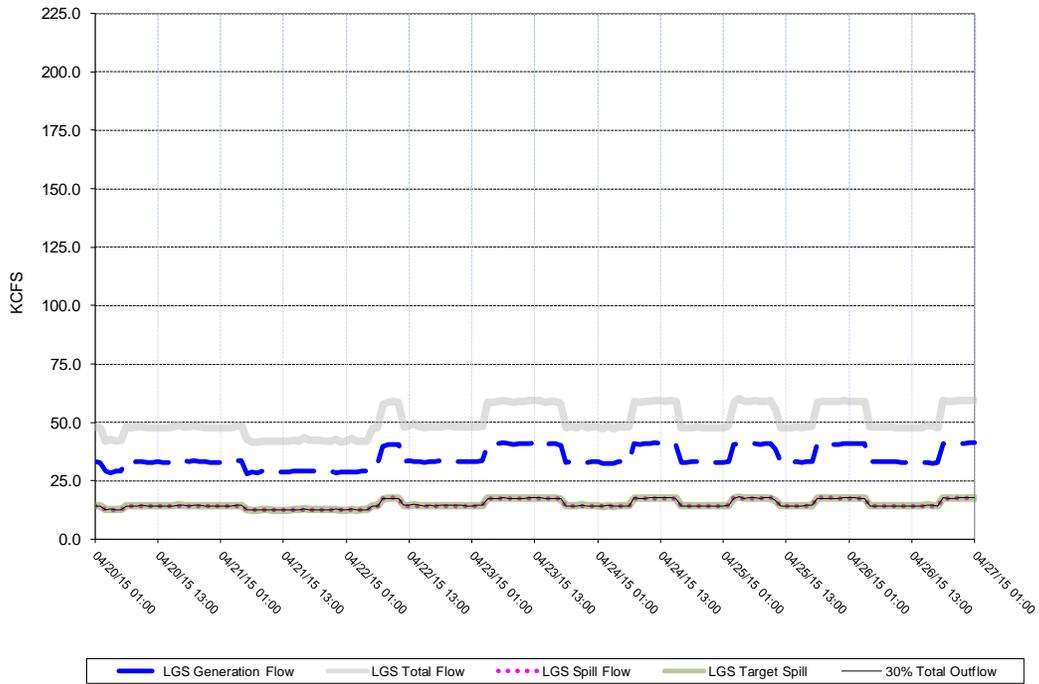


Figure 23

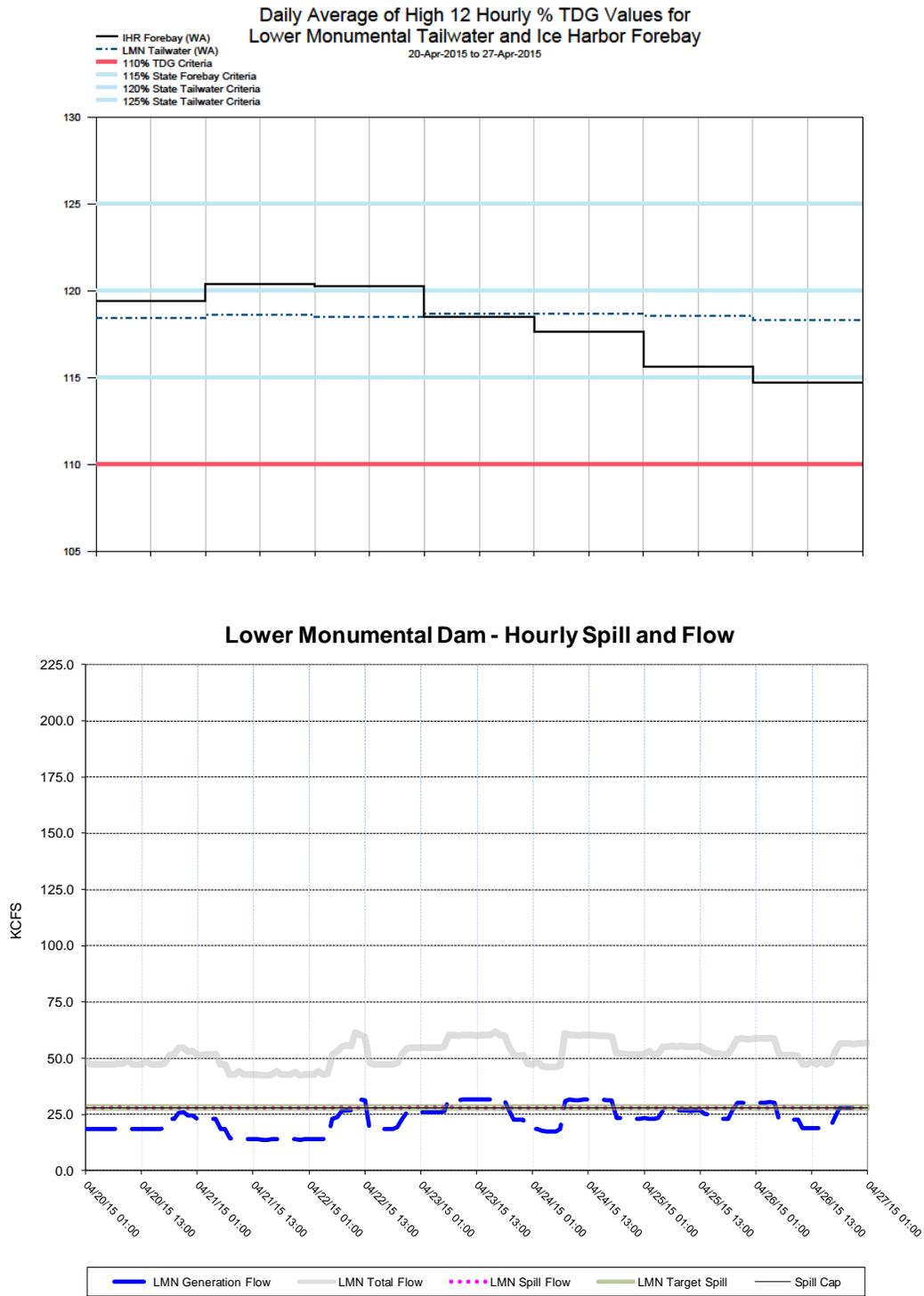


Figure 24

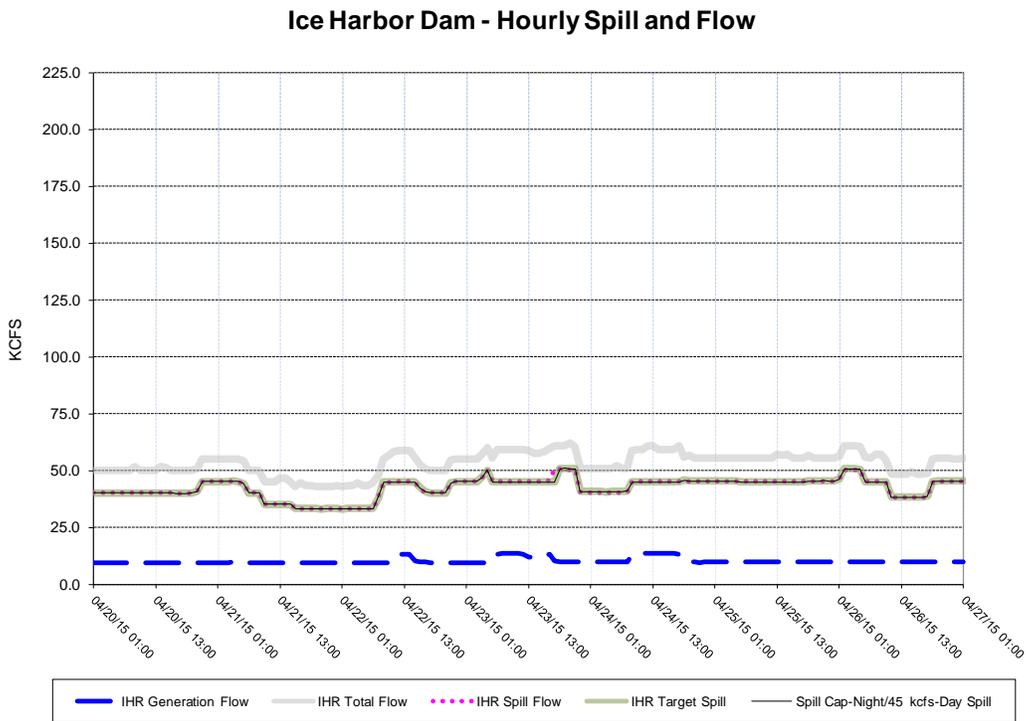
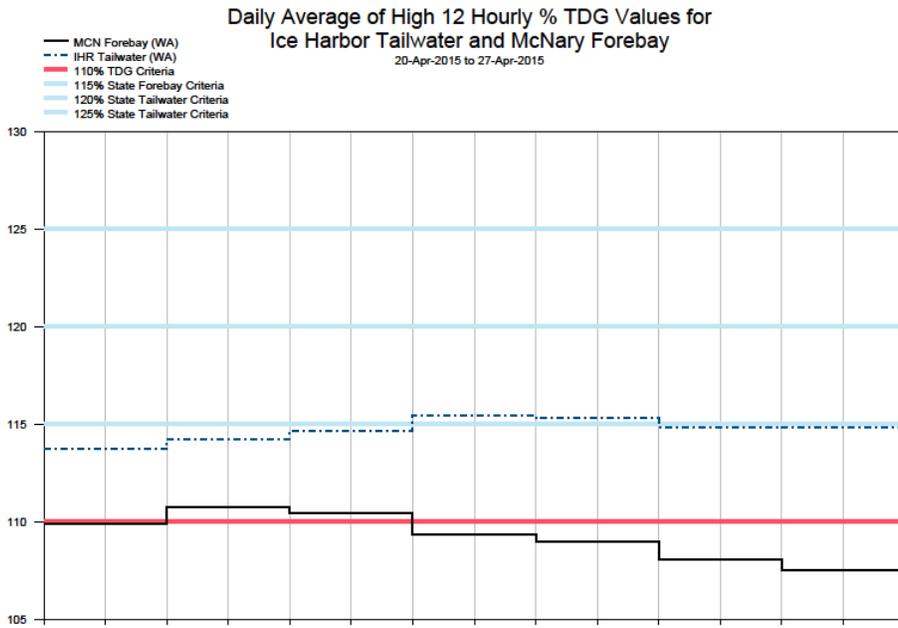
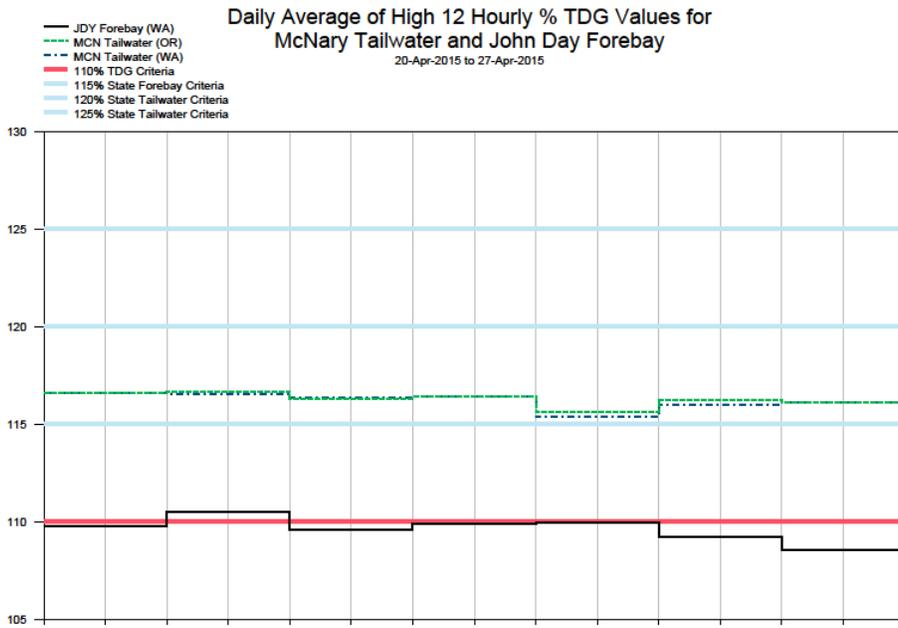


Figure 25



McNary Dam - Hourly Spill and Flow

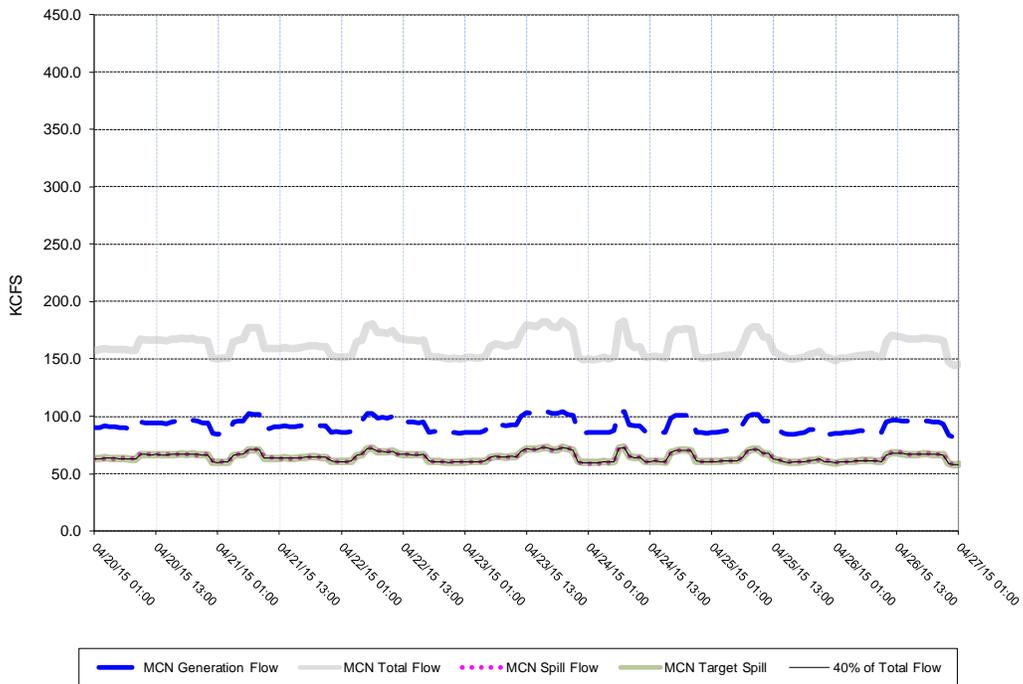
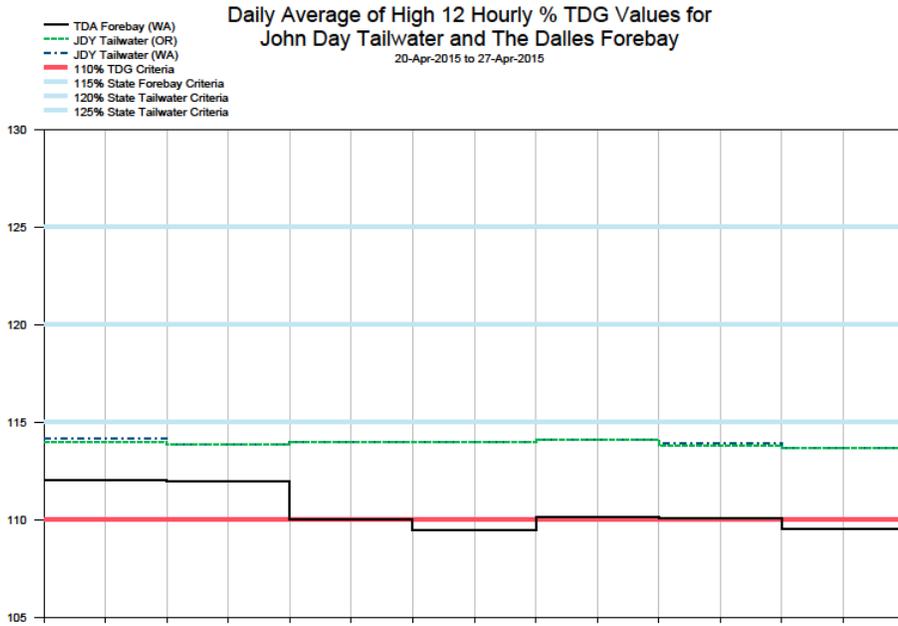


Figure 26



John Day Dam - Hourly Spill and Flow

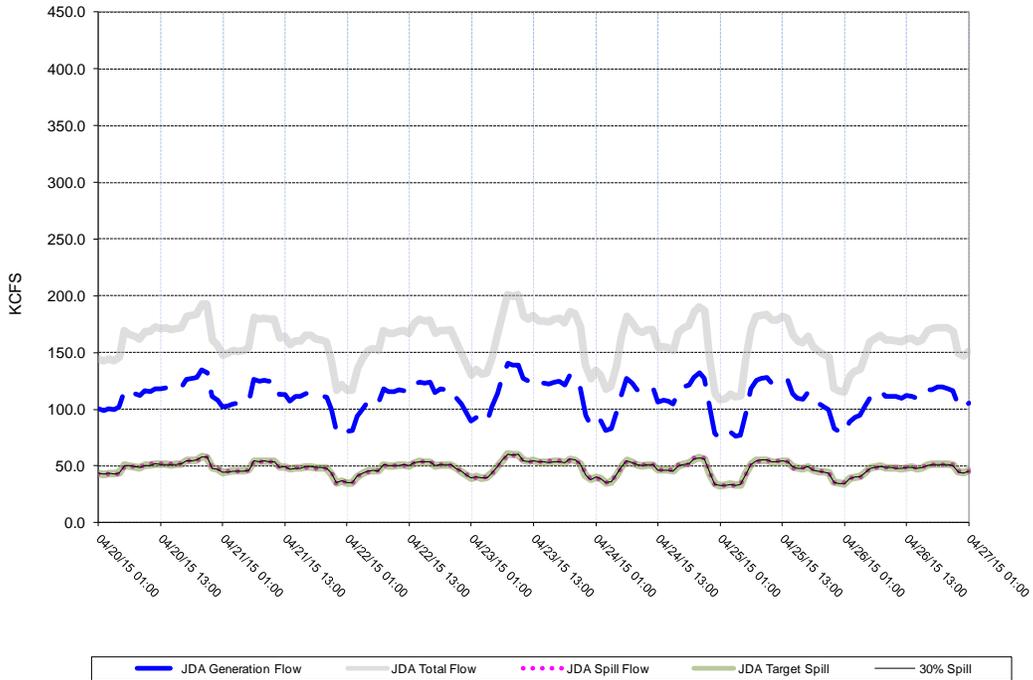
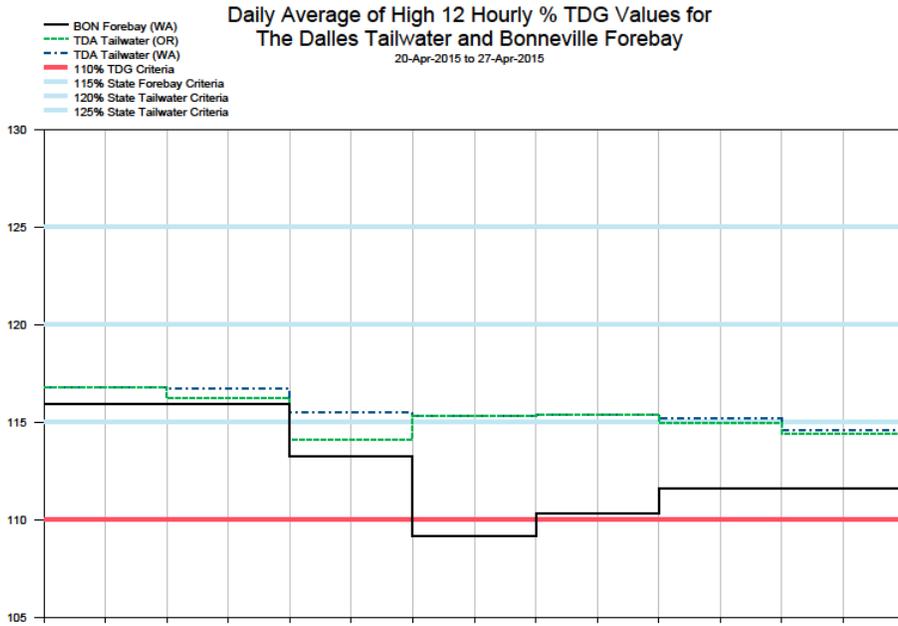


Figure 27



The Dalles Dam - Hourly Spill and Flow

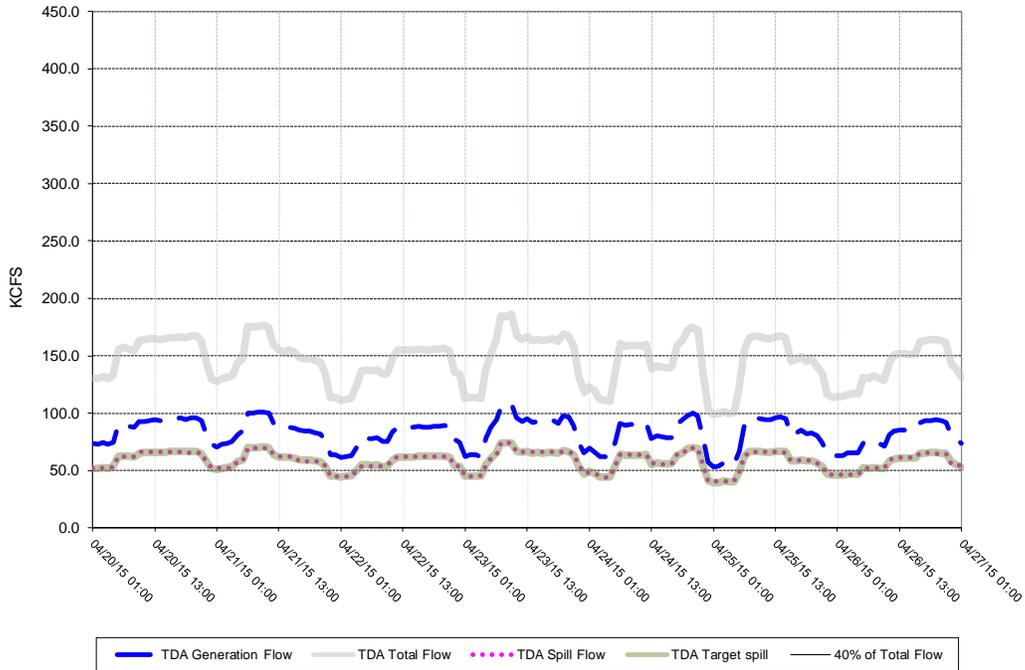


Figure 28

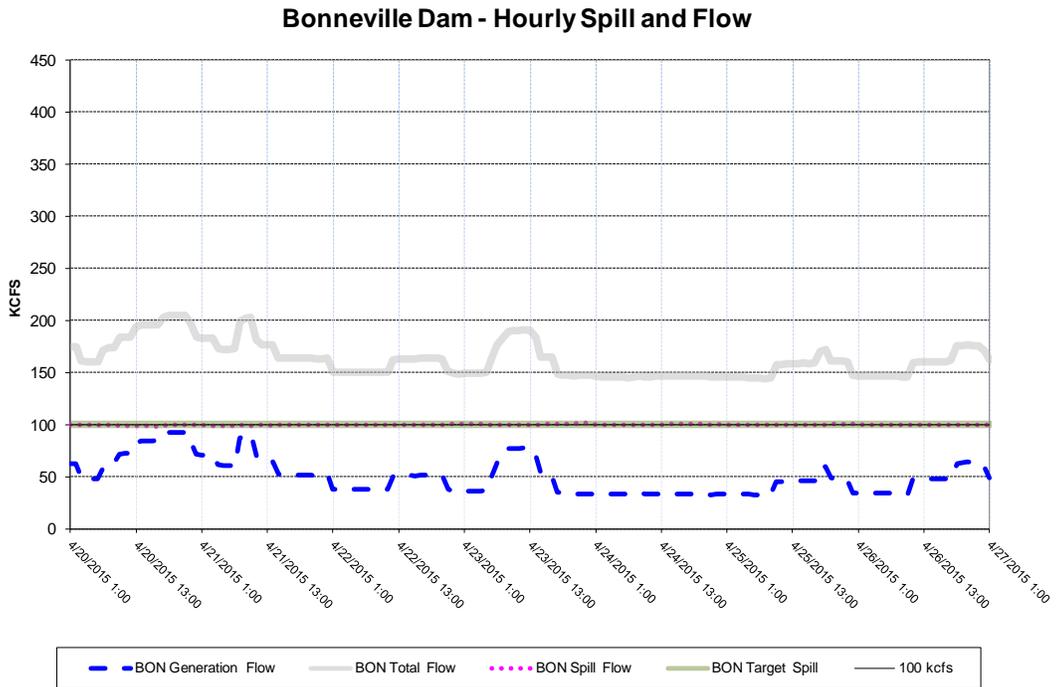
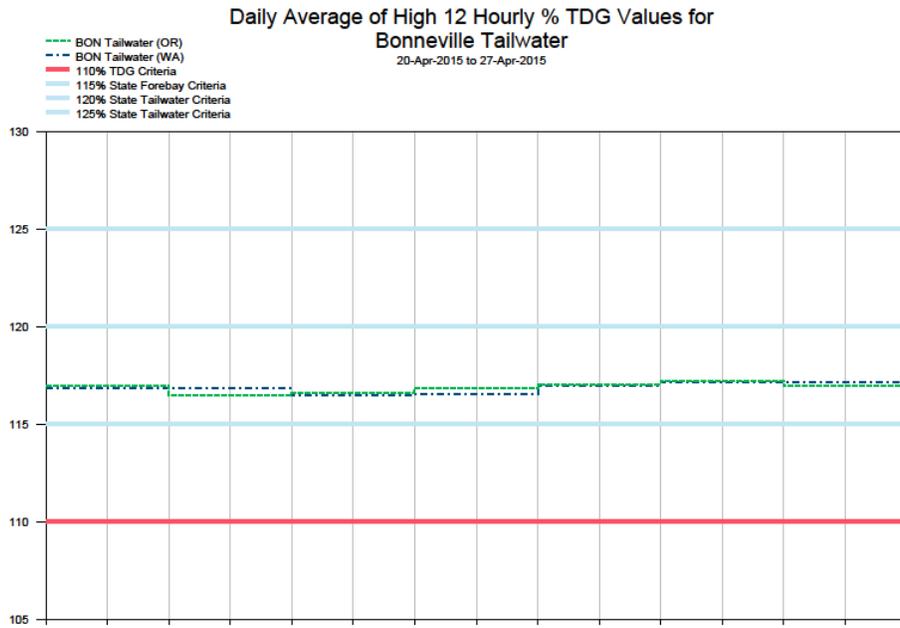


Table 1
Average Percent TDG Values For April 1 – April 26

Date	FIXED MONITORING STATIONS																			
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	IDSW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW	
	WA	WA	WA	WA	WA	WA	WA	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120
4/1/2015	102.5	102.1	102	101.3	101.9	101.5	102	106.6	105.9	111.5	111.5	104.8	108.3	109.5	104.5	105	107.1	104.4	110.3	110.2
4/2/2015	102.1	101.6	101.7	103.1	101.4	101.1	101.5	107.6	104.7	116.5	116.5	104.1	114.3	114.3	103.9	108.1	108.1	105.2	110.6	110.7
4/3/2015	100.9	110.1	102.2	108.8	101.3	117.1	101.4	115.1	104.4	113.2	116.2	104.7	112.6	114.3	106.6	108.4	108.4	105	111	110.8
4/4/2015	101.6	110.4	102.5	109.1	101.8	119.2	101.7	115.4	106.6	113.4	113.4	105	104.1	104.7	106.4	105.9	107.5	108.8	112.7	112.5
4/5/2015	103.2	110.7	103.2	109.9	105.1	126.9	107.2	115.1	107.5	113.7	113.7	106	104.9	104.9	105.3	105.6	105.5	108.8	112.9	112.9
4/6/2015	103.4	111	103.3	110	107.1	117.6	111.3	114.6	107.5	113.7	113.7	106	105.1	105.1	105.2	105.3	105.4	106.9	111.8	112.2
4/7/2015	103.1	111	105.8	111.1	107.9	118	113.9	114.7	107.3	111.4	112.1	108.9	108.2	108.2	106.4	106.4	106.4	105.6	111.4	111.8
4/8/2015	103.2	111	107.6	111.3	108	117.7	114	114	106.8	110.6	111.2	108.9	107.4	108.4	106.7	106.7	106.7	105.3	110.8	111.2
4/9/2015	101.7	111.3	107.8	111.4	107.7	118.1	113.4	114.1	106.6	109.2	109.8	107.5	107.2	107.2	106.7	106.8	106.8	106.1	111.9	111.9
4/10/2015	102.9	111.3	109.3	111.8	109.1	118.8	115.3	113.6	107.9	114.9	114.8	108.1	114.5	114.5	107.7	113.9	113.9	107.4	116.7	116.7
4/11/2015	103	111.4	109.5	111.8	109.9	119	115.7	112.6	107.9	114.1	114.9	108.1	113.5	113.5	108.6	114.2	114.2	107.4	116.4	116.6
4/12/2015	102.3	111.3	108.7	111.6	109.7	118.5	114.5	112.1	106.7	113.7	113.7	106.4	113.5	113.5	108.2	114.1	114.1	109.4	116.7	116.6
4/13/2015	103.1	112.1	109.8	112.2	110	119	113.8	112.4	106.2	114.4	114.5	107.3	113	113.4	110.3	115.6	115.6	111.9	117.2	117
4/14/2015	103.1	112.3	109.8	112.1	110	118.3	113.8	112.7	106.1	113	113.3	107.1	112.6	112.6	109.8	113.4	115	111.9	116.8	117
4/15/2015	101.2	111.1	107	110.9	107.8	118.5	111.2	113.5	103.7	114.2	113.9	104.4	111.8	111.9	106.5	112.7	112.7	108.6	117	117
4/16/2015	101	111.4	106.3	111.2	108.2	118.6	112.4	113	105	114.4	114.4	104.7	112.7	112.7	109.3	114.9	114.9	110.3	117.2	117
4/17/2015	102.5	111.9	107.2	111.9	108.9	119.3	113.6	113.4	106.3	115.3	115.3	105.6	113.5	113.5	110.1	115.6	115.6	112.5	117.4	117.3
4/18/2015	102.5	111.3	107.3	112	109.2	119.2	115.5	113.3	108.3	116.2	116.2	106.6	112.7	113.4	109.9	114.9	115.3	113.9	117.4	117.4
4/19/2015	103.2	111.7	111.3	112.8	112	118.9	118.3	113.7	109.1	116.5	116.5	107.9	114.1	114.1	111.4	116.2	116.2	114.5	117.3	117.3
4/20/2015	106.2	111.7	114.9	113.7	113	118.4	119.4	113.7	110	116.6	116.6	109.9	113.9	114.1	112	116.8	116.8	115.9	117.2	117
4/21/2015	106.1	111.6	116.9	114.2	113.6	118.6	120.4	114.2	110.7	116.7	116.5	110.5	113.9	113.8	111.9	116.2	116.6	115.9	116.7	117
4/22/2015	105.3	111.5	115.4	113.7	113.6	118.4	120.2	114.6	110.4	116.3	116.3	109.5	114	114	109.7	114.1	115.2	112.9	116.9	116.7
4/23/2015	103.7	110.9	113.6	112.8	114.2	118.7	118.4	115.4	109.3	116.4	116.4	109.9	114	113.9	109.5	115.3	115.3	109.1	117.1	116.8
4/24/2015	103.6	110.8	113.4	112.2	114.2	118.7	117.5	115.1	108.9	115.7	115.4	109.9	114.1	114.1	110.1	115.4	115.4	110.4	117.2	117.2
4/25/2015	102.6	110.8	112.4	111.9	112.9	118.5	115.6	114.8	108	116.2	116	109.2	113.8	113.8	110	114.9	115.1	111.6	117.5	117.4
4/26/2015	101.7	110.8	111.1	111.4	111.6	118.2	114.6	114.8	107.5	116.1	116.1	108.4	113.6	113.6	109.5	114.4	114.4	111.6	117.1	117.3

Total Dissolved Gas Monitoring Stations

Code	Station Name
LWG	Lower Granite Forebay
LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay
LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay
LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay
IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay
MCPW	McNary Tailwater
JDY	John Day Forebay
JHAW	John Day Tailwater
TDA	The Dalles Forebay
TDDO	The Dalles Tailwater
BON	Bonneville Forebay
CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal

FISH OPERATIONS PLAN IMPLEMENTATION REPORT

May 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' May 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in May 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in May displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

¹ Averages reported are consistent with the current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and the Washington TDG criteria adjustments have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented from Monday through Sunday.

The weekly figures begin on April 27 and end on May 31 for the following lower Snake River and lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on April 27 for the lower Snake River and the lower Columbia River projects.

April 27 – May 3	Figures 1 – 8
May 4 – May 10	Figures 9 – 16
May 11 – May 17	Figures 17 – 24
May 18 – May 24	Figures 25 – 32
May 25 – May 31	Figures 33 – 40

A. Upper Figure: Displays the daily average %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the observed percent TDG in the tailwater of the dam using the Oregon 120 %TDG standard calculated with the high 12-hour average.¹ Applies only to figures which include the lower Columbia dams.
2. The blue dot-dash line represents the observed percent TDG in the tailwater of the dam using the Washington 120 %TDG standard calculated with the high 12-hour average.¹
3. The black solid line represents the observed percent TDG in the forebay of the next dam downstream using the Washington 115 %TDG standard calculated with the high 12-hour average.¹

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

II. A table is included at the end of the figures that lists the average daily %TDG for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects, tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the May 2015 Spill Variance Table.³ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour

³ Involuntary spill conditions appear in the figures, but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

(except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams⁴, which may range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

May 2015 Operations

The month of May was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the May 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 4.2 MAF (Million Acre Feet) or 61% of average as measured at Lower Granite Dam. For the lower Columbia, the Runoff Processor indicated the May 2015 adjusted volume runoff was below the 30 year average (1981-2010): 18.3 MAF or 72% of average as measured at The Dalles. The monthly precipitation summary for May was above average at 129% on the Snake River above Ice Harbor Dam and average on the Columbia River above The Dalles Dam at 97% due to thunderstorm activity in the southern part of the Columbia Basin during the month.

⁴ As specified in the 2015 FOP (p. 14), this applies when the spill level is below 40% of total flow at The Dalles Dam.

During the May 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 20 kcfs, 24 hours/day.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day.
- Lower Monumental Dam - The hourly target spill level was the %TDG cap, 24 hours/day.
- Ice Harbor Dam - The hourly target spill level was 45 kcfs during the day and the %TDG cap at night. Starting on April 28 at 0500 hours, the hourly target spill level alternated between 30% of total project outflow, 24 hours/day vs. 45 kcfs during the day and the %TDG cap during the nighttime spill hours (1800-0500).⁵
- McNary Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- John Day Dam - The hourly target spill level alternated every two days between 40% and 30% of total project outflow, 24 hours/day. Spill level changes occurred at 2000 hours.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level was 100 kcfs, 24 hours/day.

Operational Adjustments

No Operational Adjustments to report.

⁵ As noted in the April report, spill operation treatments were rearranged at Ice Harbor to accommodate a post-construction evaluation of modifications made to spillbay 2 to improve juvenile fish passage survival. Due to this spill operation rearrangement, the hourly target spill level of 45 kcfs during the day and the %TDG cap at night continued up until May 8. Starting on May 8 at 0500 hours, the hourly target spill level alternated every two days between 30% of total project outflow, 24 hours/day vs. 45 kcfs during the day and the %TDG cap at night. Night spill hours are 1800-0500. This evaluation is described in FPP Appendix A, and the rearrangement of spill operation treatments was further coordinated through the FPOM on April 9.

May 2015 Spill Variance Table

Table 1: May 2015 (4/27 – 5/31) – FOP Implementation Report Table

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Little Goose	Reduced Spill	5/2/15	1500	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.7%.
Little Goose	Reduced Spill	5/4/15	0500	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.7%.
Lower Monumental	Reduced Spill	5/2/15	2000-2100	2	Navigation	Hourly spill decreased to 15.2 and 19.5 kcfs (below 26 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/3/15	1900-2000	2	Navigation	Hourly spill decreased to 20.1 and 21.2 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/4/15	1800-2000	3	Navigation	Hourly spill decreased to 17.5, 17.6 and 18.0 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/5/15	1900-2000	2	Navigation	Hourly spill decreased to 12.8 and 20.0 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/6/15	1700-1900	3	Navigation	Hourly spill decreased to 11.5, 21.3 and 23.1 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/8/15	1400	1	Human/Program Error	Hourly spill decreased to 21.4 kcfs (below 24 kcfs ±2 kcfs range) due to spill control software program losing contact with the spillway.
Lower Monumental	Reduced Spill	5/8/15	1800-2000	3	Navigation	Hourly spill decreased to 18.1, 18.4 and 21.5 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/9/15	1800	1	Navigation	Hourly spill decreased to 9.7 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.

⁶ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Lower Monumental	Reduced Spill	5/10/15	1800-2000	3	Navigation	Hourly spill decreased to 17.9, 18.2 and 21.0 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/11/15	1700-1900	3	Navigation	Hourly spill decreased to 16.1, 17.4 and 21.0 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/12/15	1900-2000	2	Navigation	Hourly spill decreased to 14.8 and 20.8 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/13/15	1800-1900	2	Navigation	Hourly spill decreased to 15.4 and 21.4 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/14/15	1900-2000	2	Navigation	Hourly spill decreased to 14.3 and 19.1 kcfs (below 25 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/15/15	1800-1900	2	Navigation	Hourly spill decreased to 13.8 kcfs for both hours (below 27 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/16/15	1900	1	Navigation	Hourly spill decreased to 18.4 kcfs (below 27 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/17/15	1800-1900	2	Navigation	Hourly spill decreased to 20.0 and 22.6 kcfs (below 27 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/18/15	1800-2000	3	Navigation	Hourly spill decreased to 18.6, 22.2 and 24.2 kcfs (below 27 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/19/15	1800-1900	2	Navigation	Hourly spill decreased to 19.5 and 23.1 kcfs (below 27 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/20/15	1800-1900	2	Navigation	Hourly spill decreased to 12.6 and 19.9 kcfs (below 25 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/21/15	1900-2000	2	Navigation	Hourly spill decreased to 13.1 and 20.2 kcfs (below 25 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Lower Monumental	Reduced Spill	5/22/15	1800-1900	2	Navigation	Hourly spill decreased to 13.8 and 17.7 kcfs (below 23 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/24/15	1700-1800	2	Navigation	Hourly spill decreased to 21.4 and 14.1 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/26/15	1700-1800	2	Navigation	Hourly spill decreased to 12.5 and 19.7 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/28/15	1800-1900	2	Navigation	Hourly spill decreased to 12.5 and 16.6 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	5/30/15	1800-1900	2	Navigation	Hourly spill decreased to 15.0 and 18.4 kcfs (below 24 kcfs ± 2 kcfs range). Reduced spill for safe passage of fish barge.
Ice Harbor	Reduced Spill	4/29/15	0200	1	Operational Limitation	Hourly spill of 37.4 kcfs was 2.5 kcfs below FOP minimum generation spill, while generation levels drifted above minimum range for Unit 1 (8.2-10.0 kcfs) to 10.1 kcfs. See FOP p. 3.
Ice Harbor	Reduced Spill	5/11/15	0400	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% $\pm 1\%$ range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.7%.
Ice Harbor	Reduced Spill	5/11/15	0900-1000	2	Navigation	Hourly spill decreased to 28.8 and 28.9 % (below 30.0% $\pm 1\%$ range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.7%.
Ice Harbor	Reduced Spill	5/12/15	0900	1	Operational Limitation	Hourly spill remained at 40.0 kcfs (below FOP 45 kcfs ± 2 kcfs) while generation levels drifted above minimum range for Unit 1 (8.2-10.0 kcfs) to 10.1 kcfs. See FOP p. 3.
Ice Harbor	Reduced Spill	5/20/15	2200	1	Navigation	Hourly spill decreased to 28.7 % (below 30.0% $\pm 1\%$ range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 40.7%.

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Ice Harbor	Reduced Spill	5/26/15	0100	1	Navigation	Hourly spill decreased to 28.9 % (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.8%.
McNary	Additional Spill	4/28/15	0700	1	Transmission Stability	Hourly spill increased to 43.6% (above 40.0% ±1% range) due to an unexpected transmission line outage. 24 hr avg. spill was 40.1%.
John Day	Additional Spill	5/11/15	1700	1	Transmission Stability	Hourly spill increased to 31.1% (above 30.0% ±1% range). Project on response during rapidly changing load and/or intermittent generation (see FOP p. 3-4).
John Day	Reduced Spill	5/12/15	1100-1200	2	Transmission Stability	Hourly spill decreased to 38.6 and 36.4% (below 40.0% ±1% range). FCRPS response to loss of regional generation. John Day and The Dalles were allocated more load for part of the hour to assure system reliability. 24 hr avg. spill was 39.7%.
John Day	Reduced Spill	5/16/15	0600	1	Human/Program Error	Hourly spill decreased to 38.5% (below 40.0% ±1% range). Delay in changing spill to requested 80 kcfs. 24 hr avg. spill was 39.8%.
The Dalles	Reduced Spill	5/12/15	1100	1	Transmission Stability	Hourly spill decreased to 38.5% (below 40.0% ±1% range). FCRPS response to loss of regional generation. John Day and The Dalles were allocated more load for part of the hour to assure system reliability. 24 hr avg. spill was 40.1%.
The Dalles	Additional Spill	5/14/15	2300	1	Transmission stability	Hourly spill increased to 41.2% (above 40.0% ±1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24 hr avg. spill was 40.0%.
The Dalles	Additional Spill	5/22/15	2100	1	Transmission stability	Hourly spill increased to 41.1% (above 40.0% ±1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24 hr avg. spill was 39.9%.

Figure 1

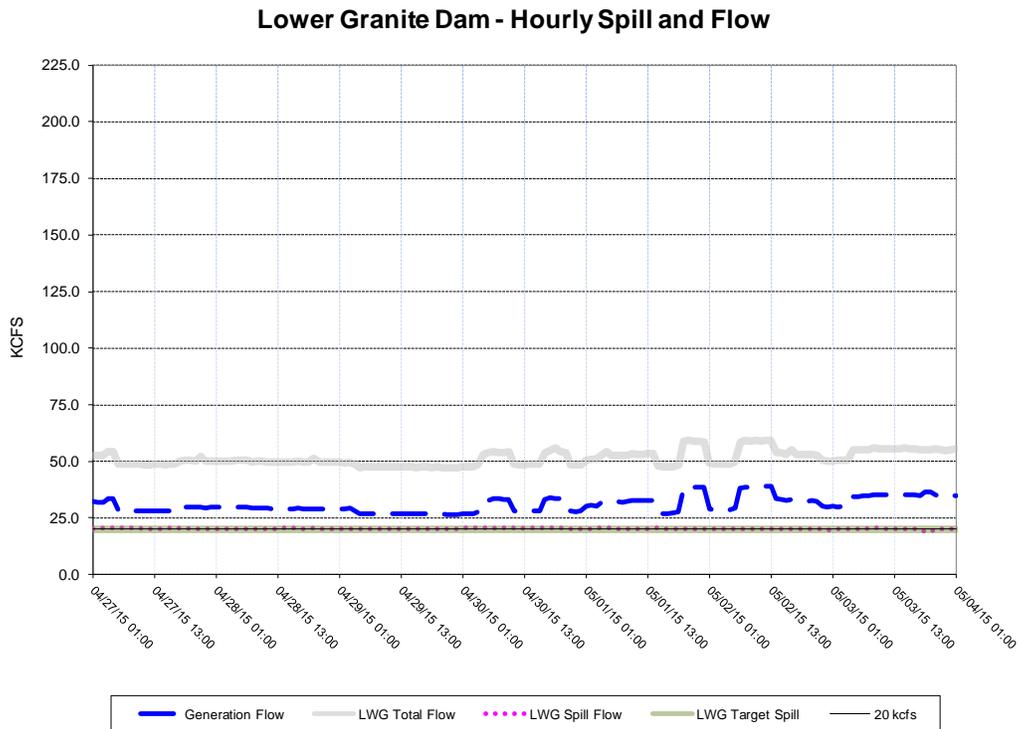
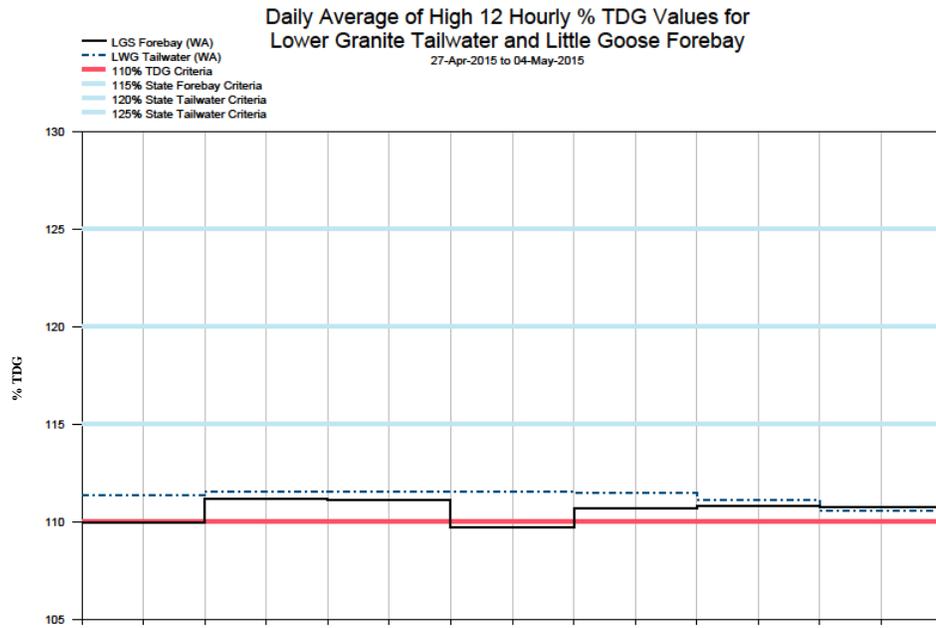


Figure 2

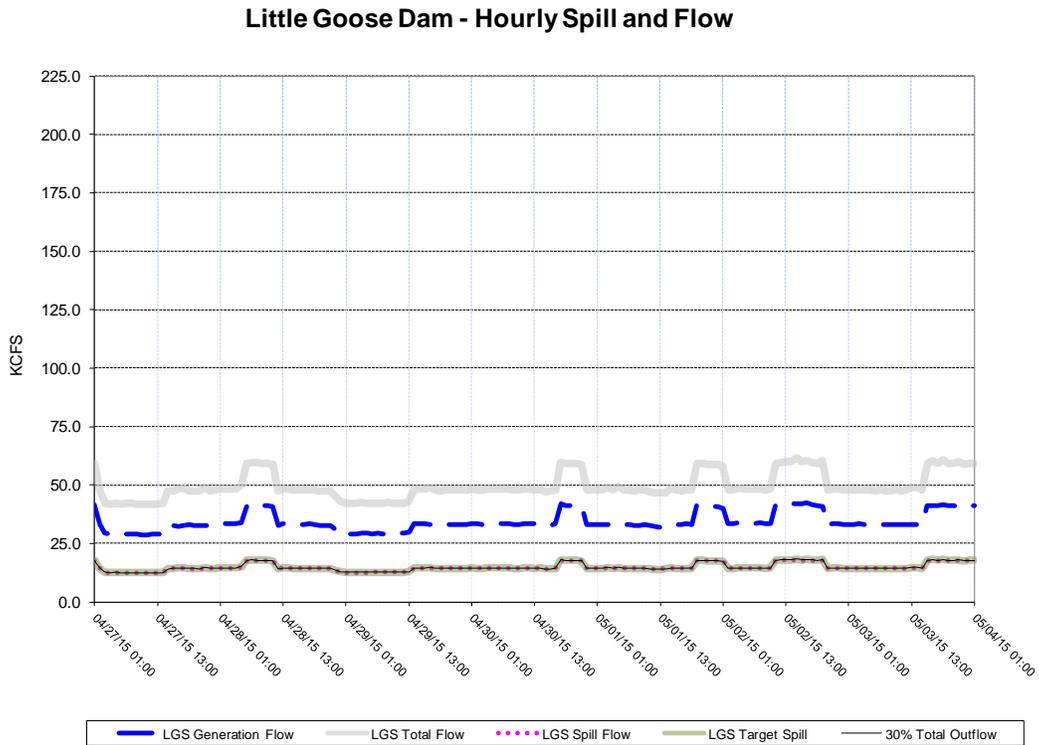
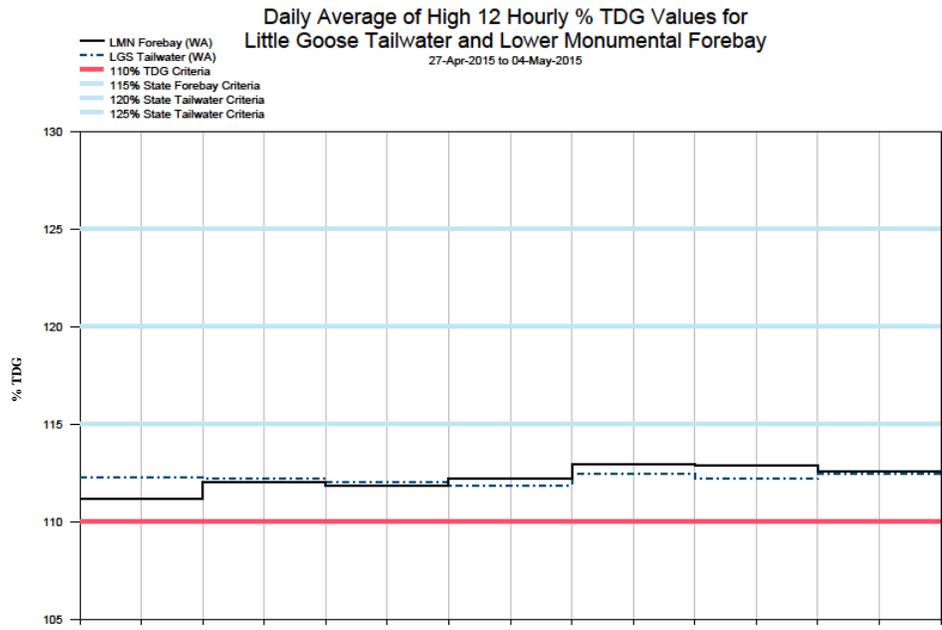


Figure 3

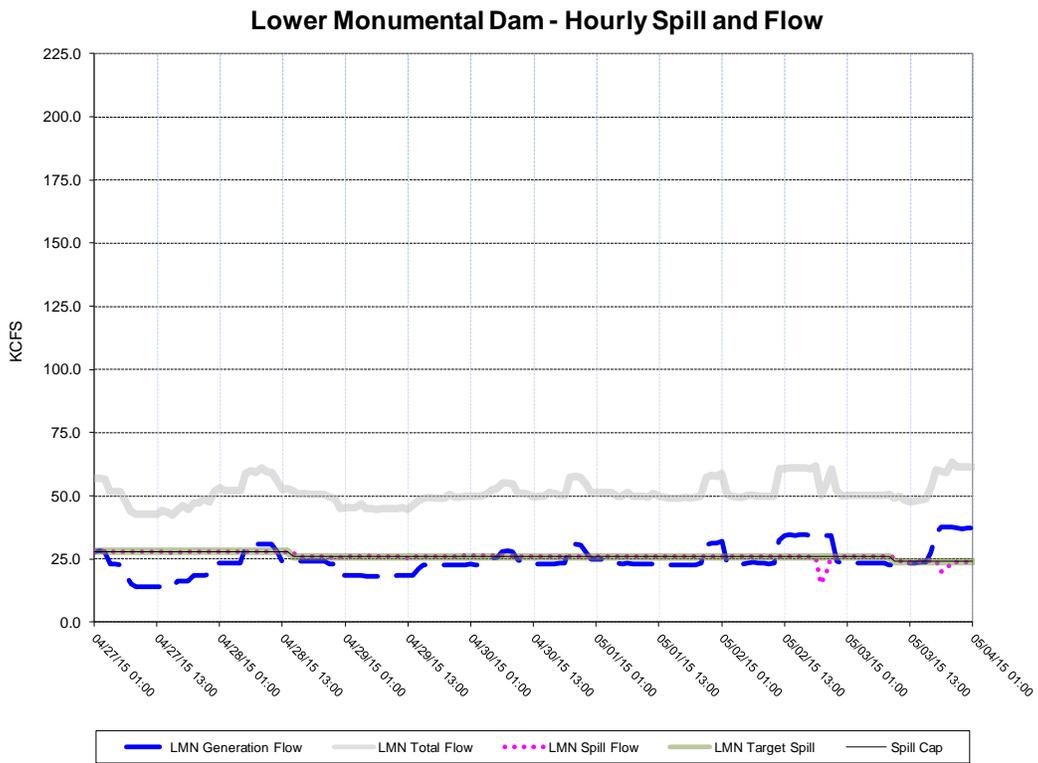
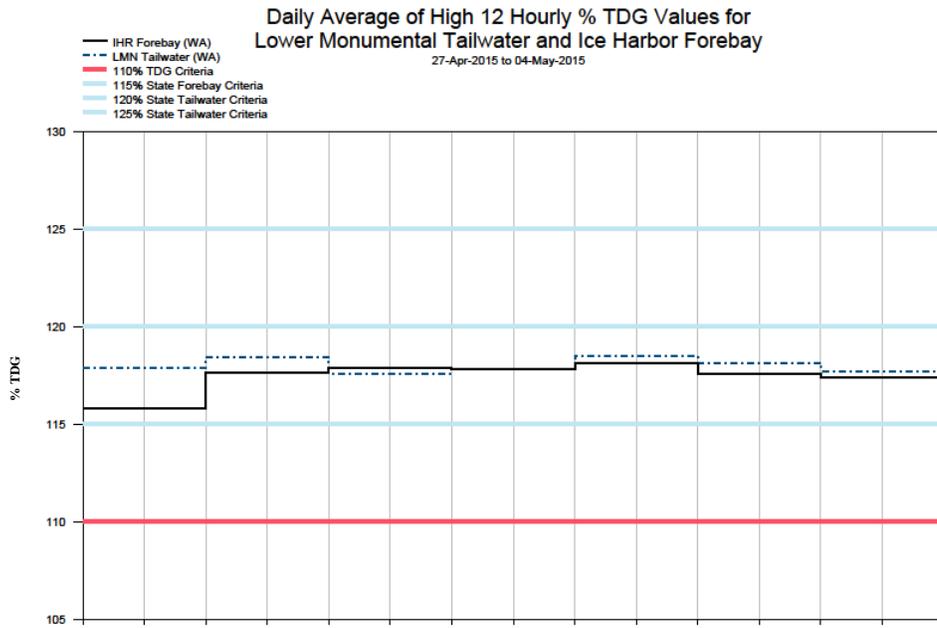


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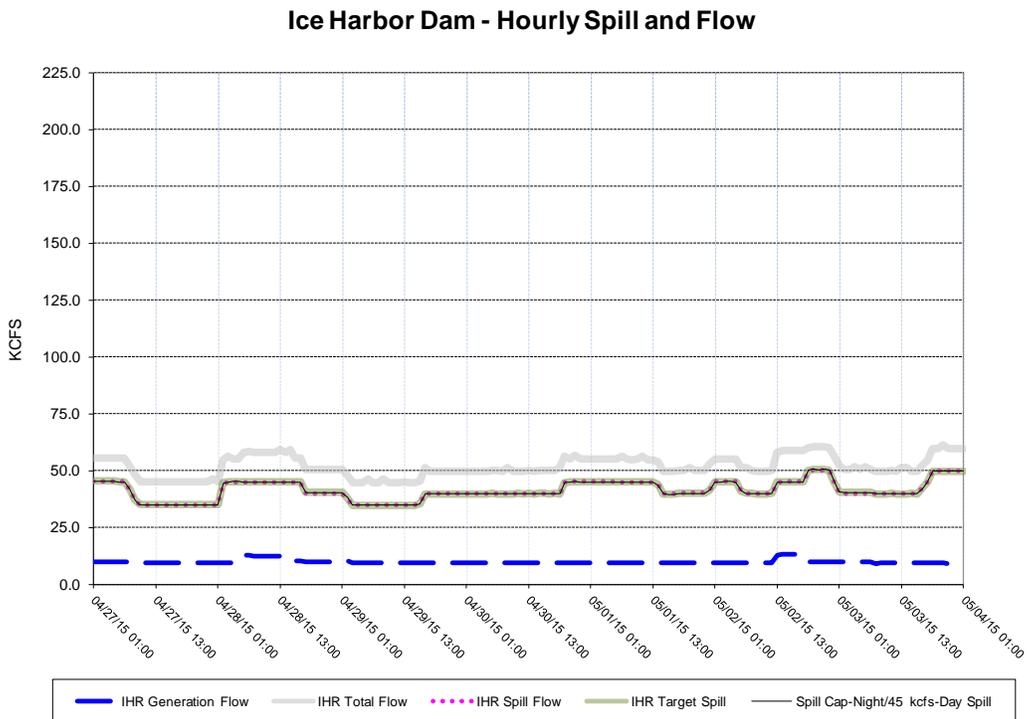
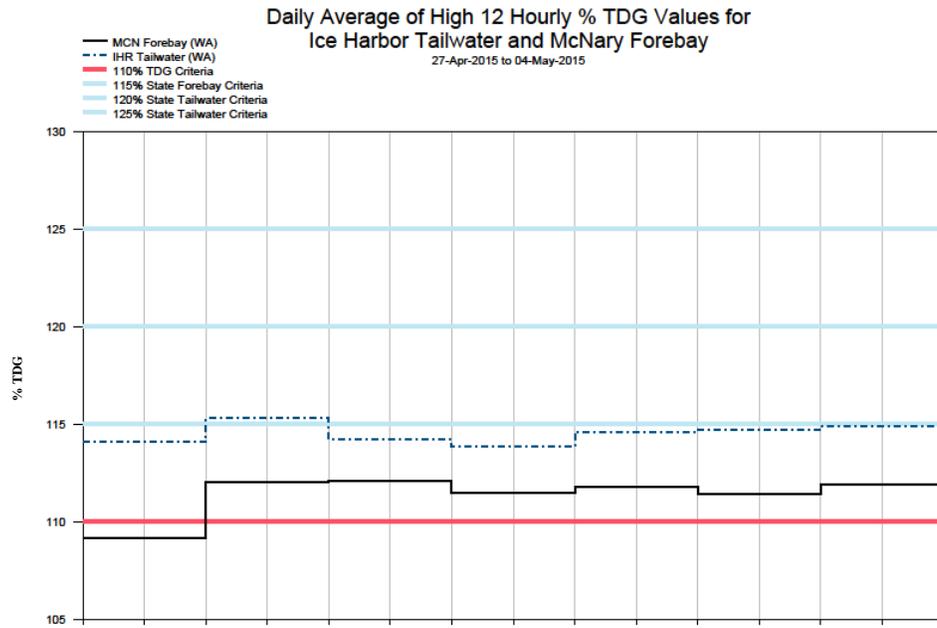
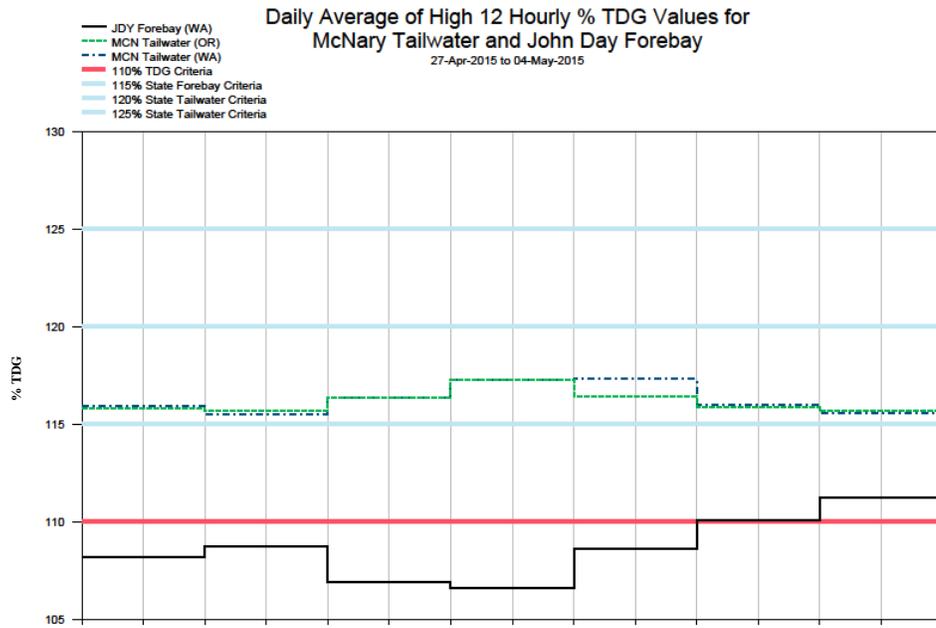


Figure 5



McNary Dam - Hourly Spill and Flow

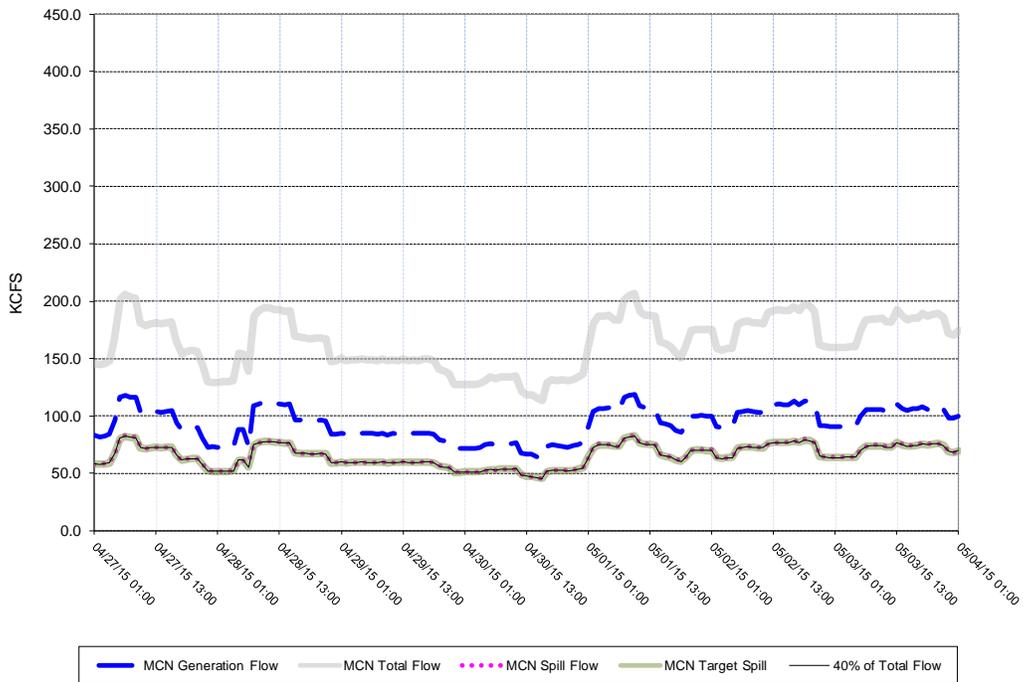
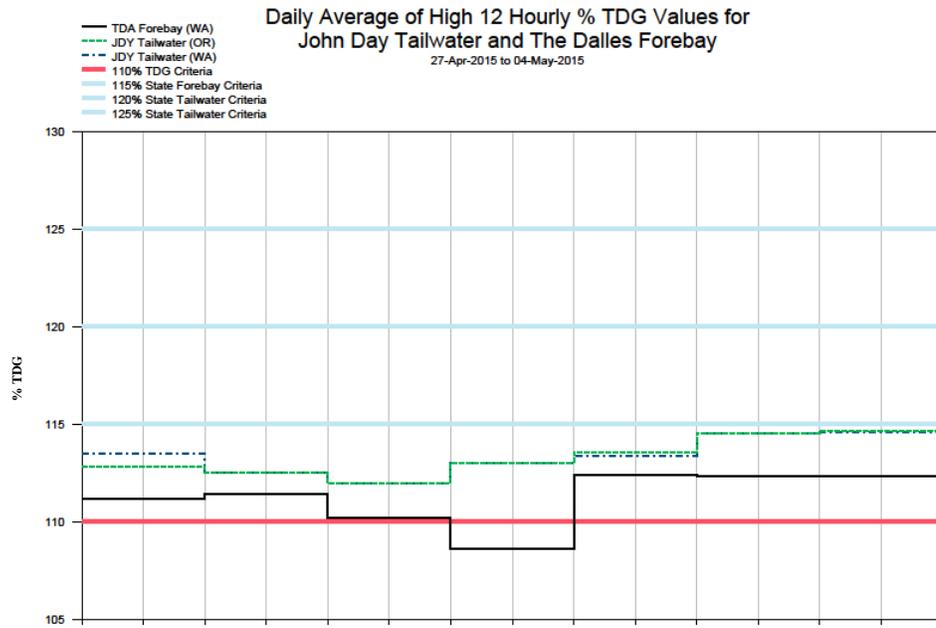


Figure 6



John Day Dam - Hourly Spill and Flow

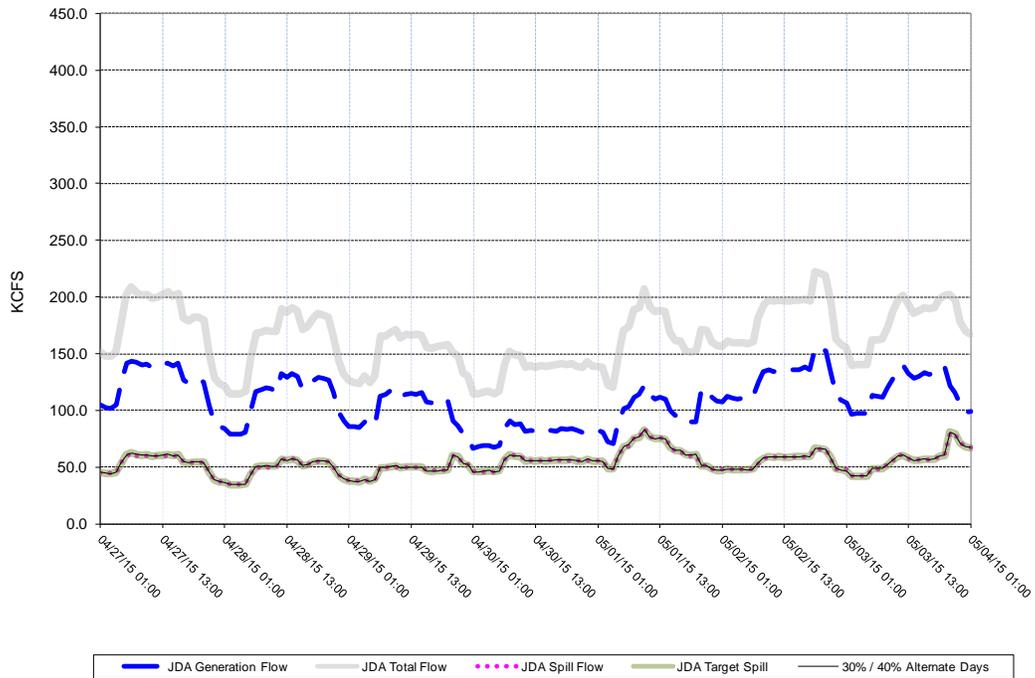
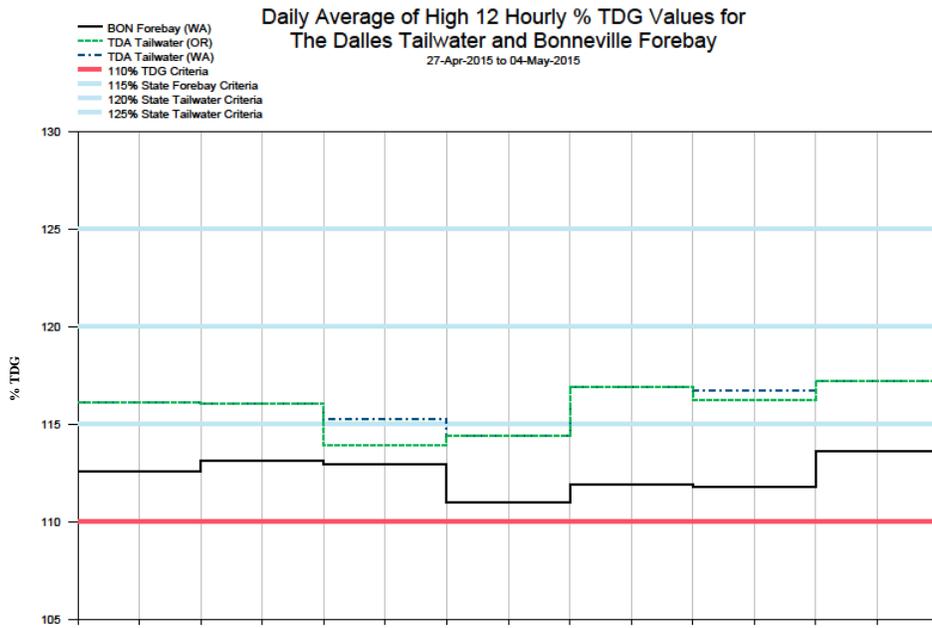


Figure 7



The Dalles Dam - Hourly Spill and Flow

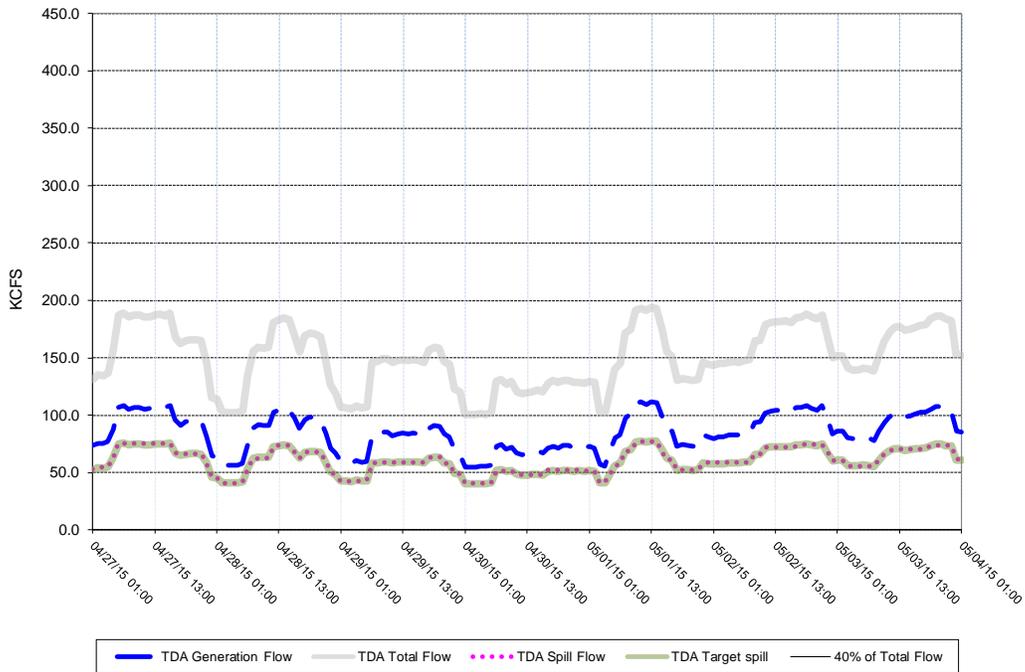


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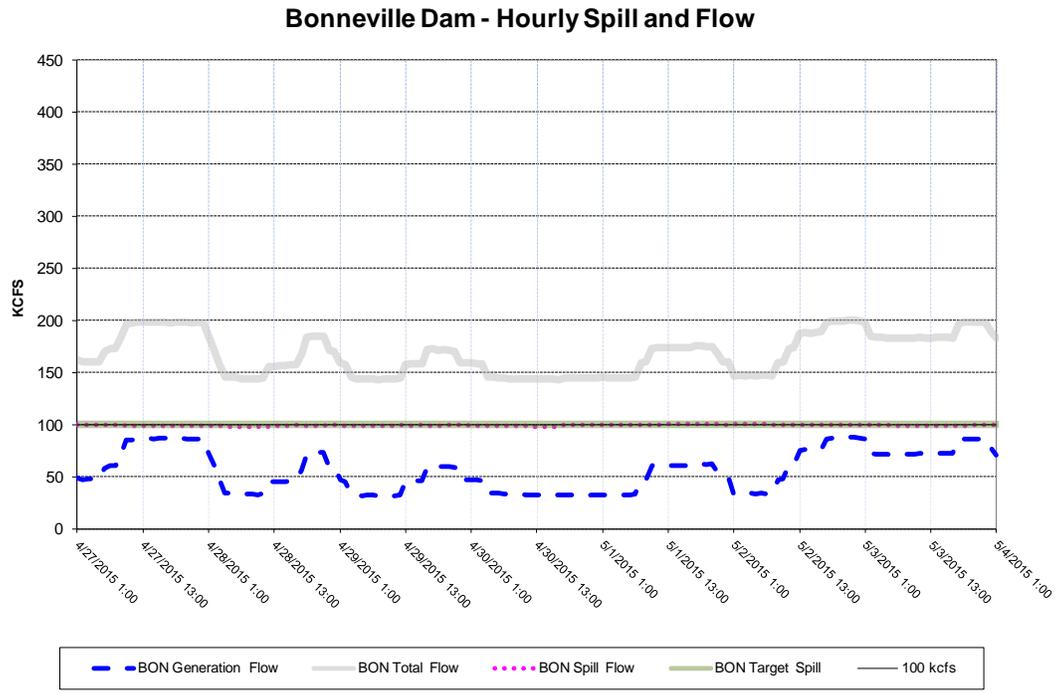
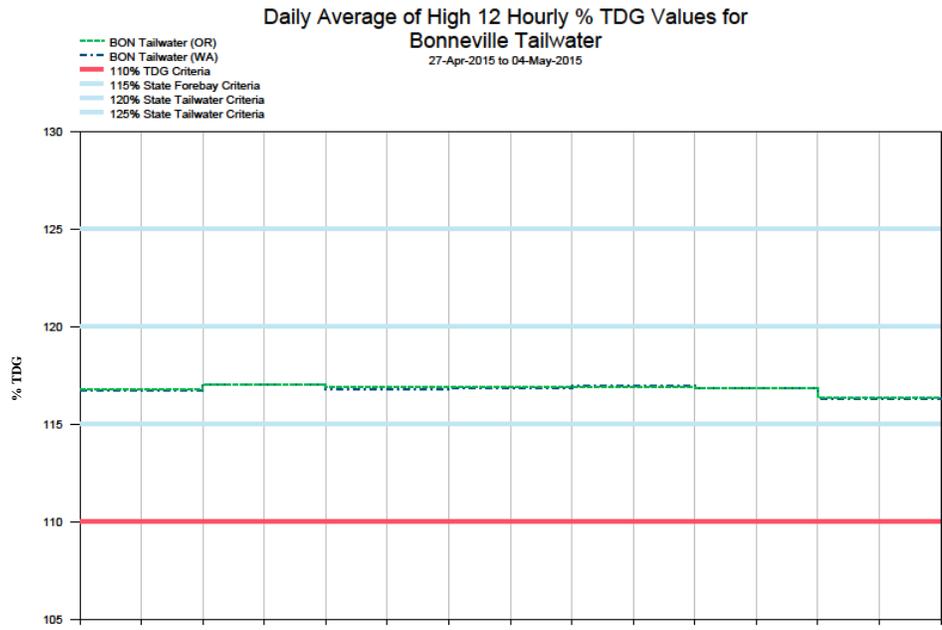


Figure 9

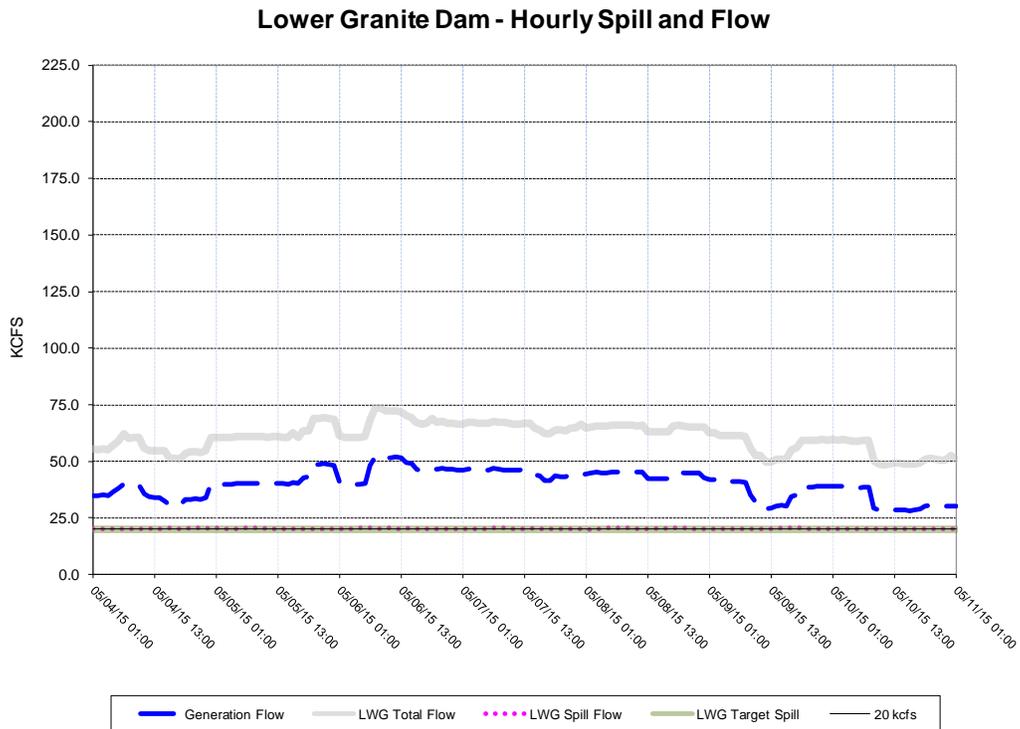
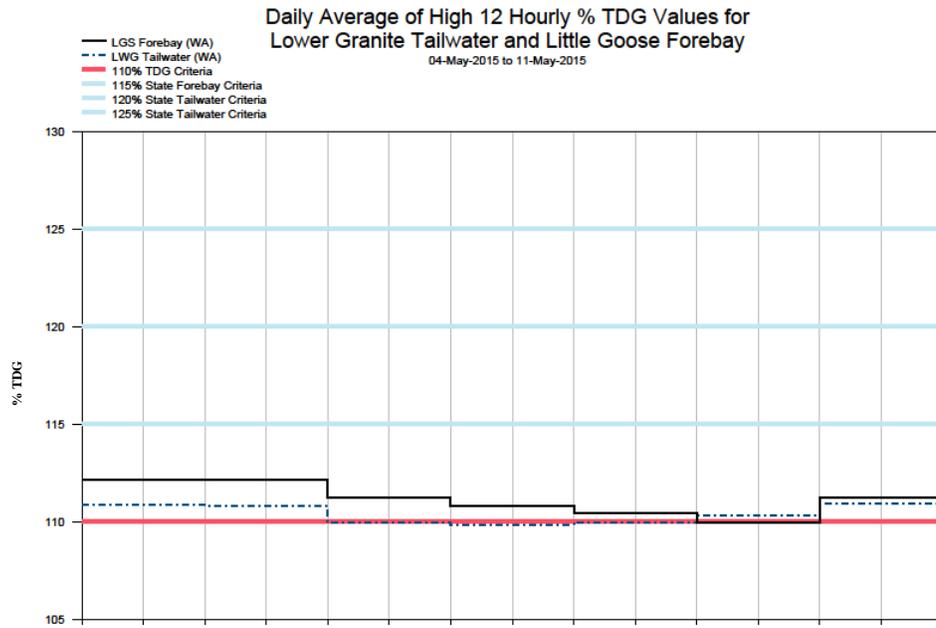
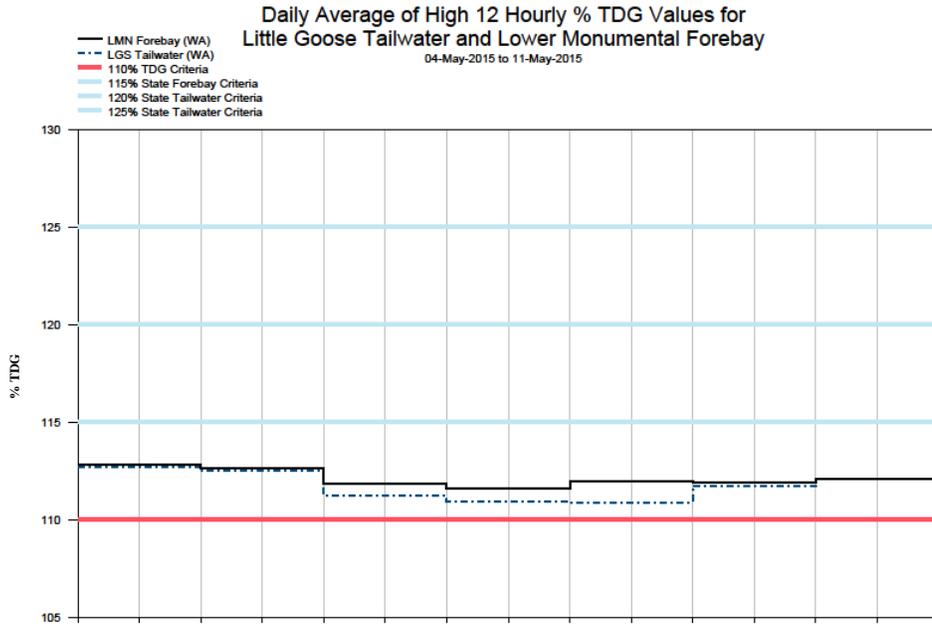


Figure 10



Little Goose Dam - Hourly Spill and Flow

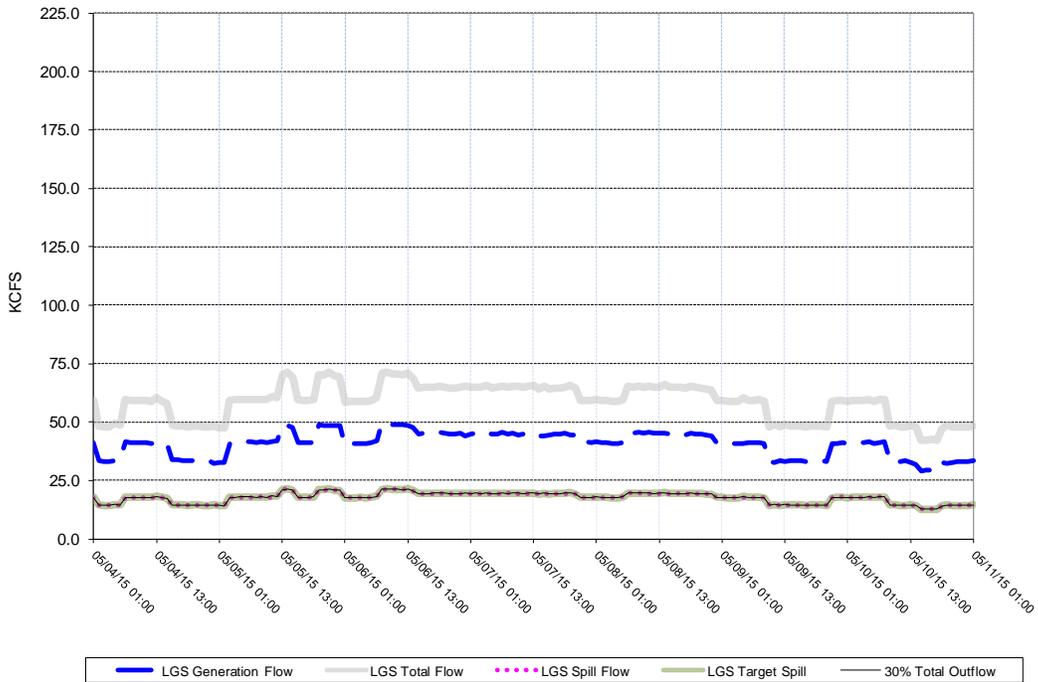


Figure 11

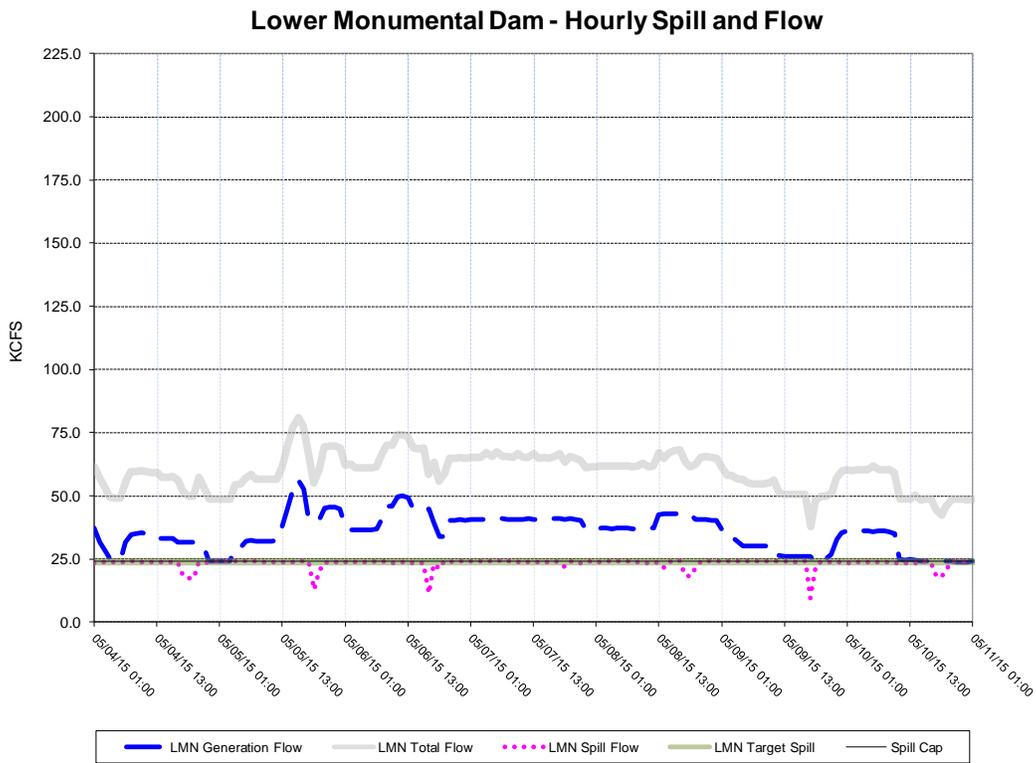
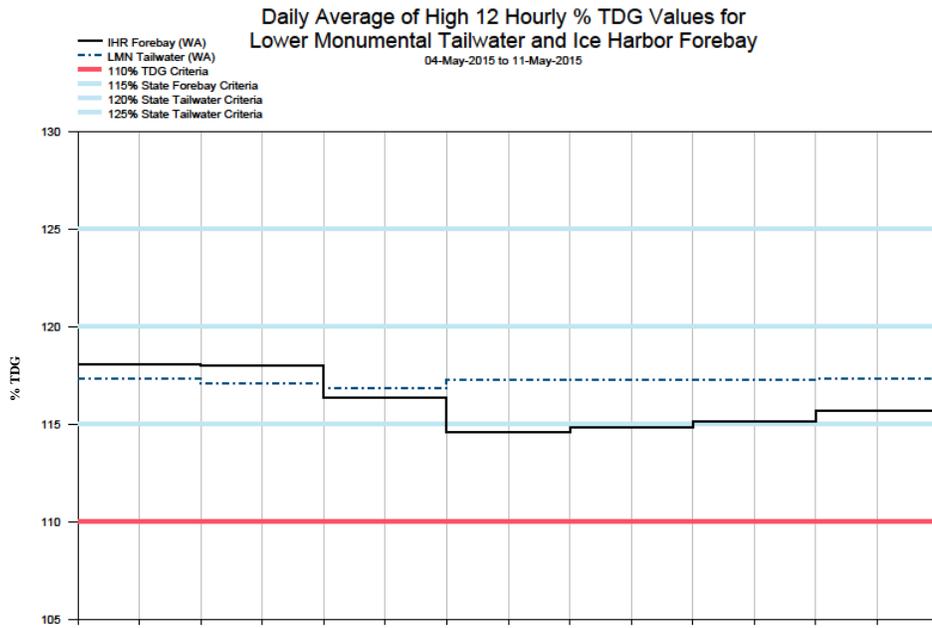


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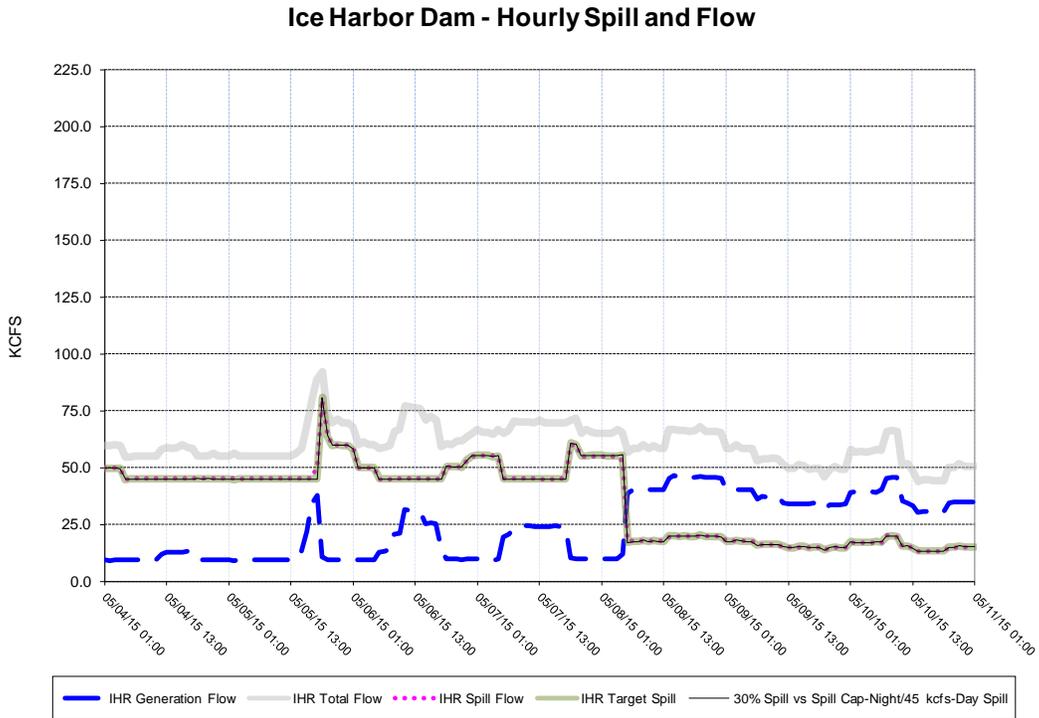
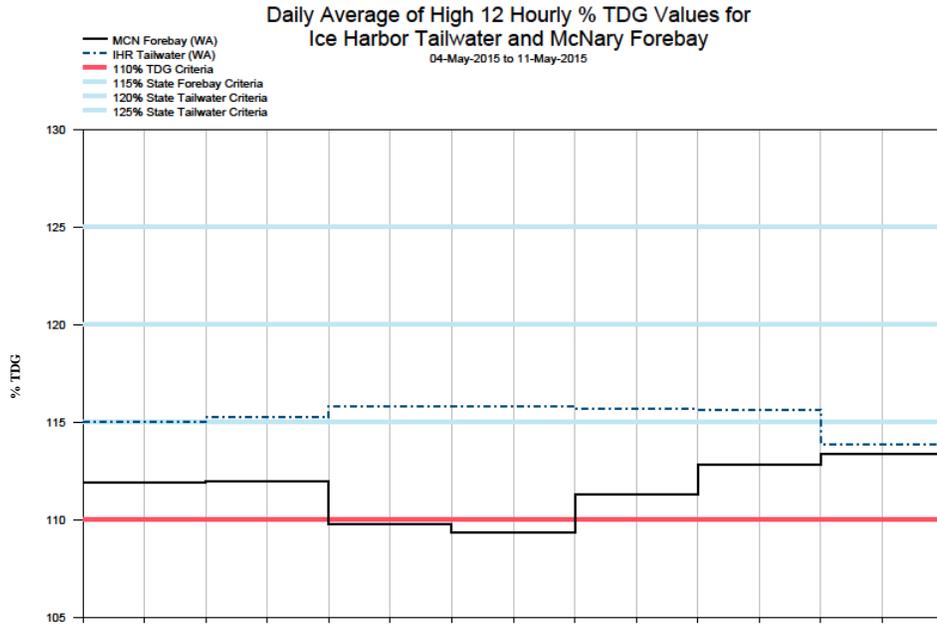
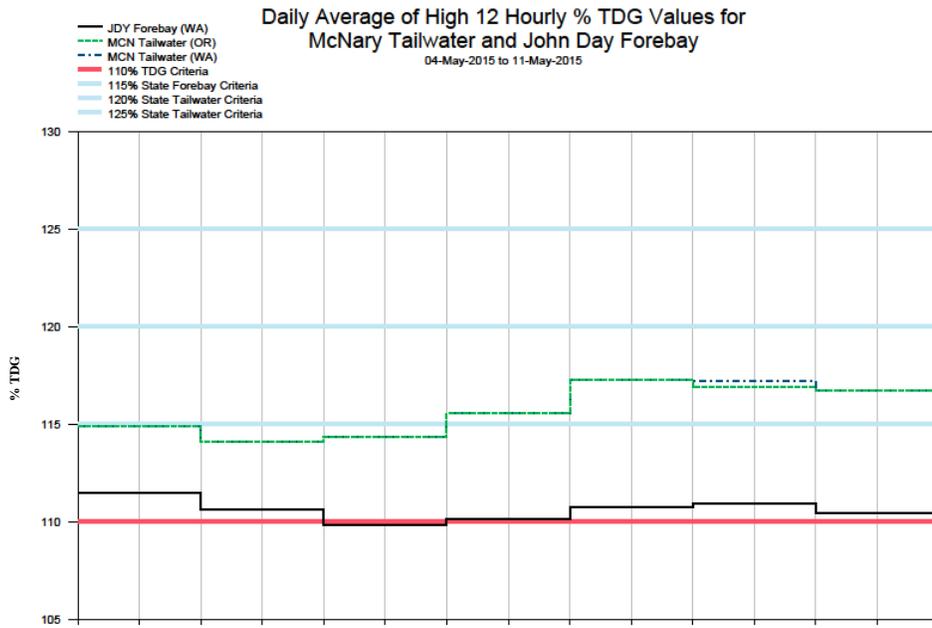


Figure 13



McNary Dam - Hourly Spill and Flow

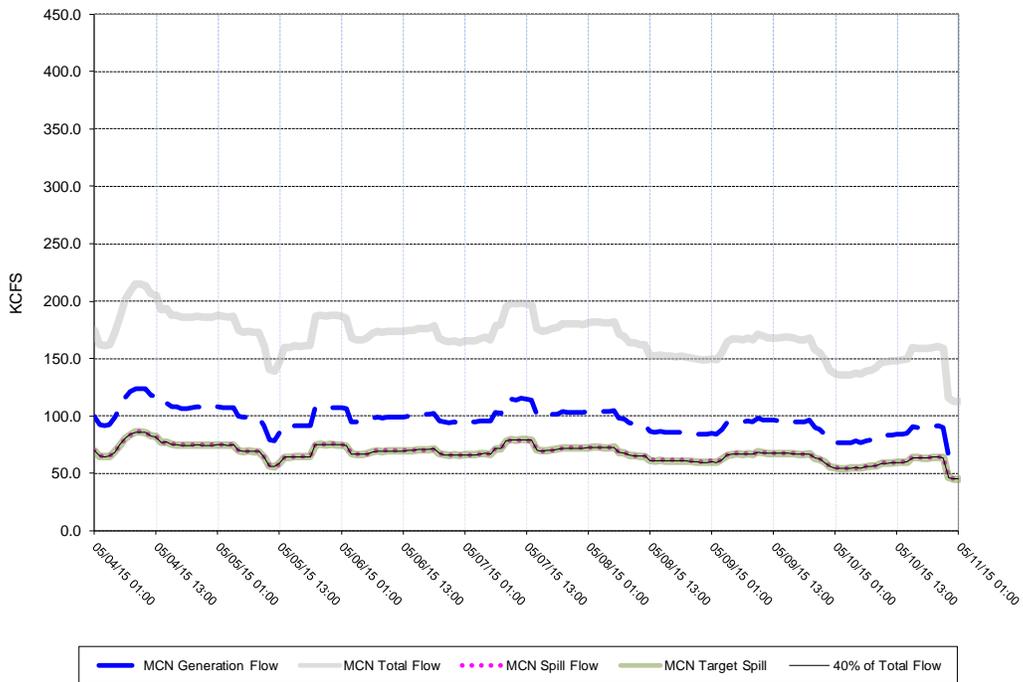
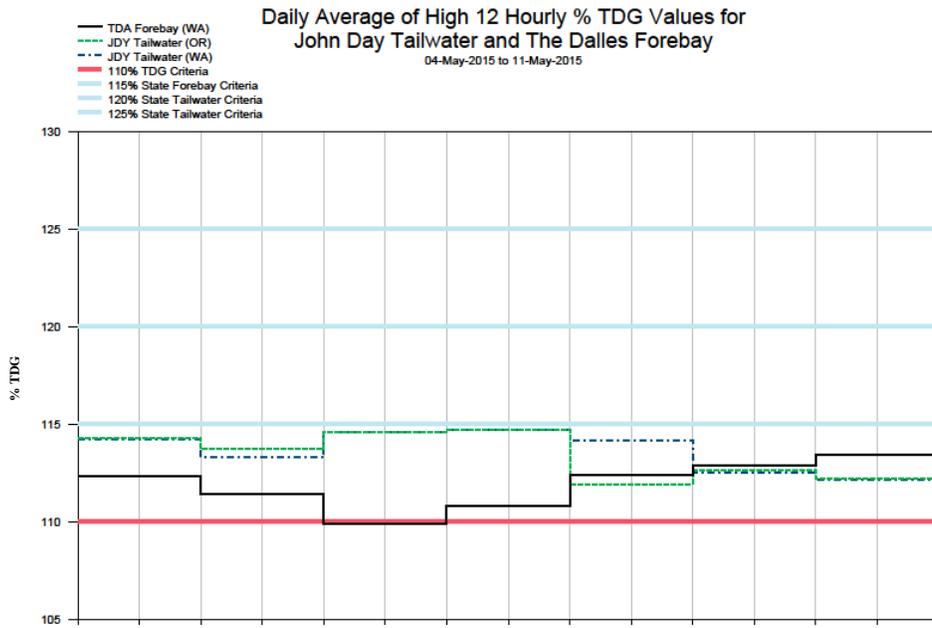


Figure 14



John Day Dam - Hourly Spill and Flow

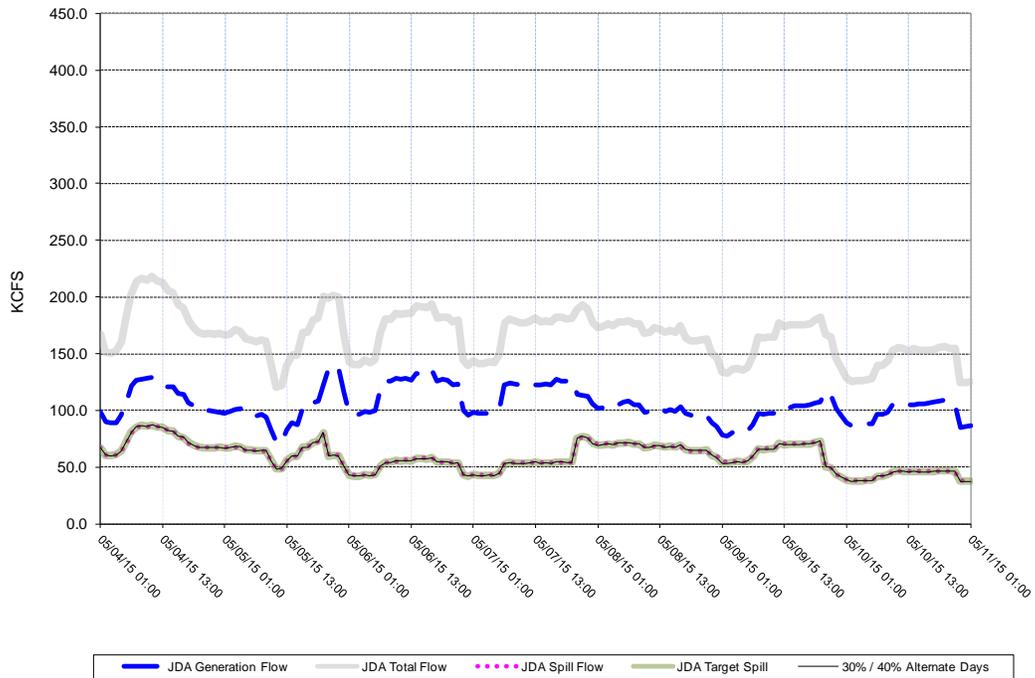
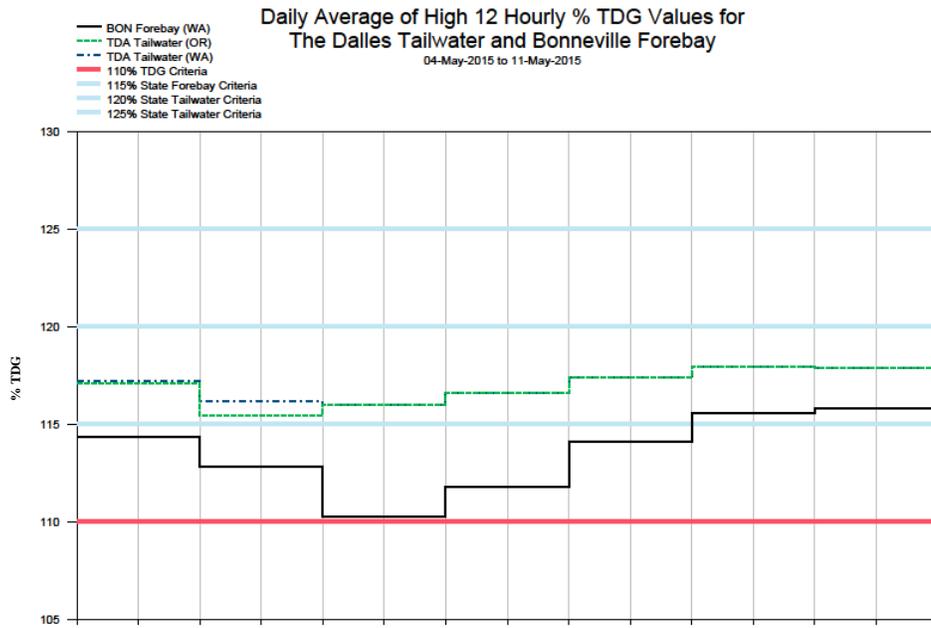


Figure 15



The Dalles Dam - Hourly Spill and Flow

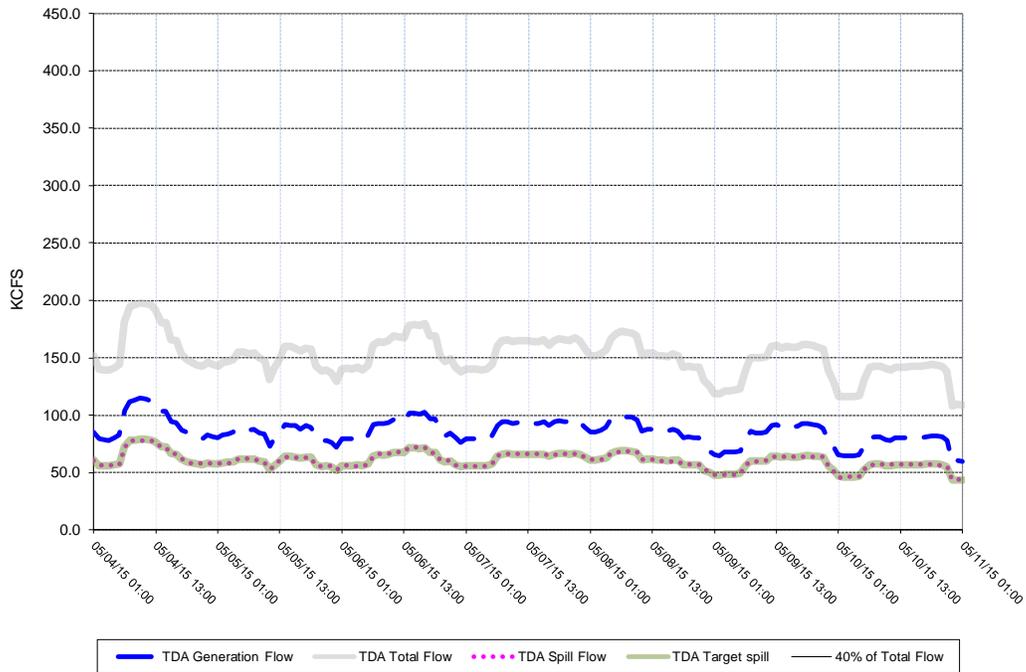


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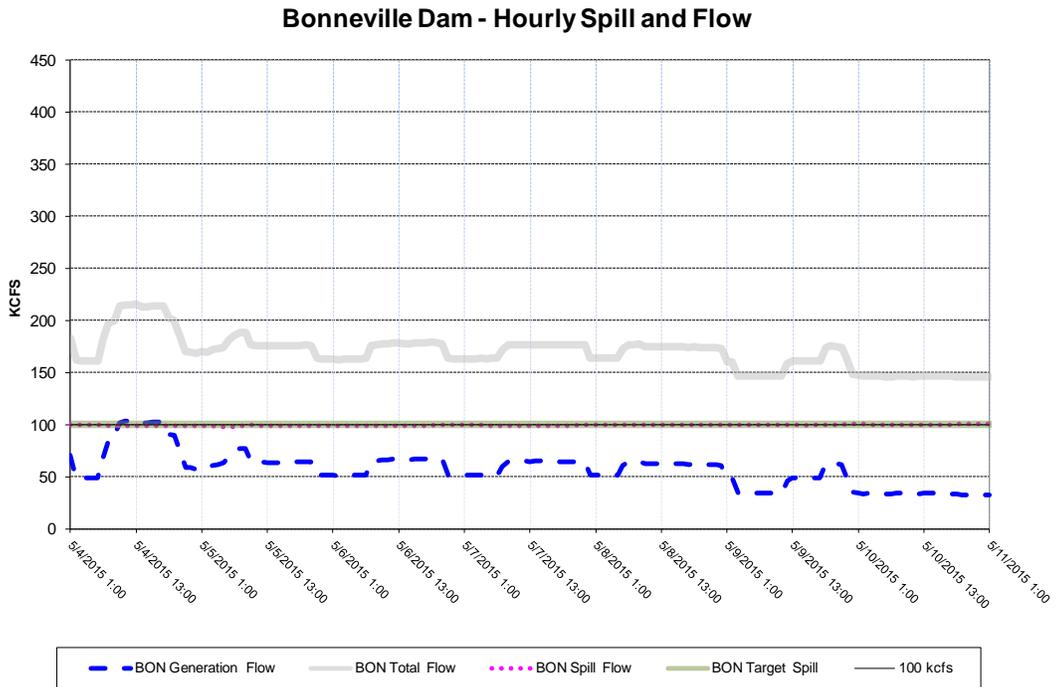
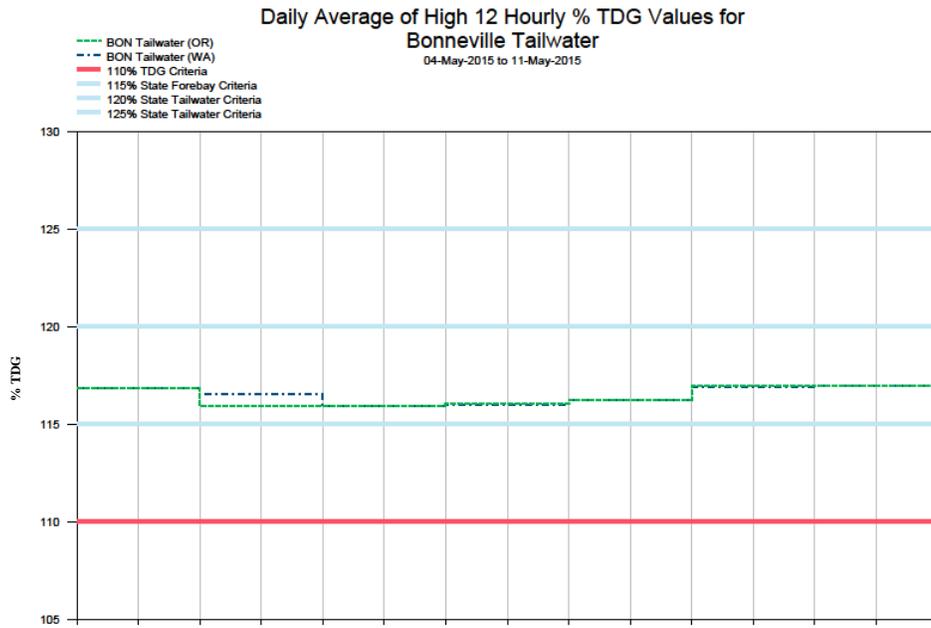


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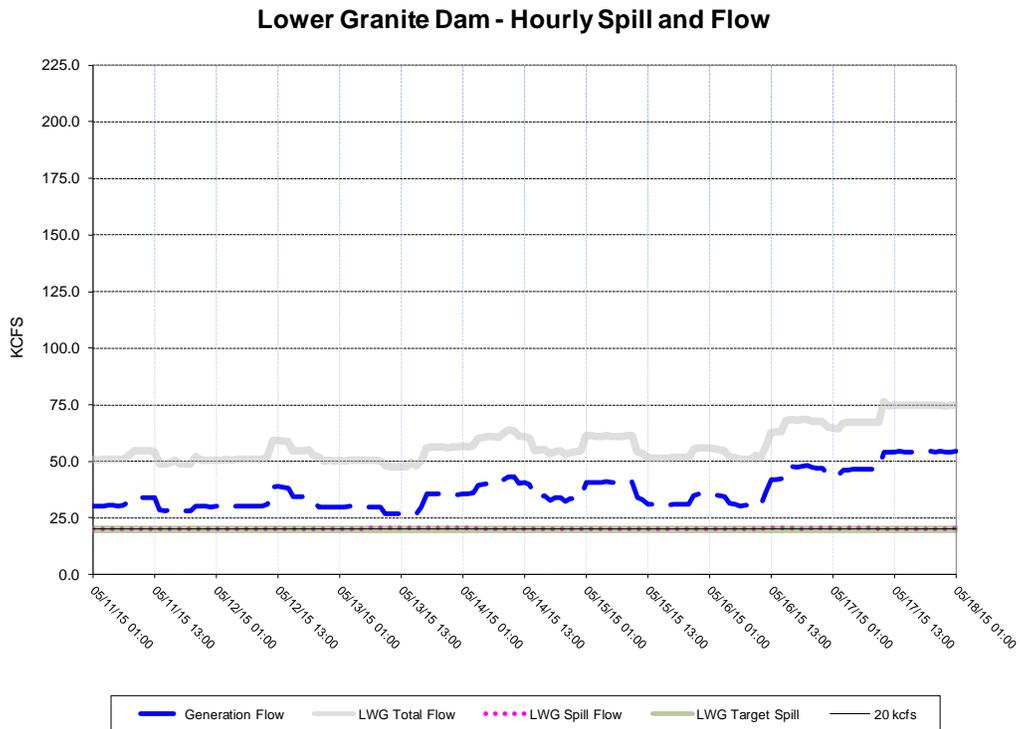
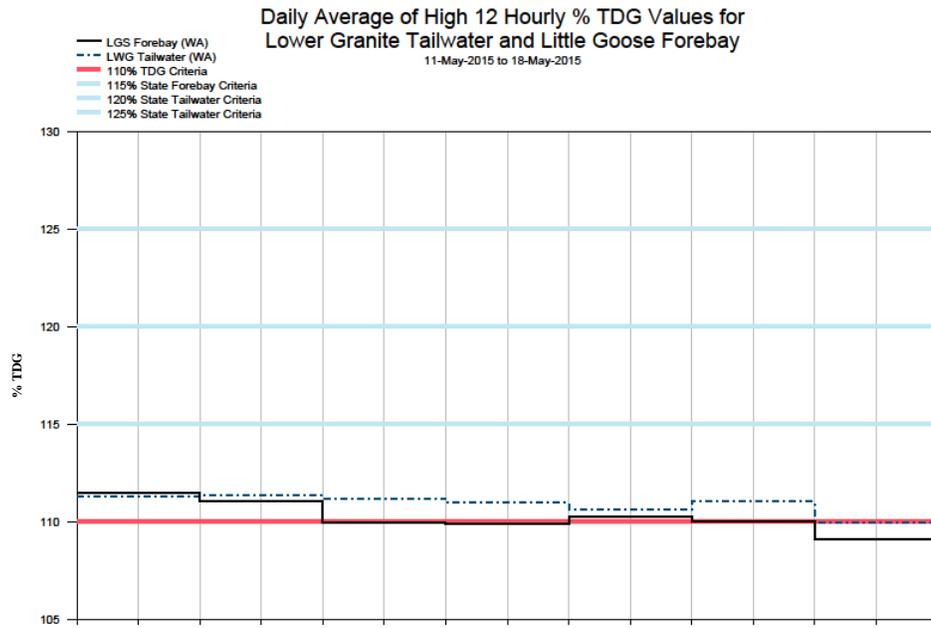
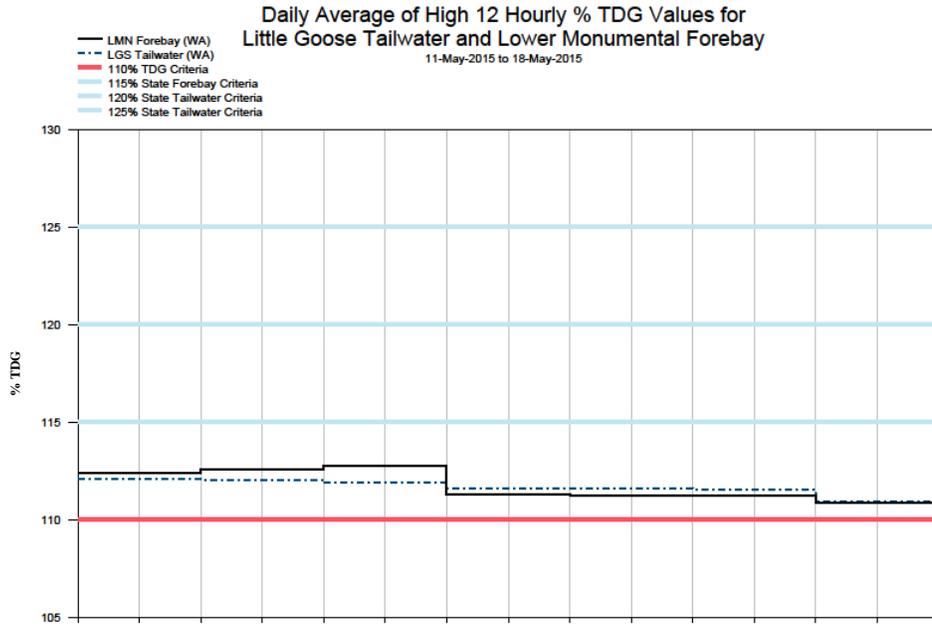


Figure 18



Little Goose Dam - Hourly Spill and Flow

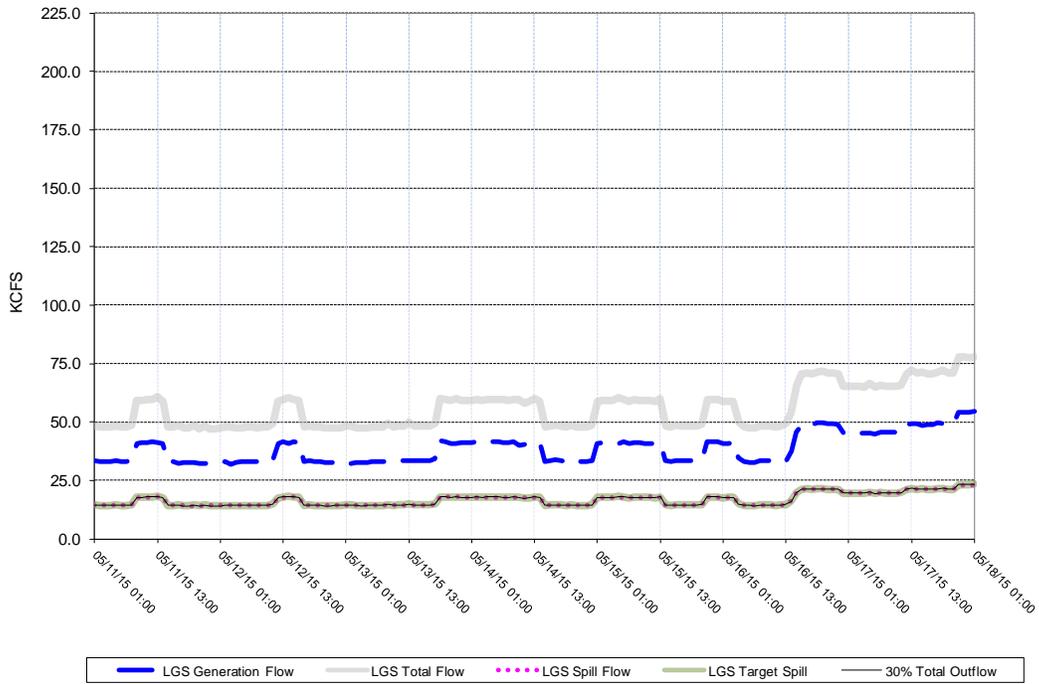


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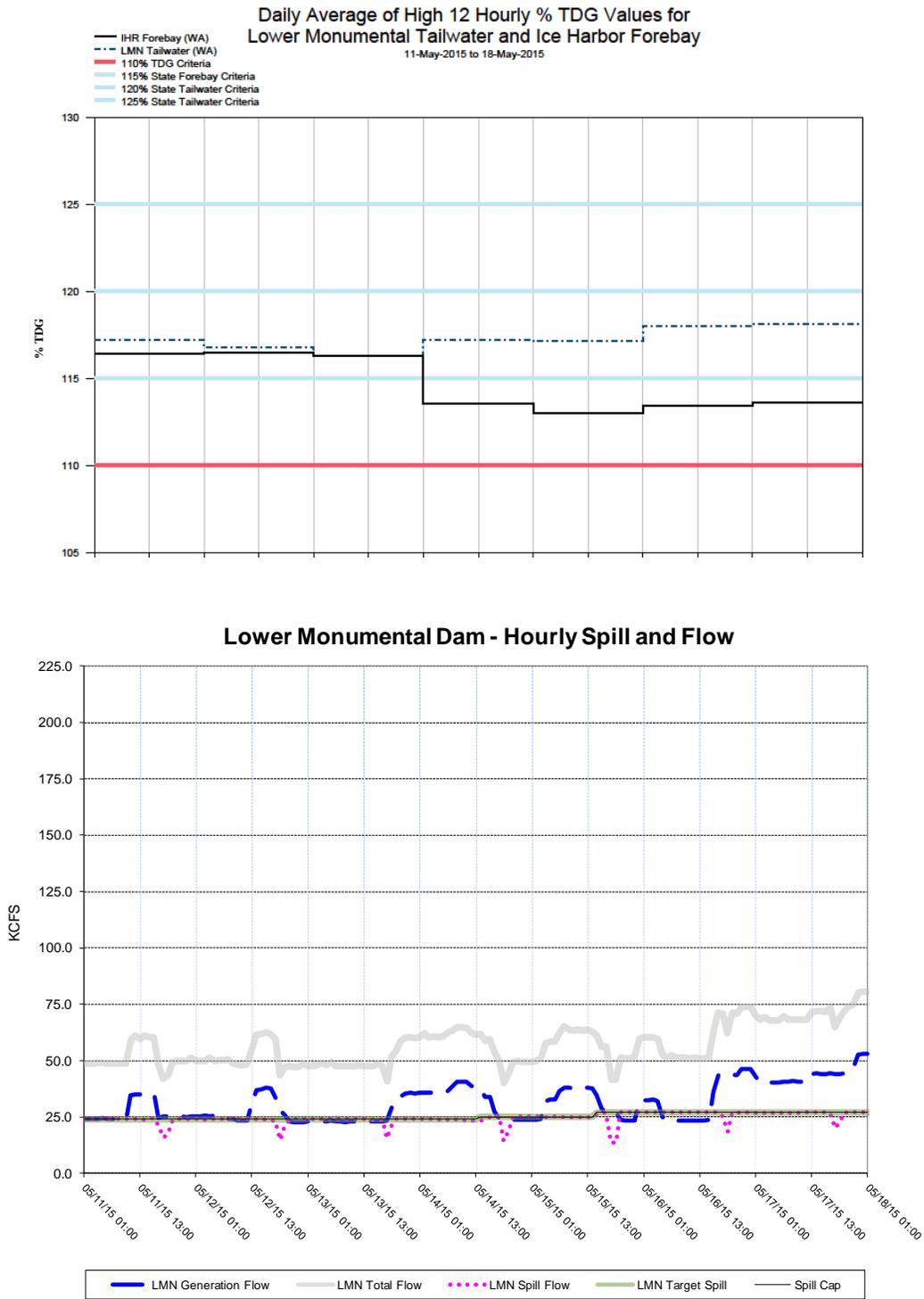


Figure 20

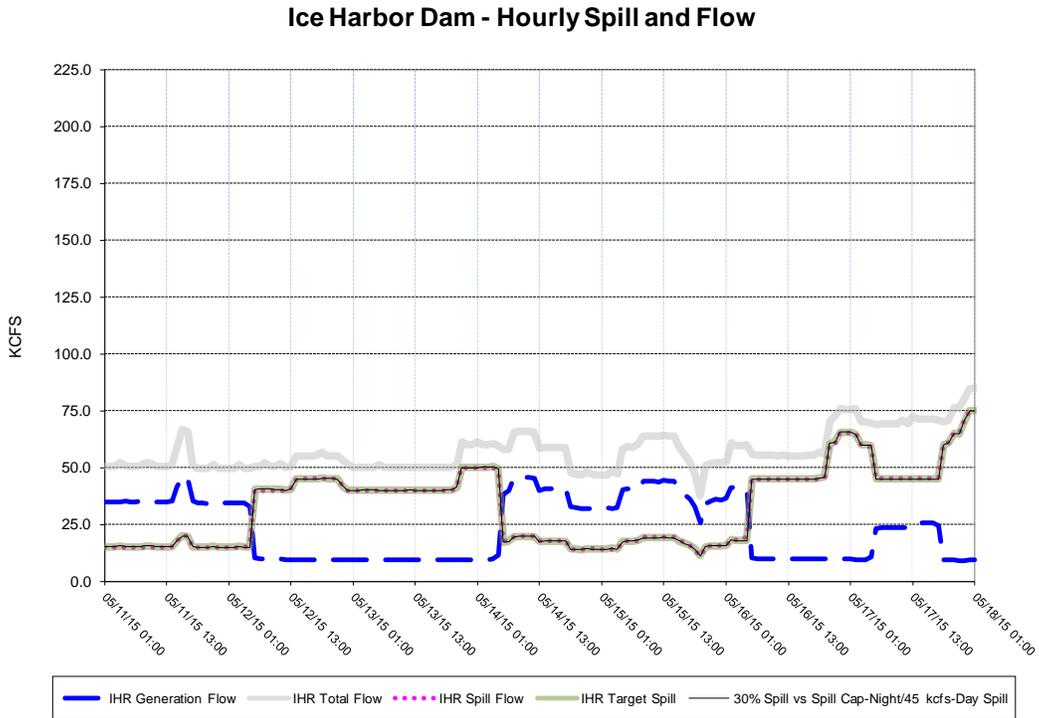
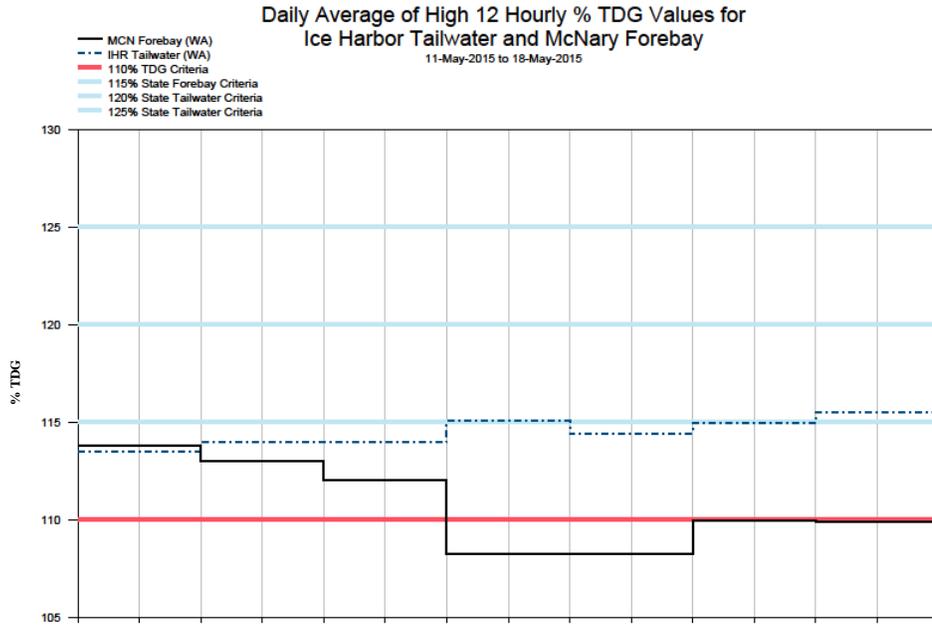
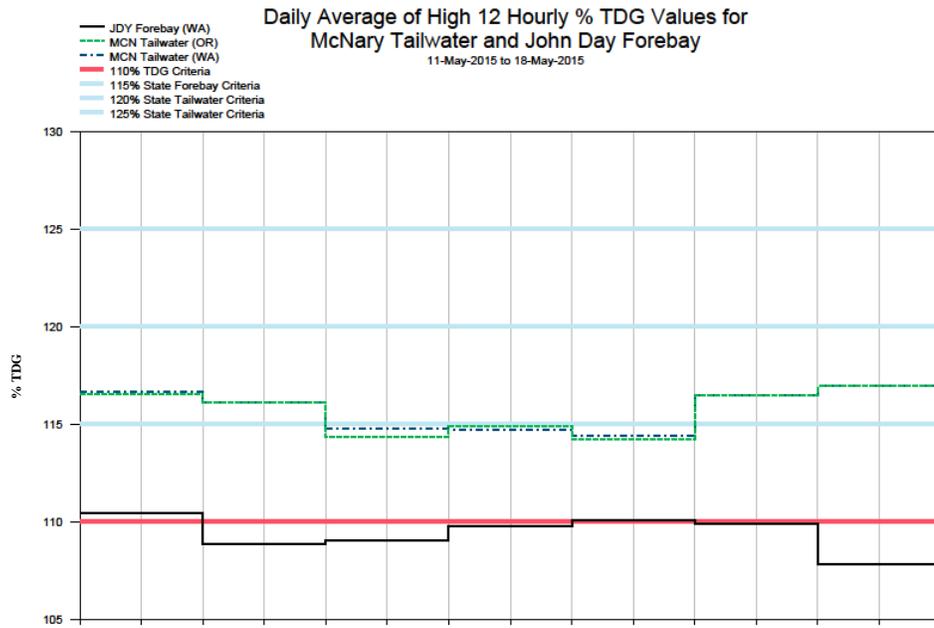


Figure 21



McNary Dam - Hourly Spill and Flow

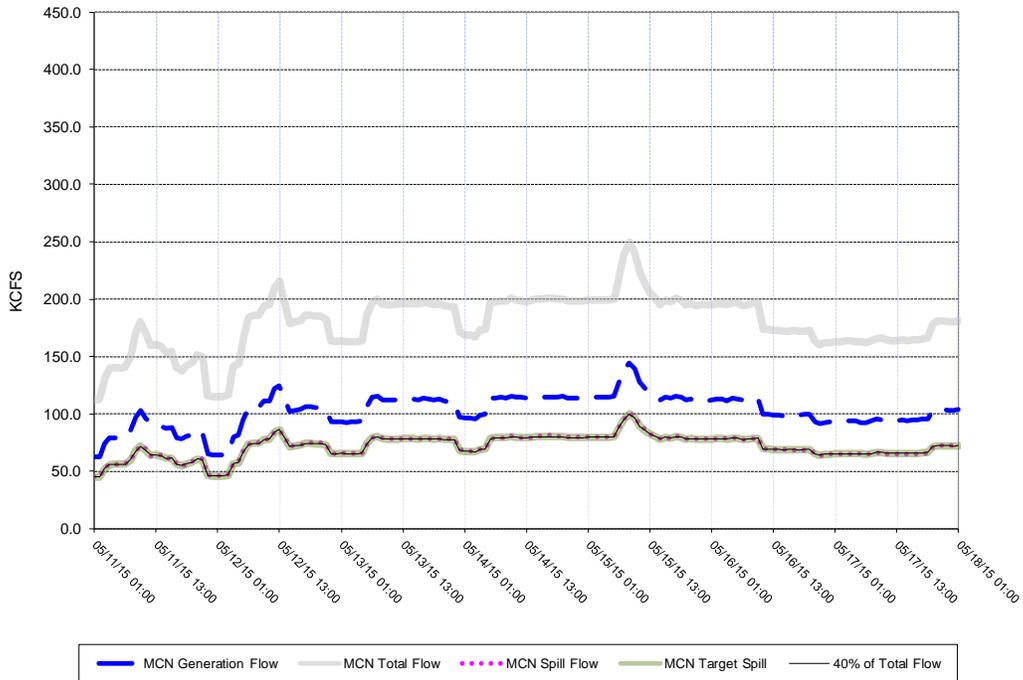
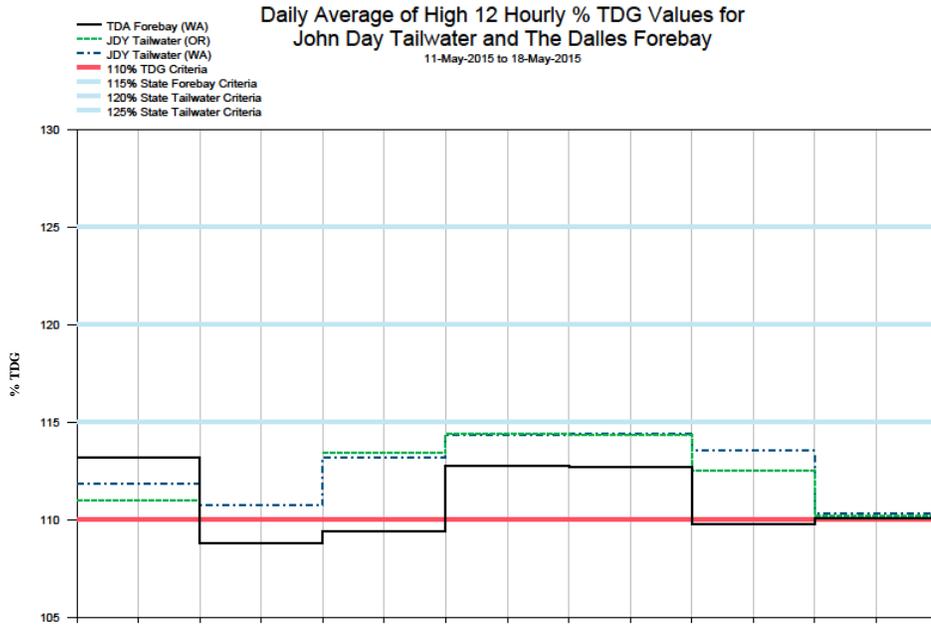


Figure 22



John Day Dam - Hourly Spill and Flow

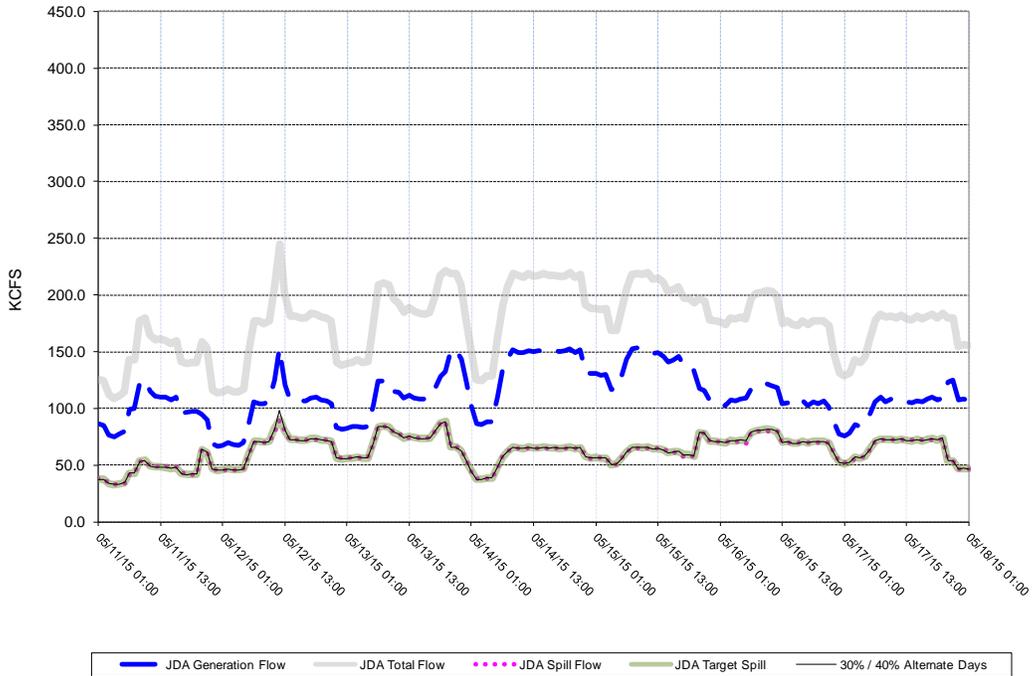
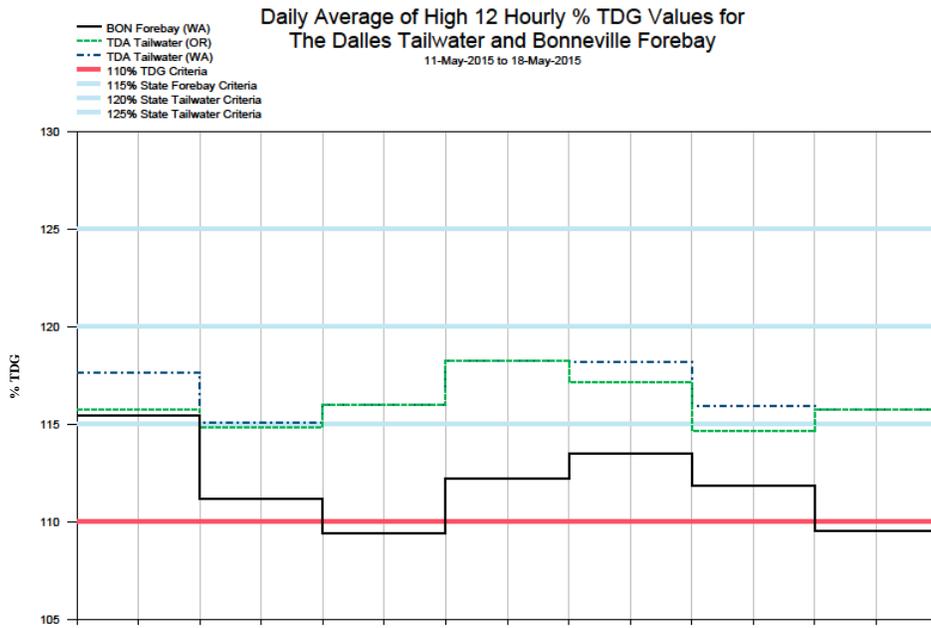


Figure 23



The Dalles Dam - Hourly Spill and Flow

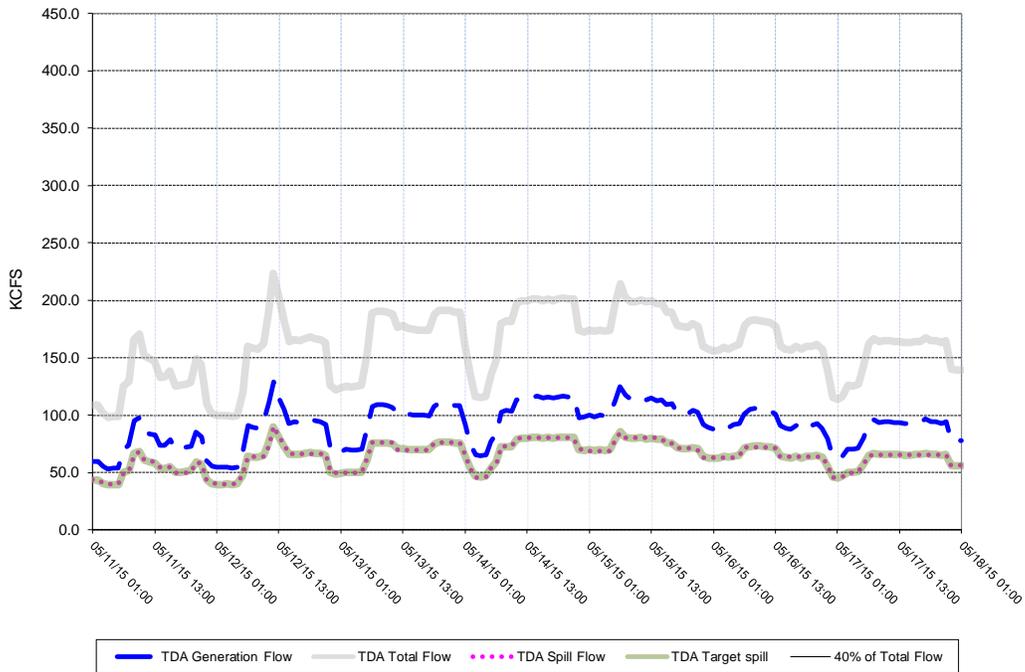


Figure 24

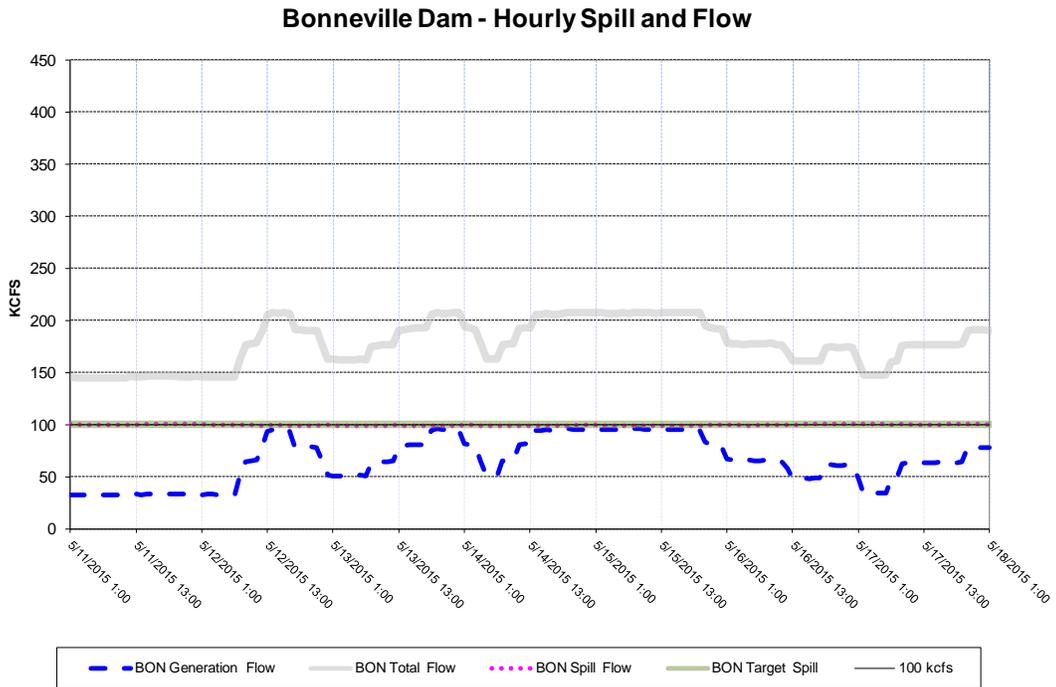
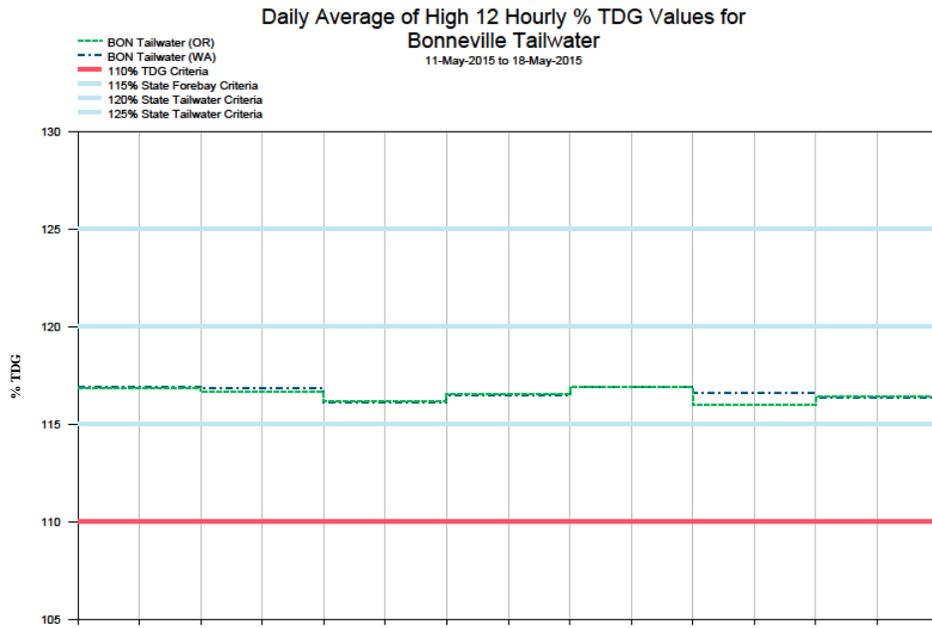


Figure 25

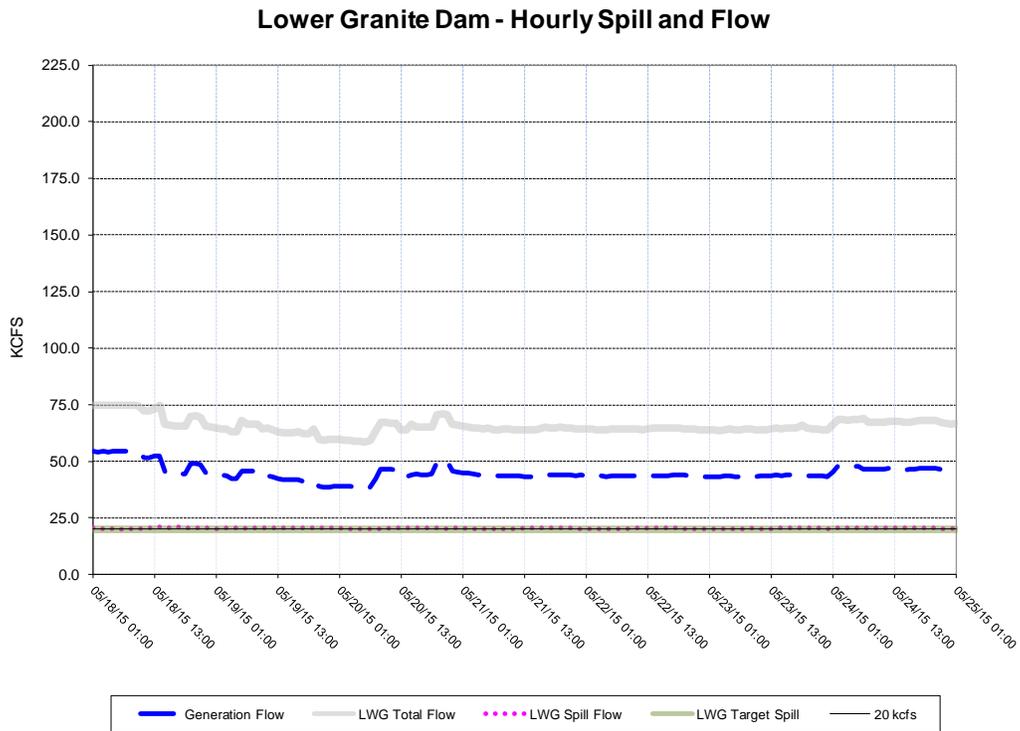
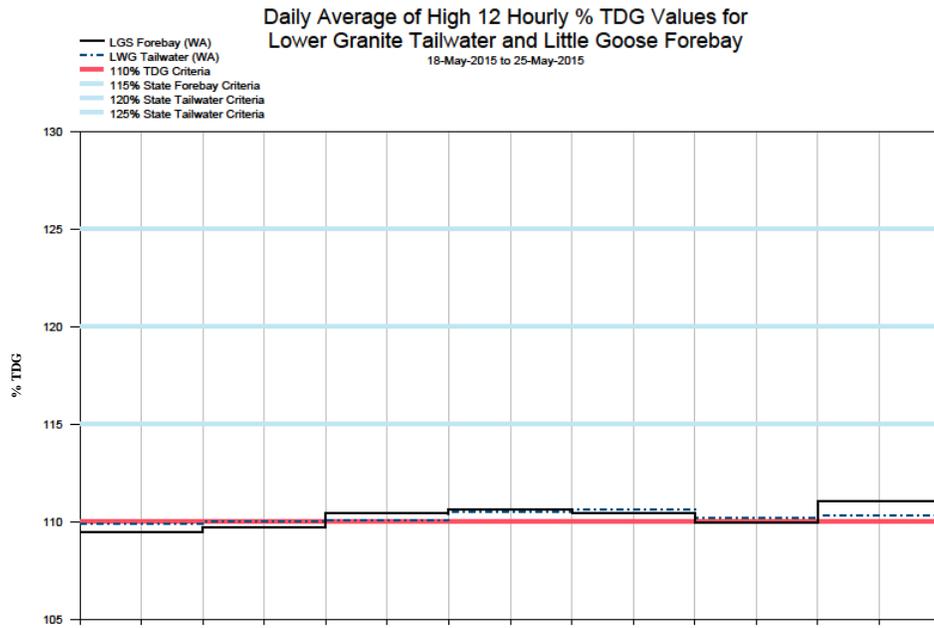
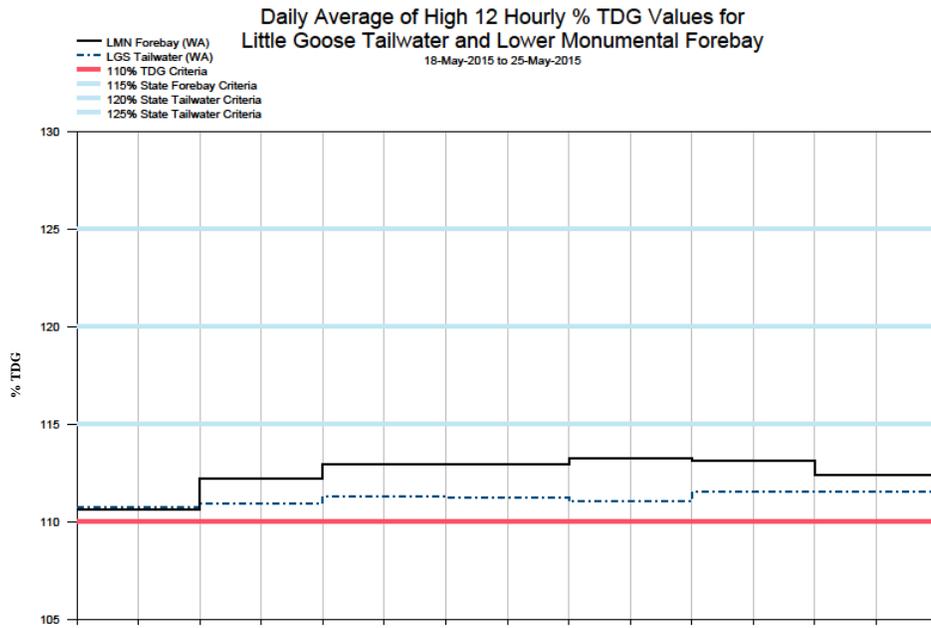


Figure 26



Little Goose Dam - Hourly Spill and Flow

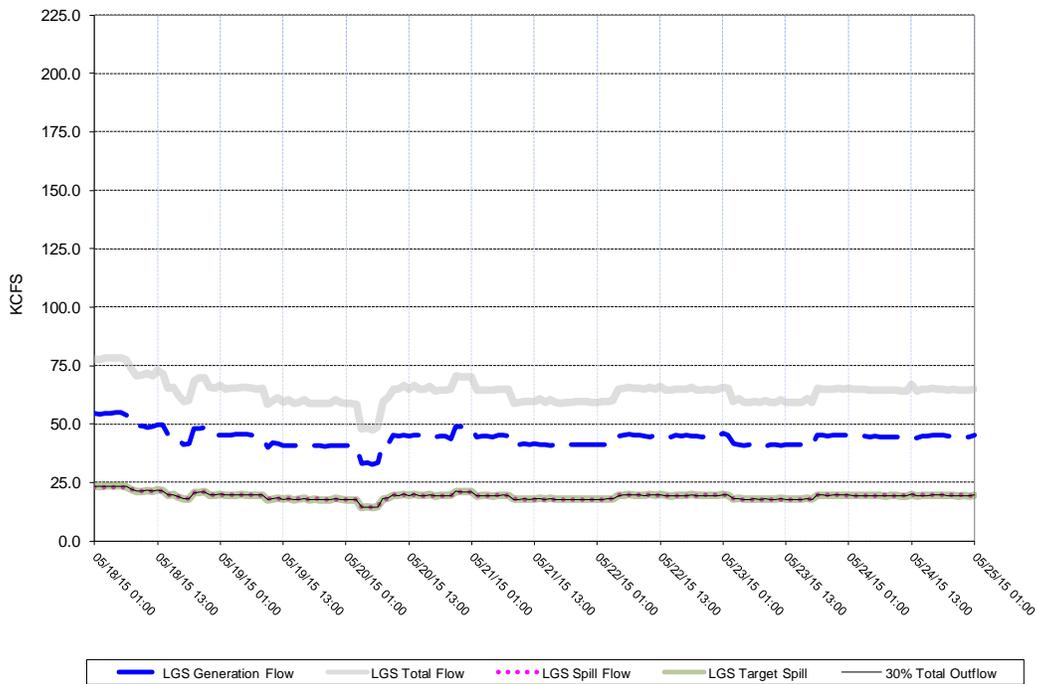


Figure 27

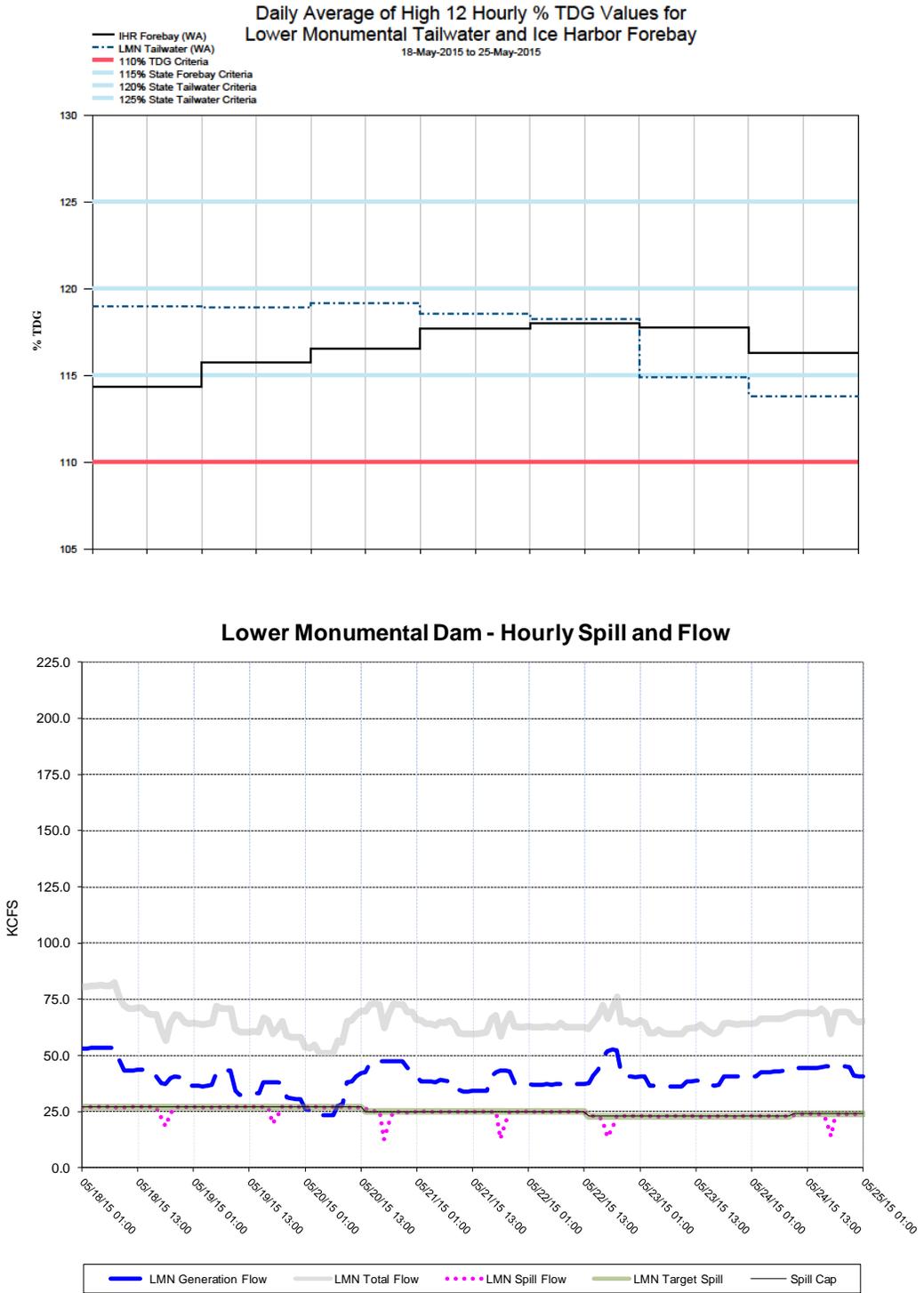


Figure 28

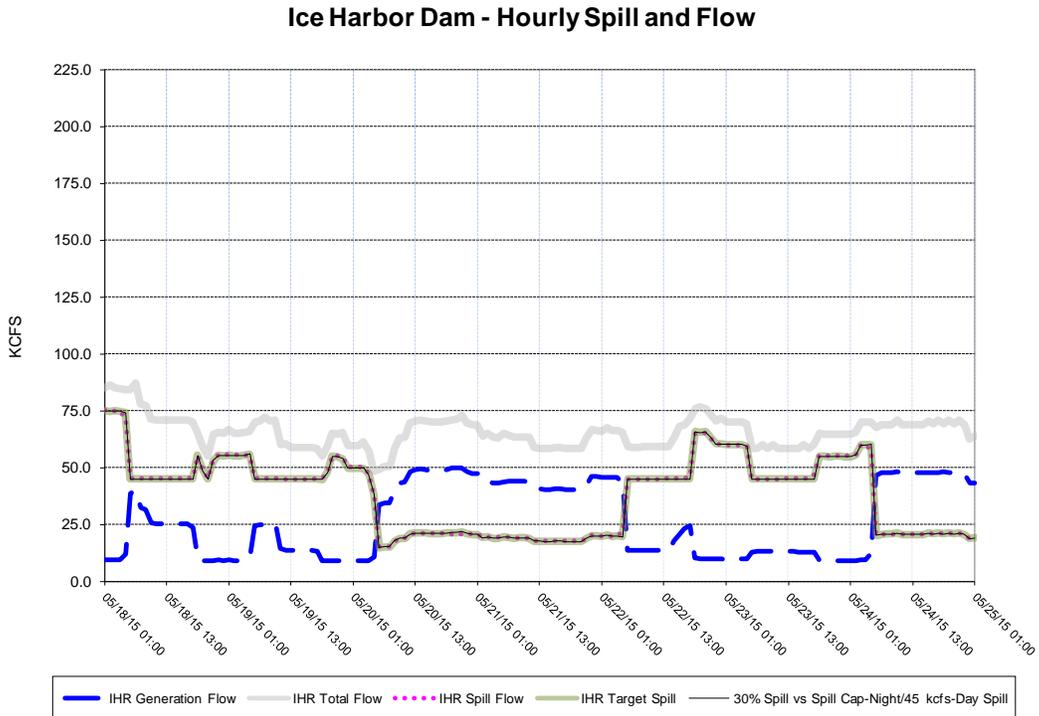
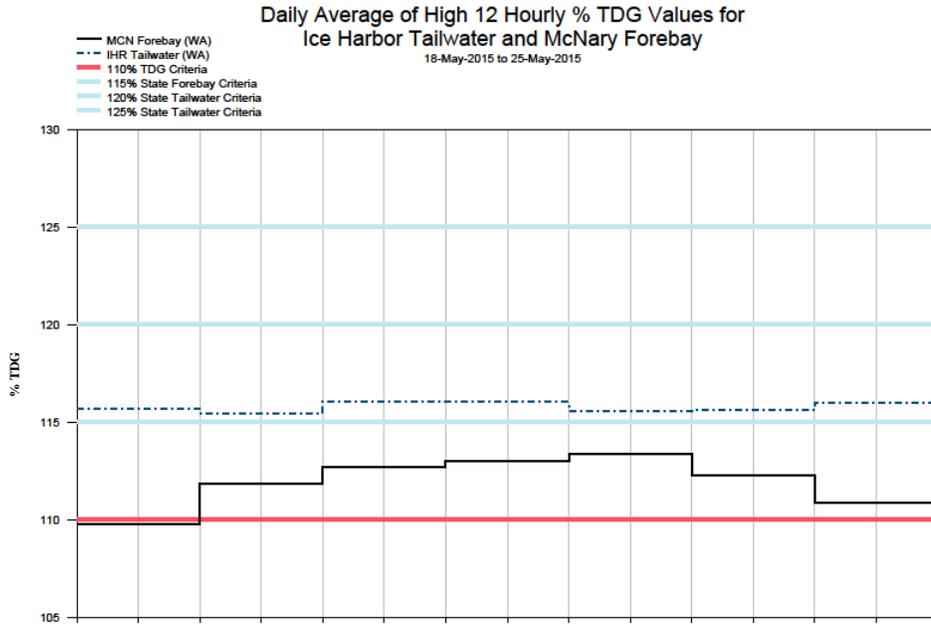
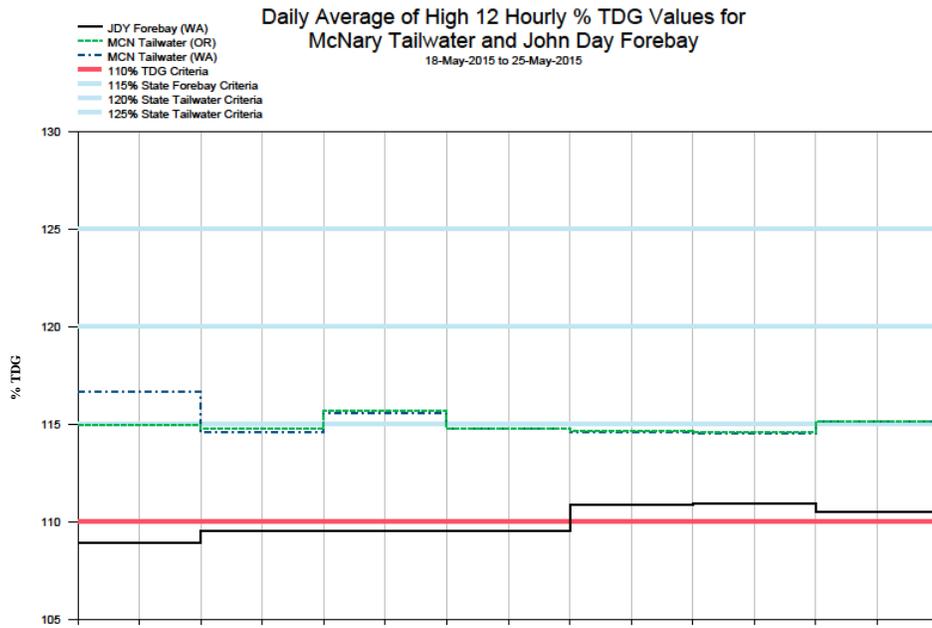


Figure 29



McNary Dam - Hourly Spill and Flow

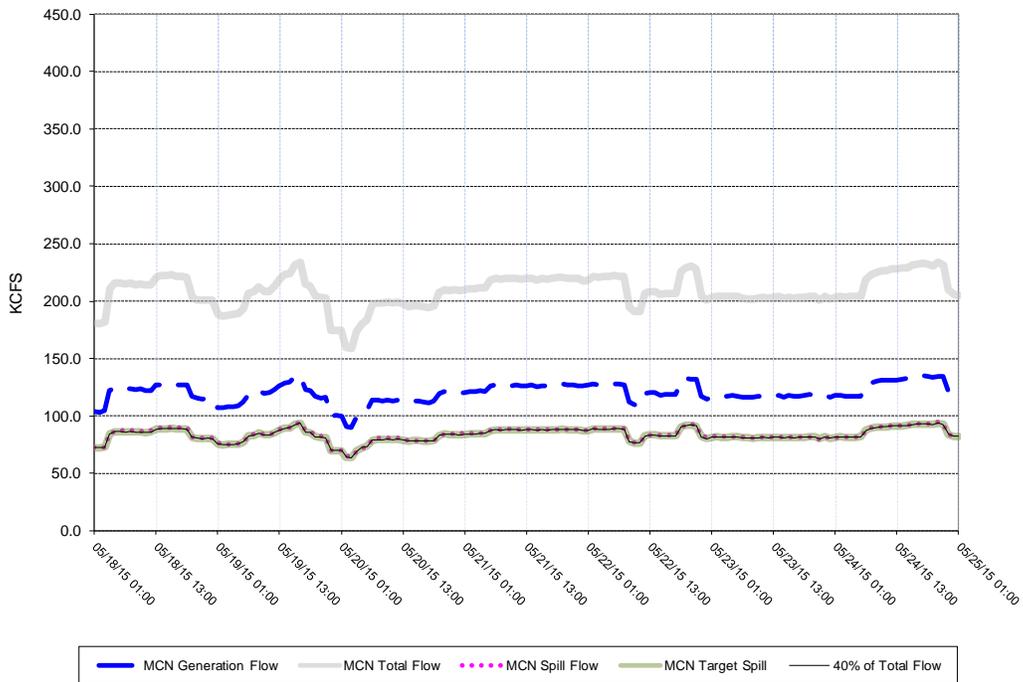
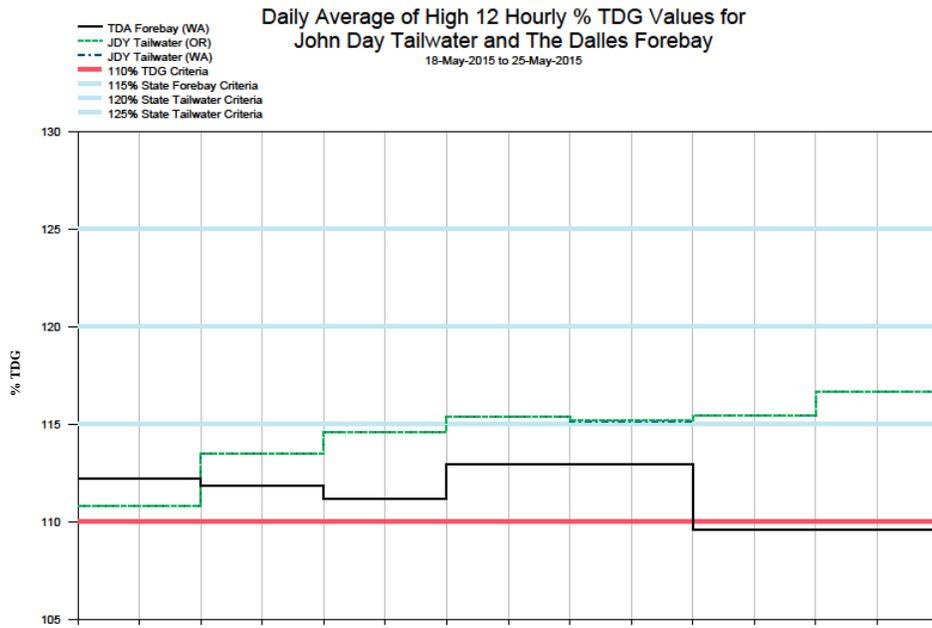


Figure 30



John Day Dam - Hourly Spill and Flow

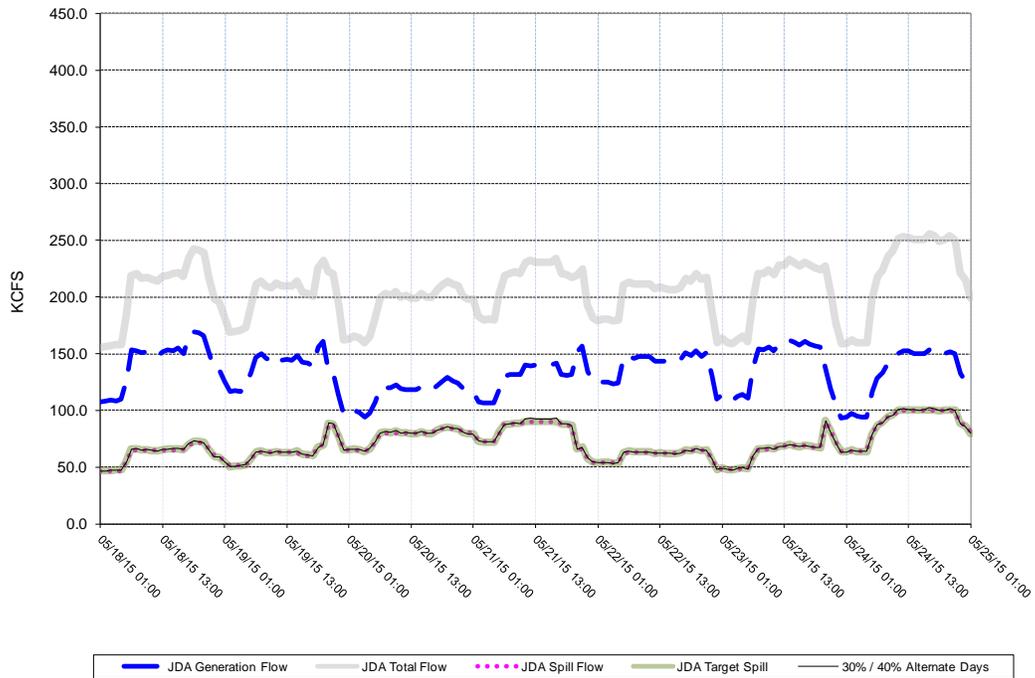
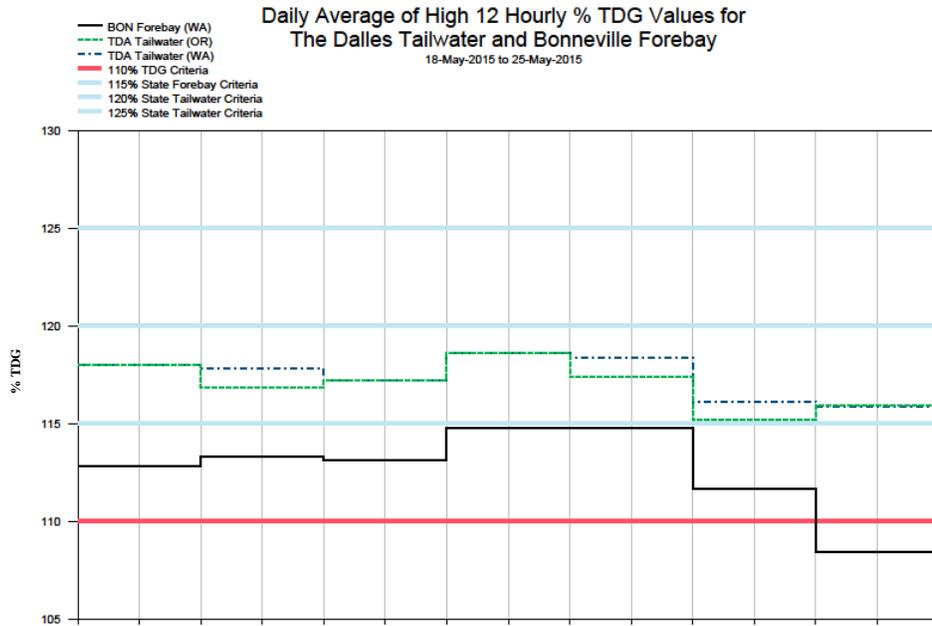


Figure 31



The Dalles Dam - Hourly Spill and Flow

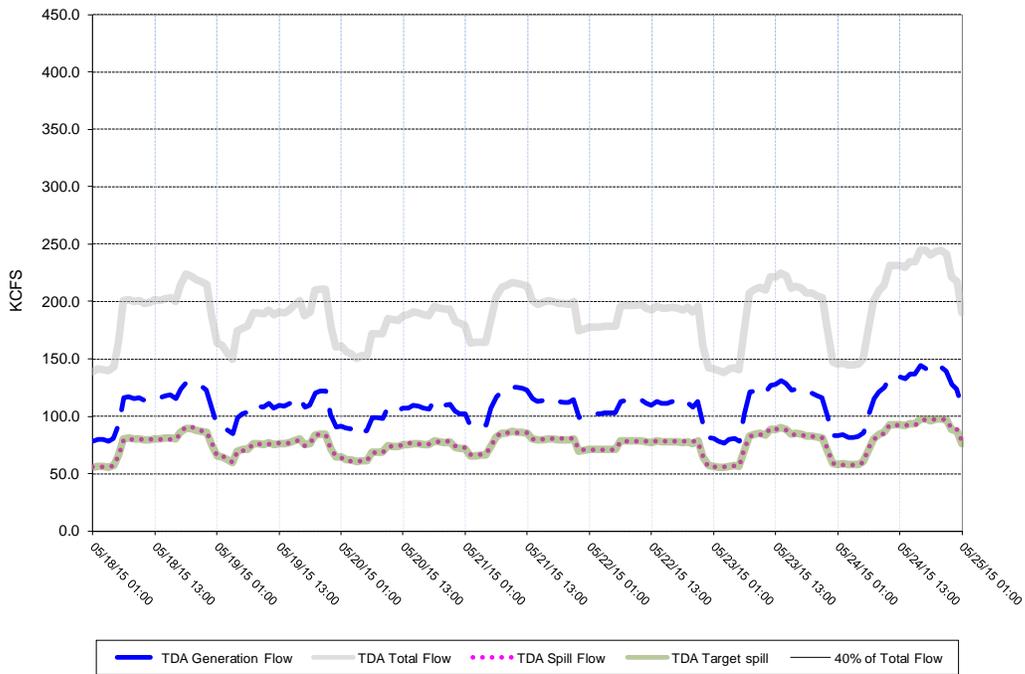


Figure 32

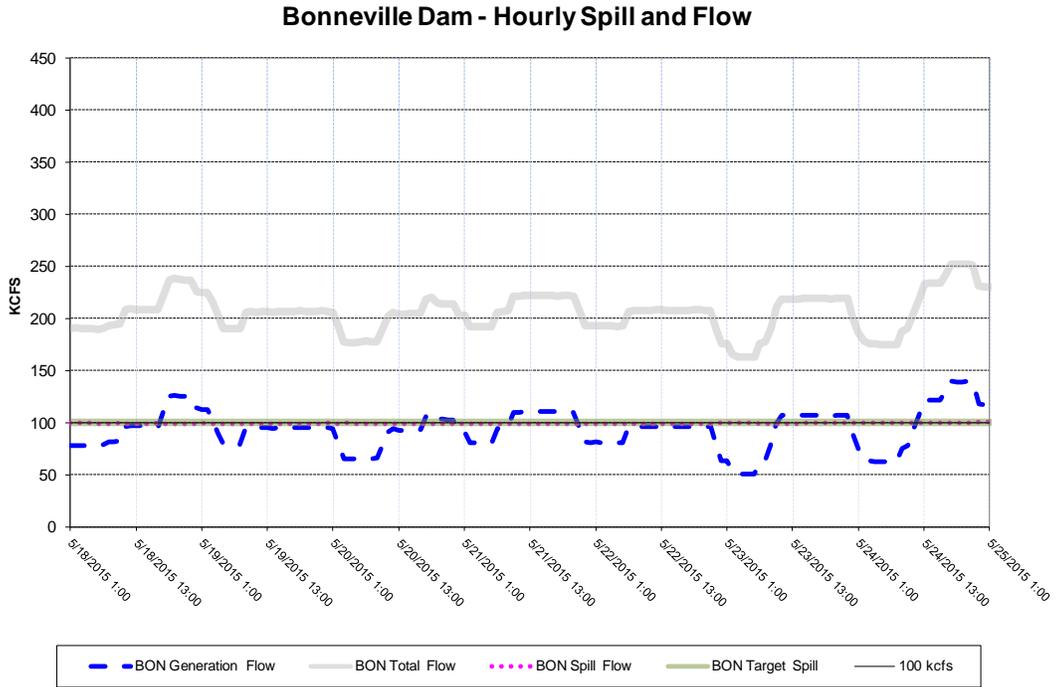
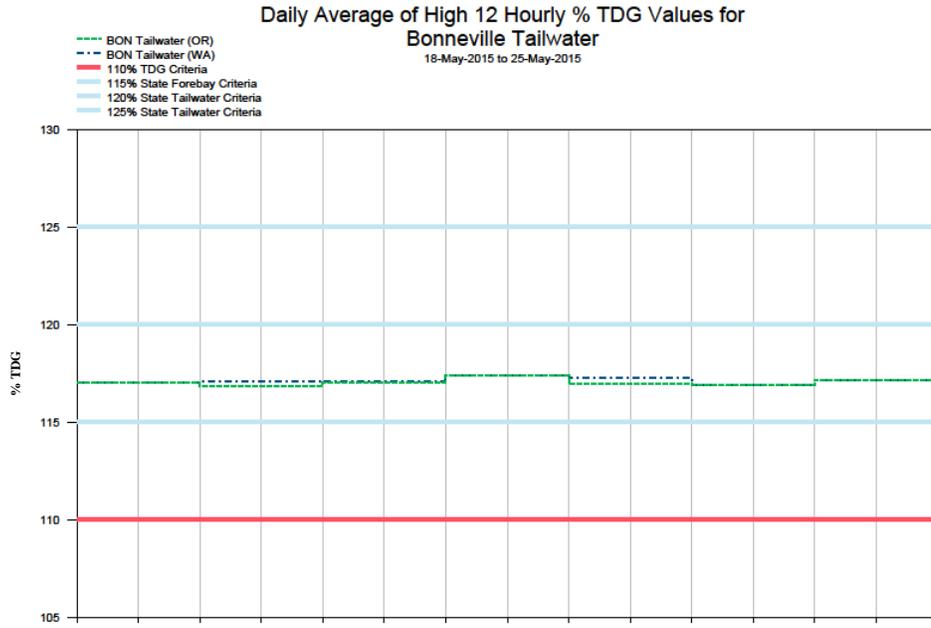


Figure 33

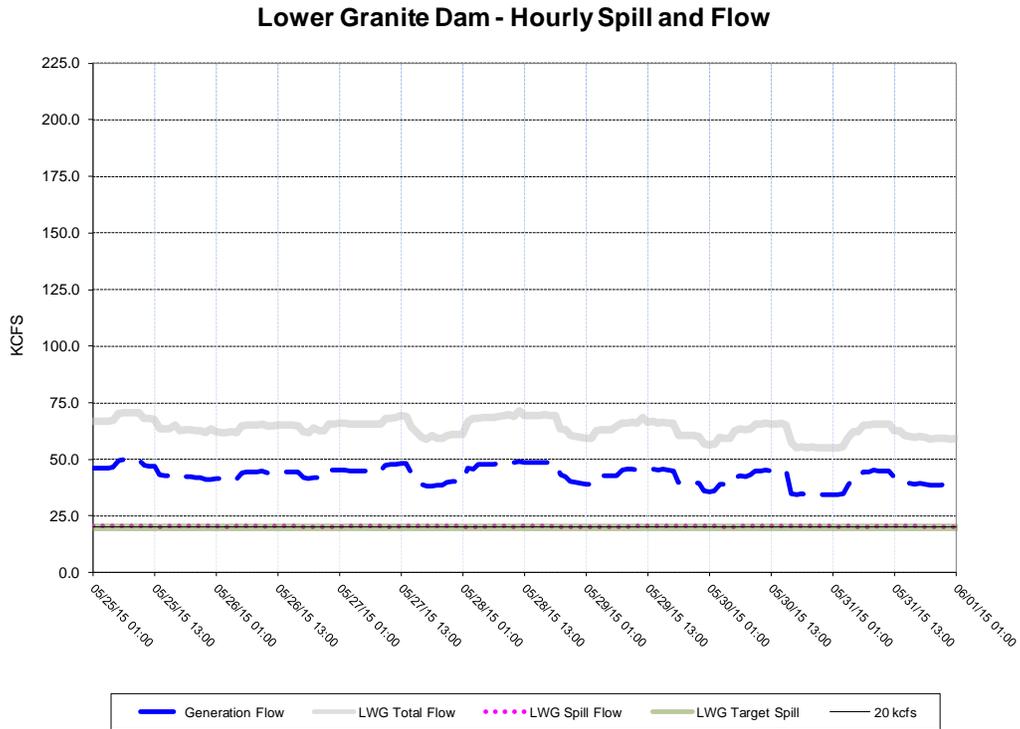
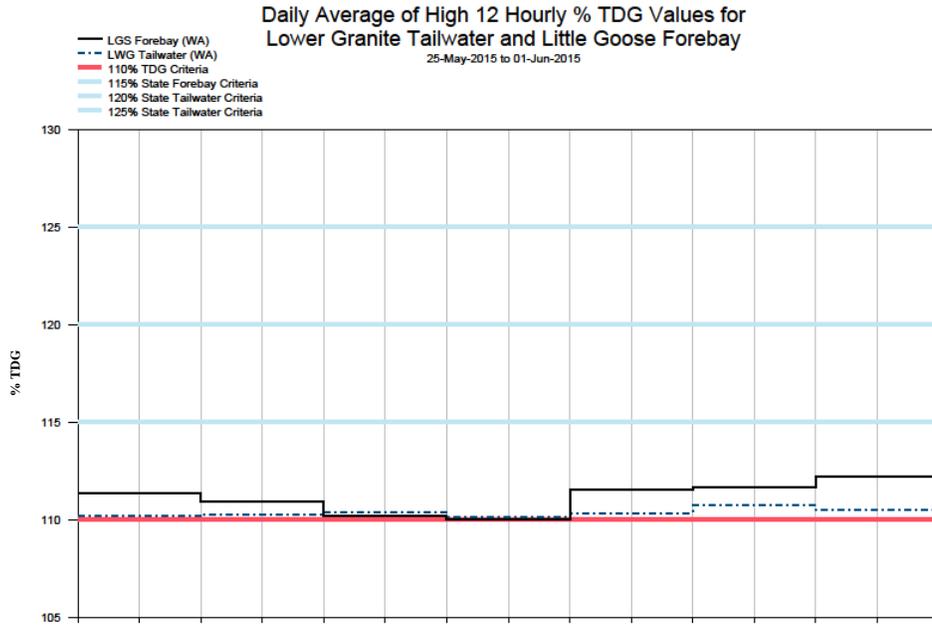
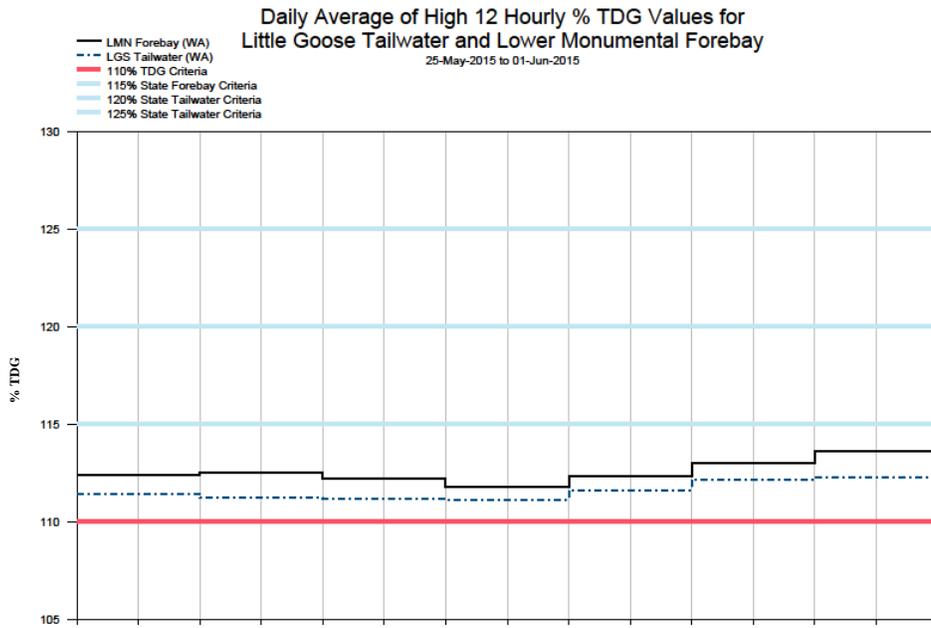


Figure 34



Little Goose Dam - Hourly Spill and Flow

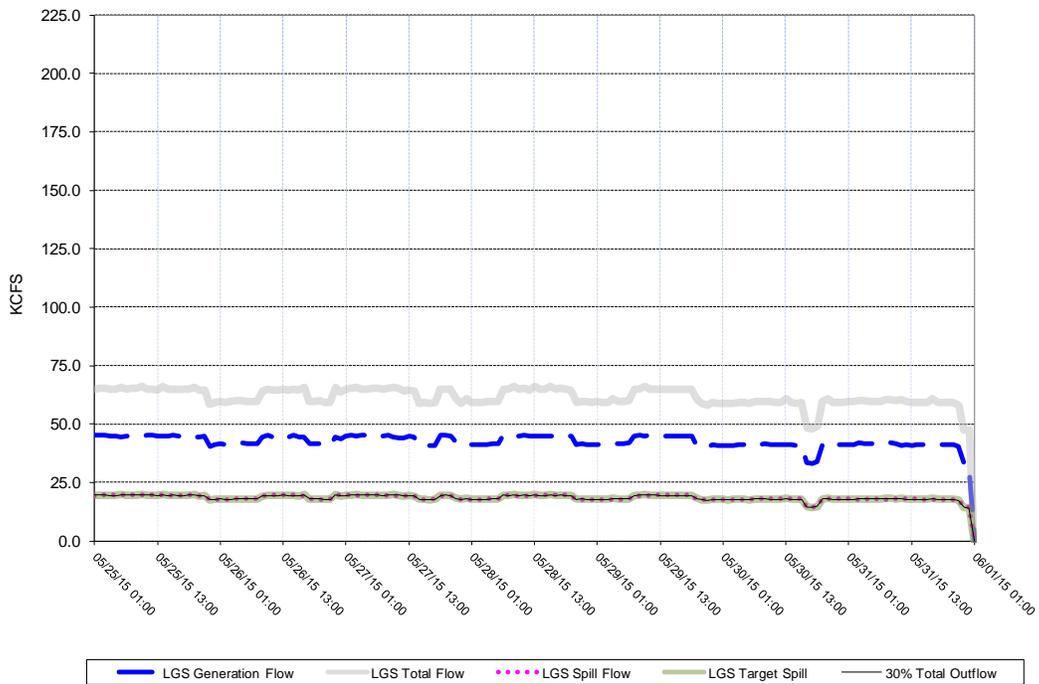


Figure 35

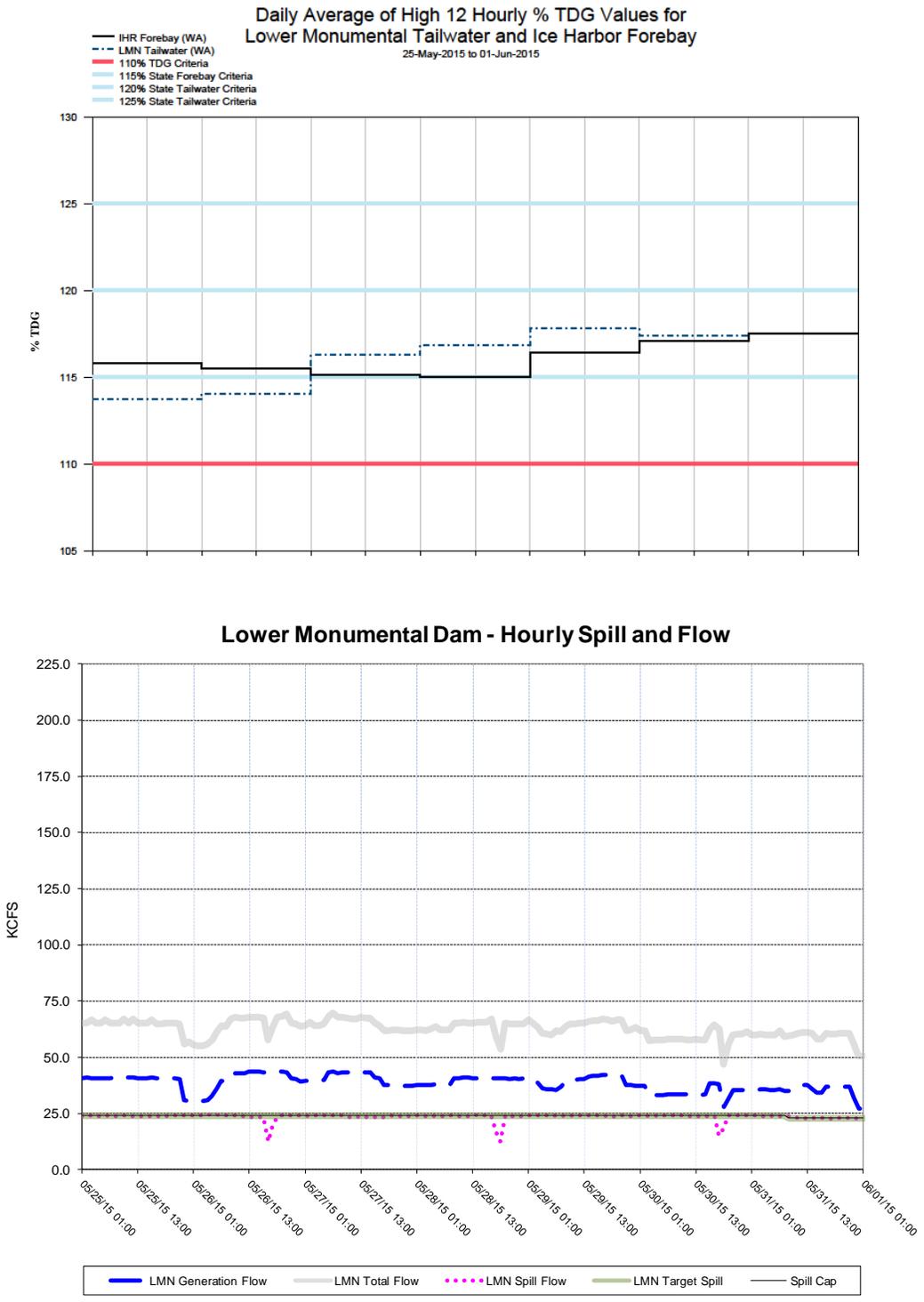


Figure 36

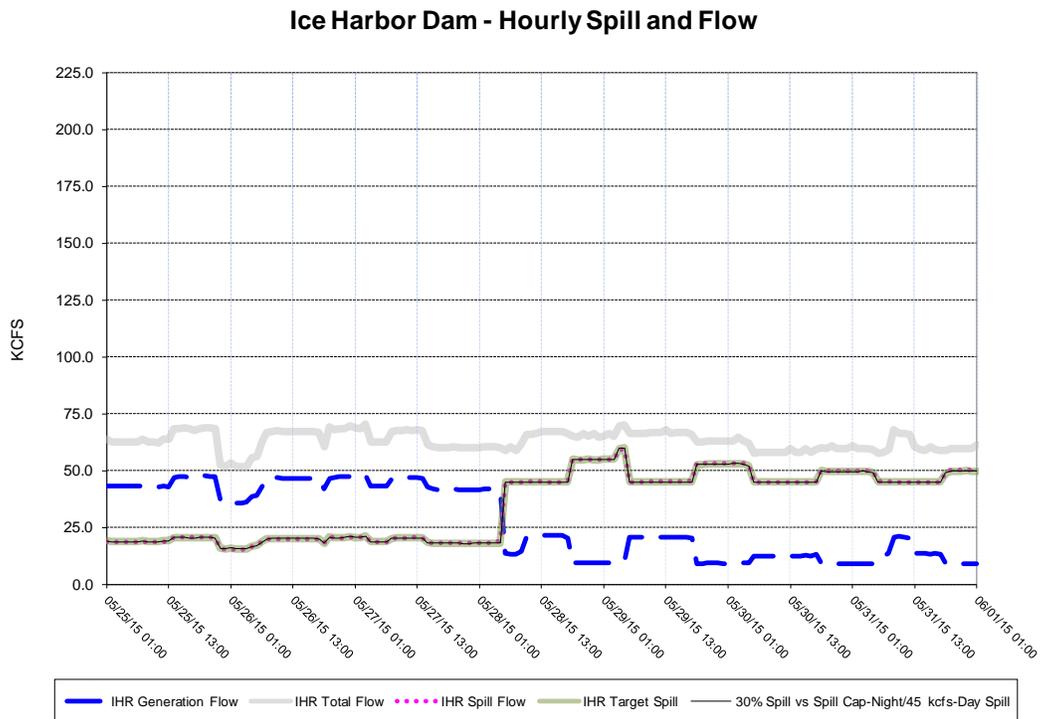
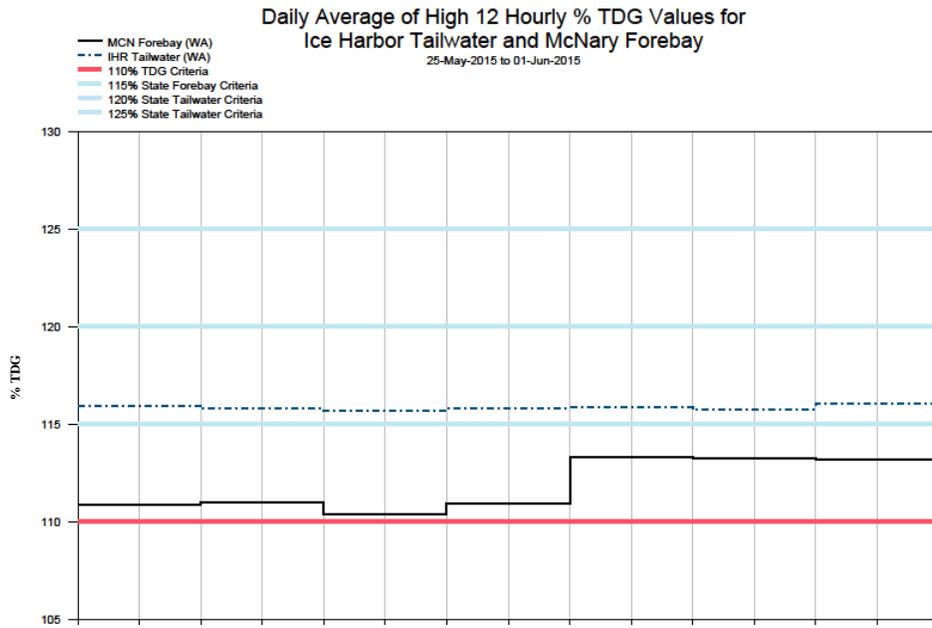
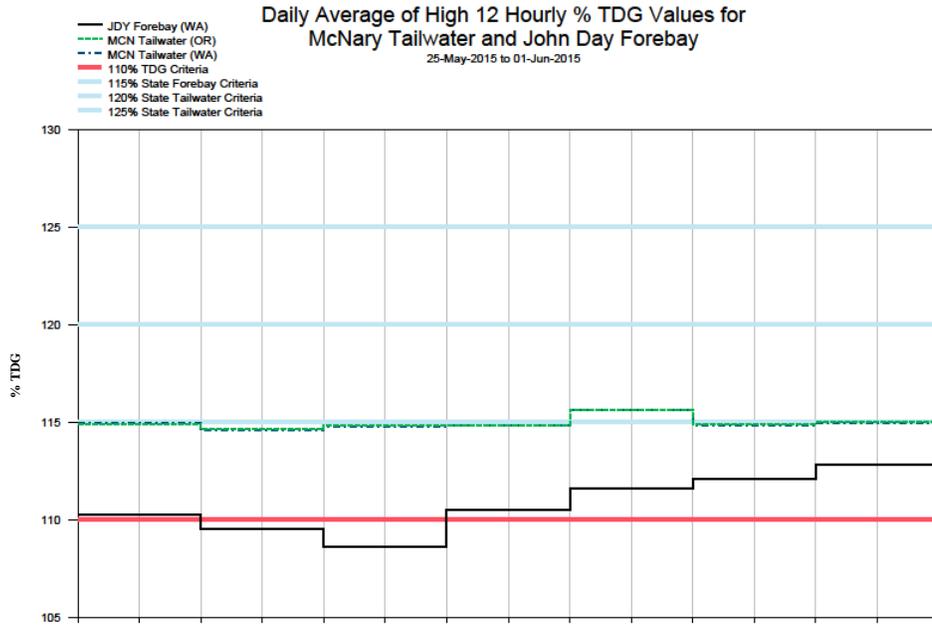


Figure 37



McNary Dam - Hourly Spill and Flow

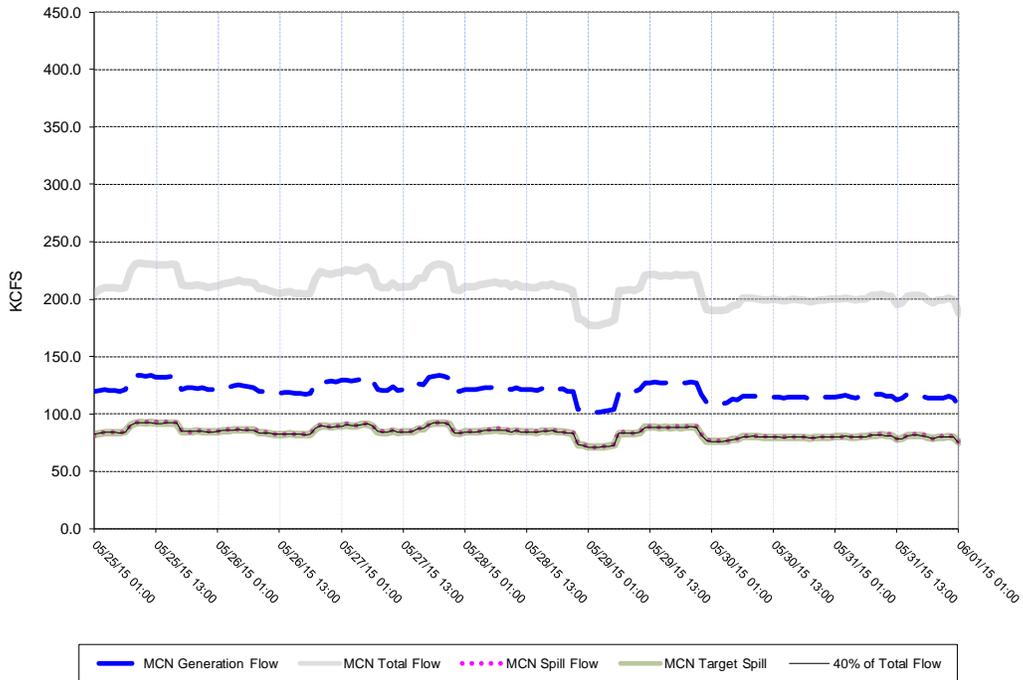
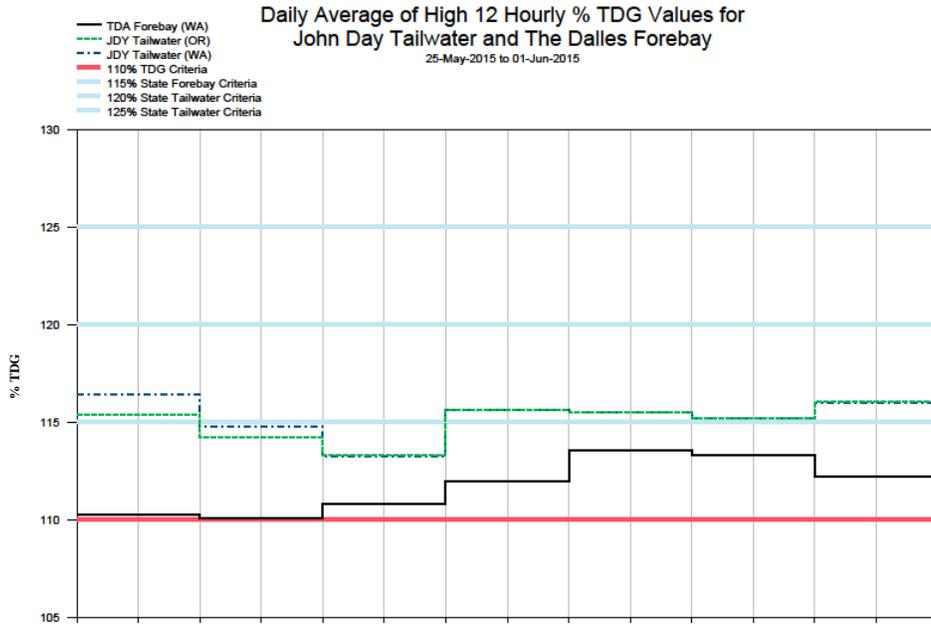


Figure 38



John Day Dam - Hourly Spill and Flow

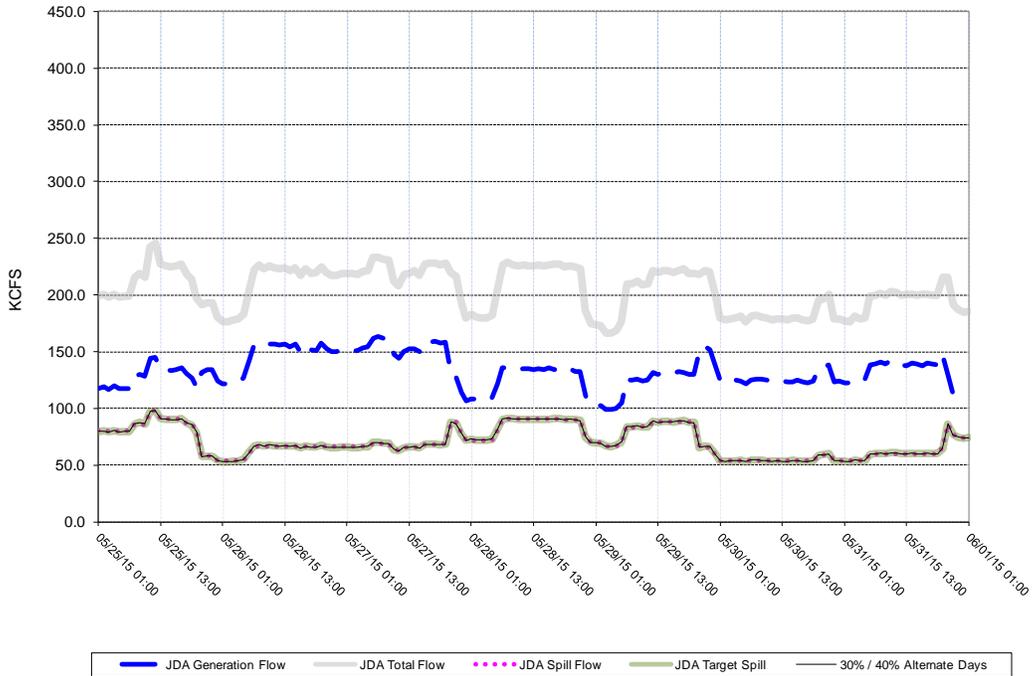
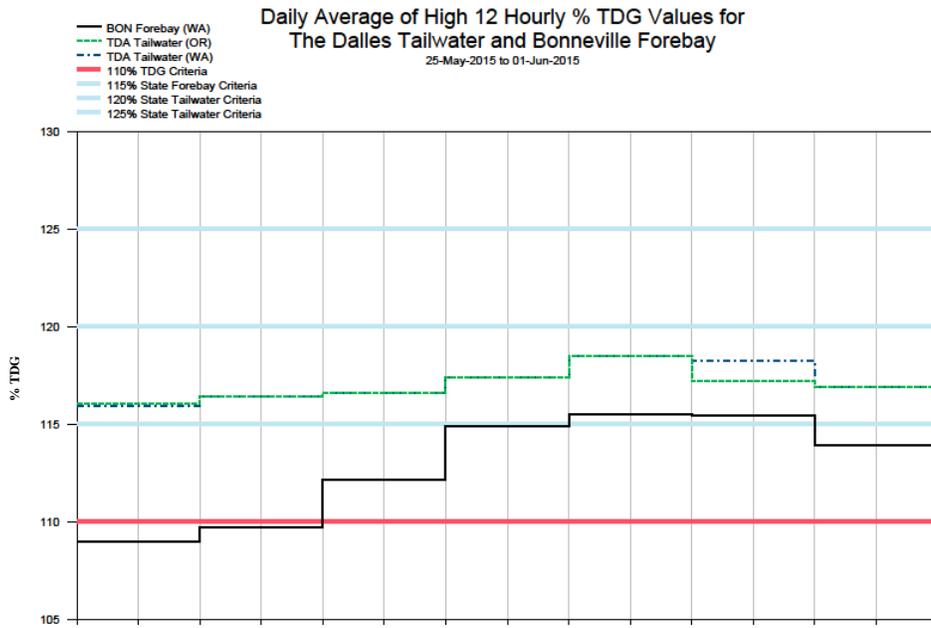


Figure 39



The Dalles Dam - Hourly Spill and Flow

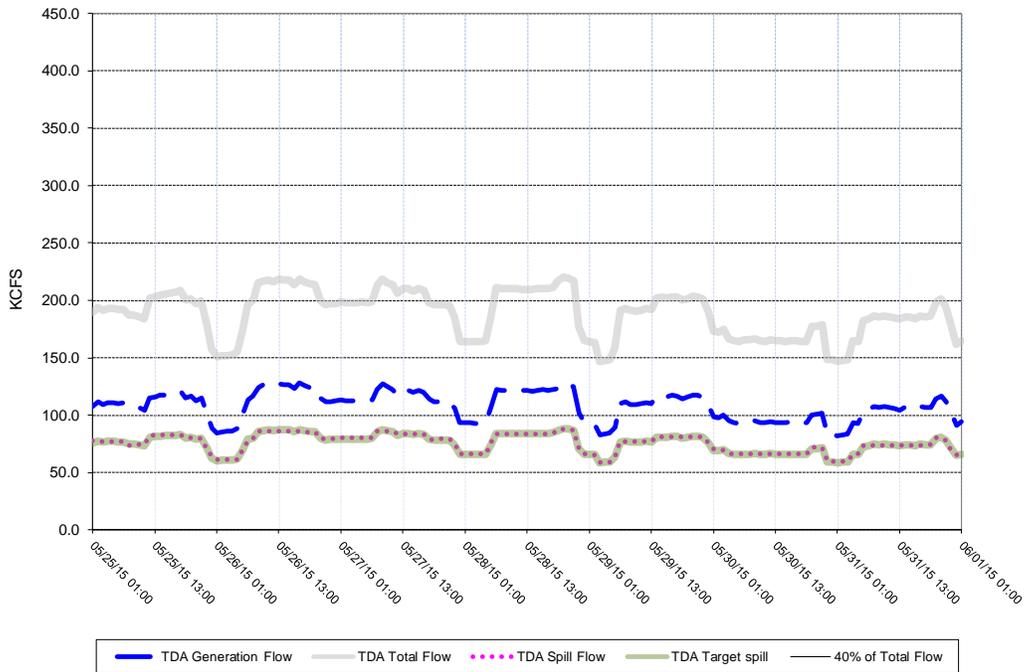


Figure 40

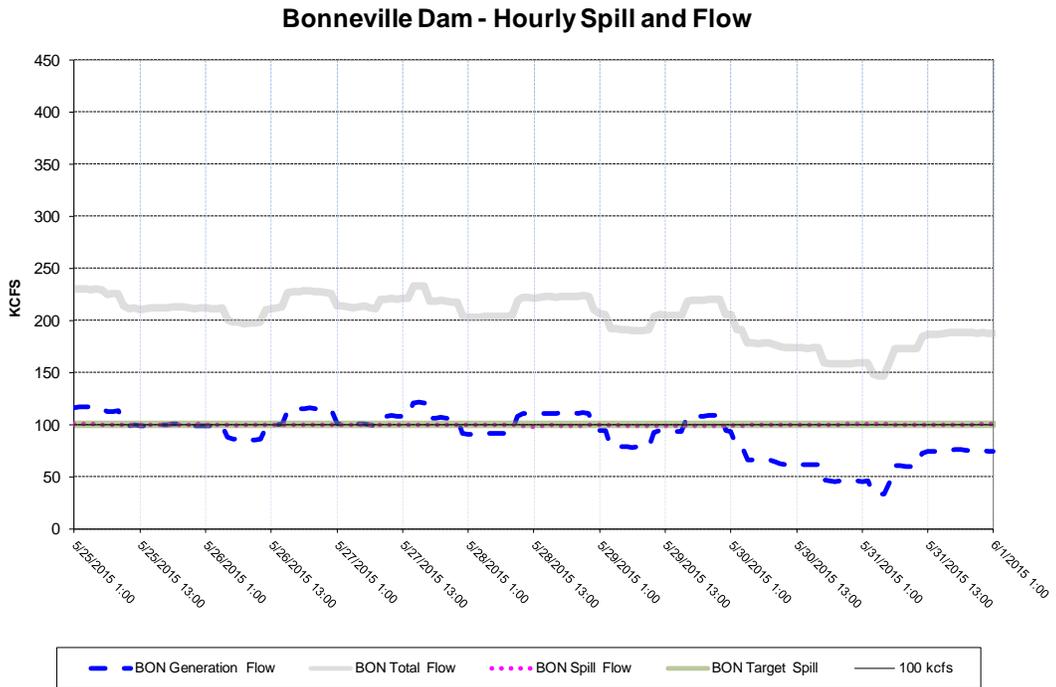
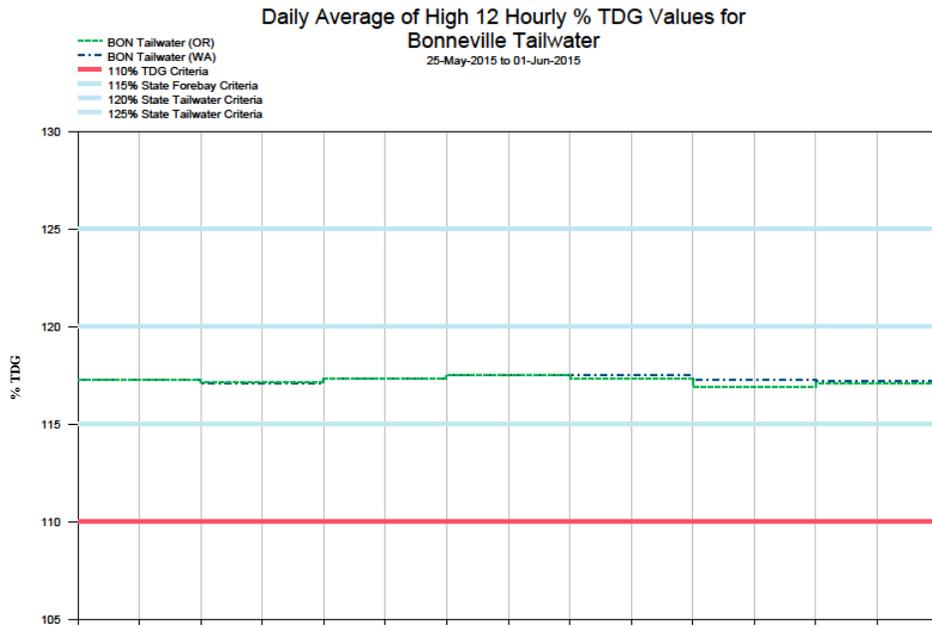


Table 1
Average Percent TDG Values For April 27 – May 31

Date	FIXED MONITORING STATIONS																			
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	IDSW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW	
	WA	WA	WA	WA	WA	WA	WA	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120
4/27/2015	101.4	111.4	110	112.2	111.3	117.9	116	114.1	109.4	115.7	115.9	108.3	112.8	113.3	111.2	116.1	116.1	112.6	116.9	116.9
4/28/2015	102.3	111.5	111.1	112.2	112	118.4	117.7	115.3	112.1	115.7	115.4	108.7	112.5	112.5	111.4	116	116	113.1	117.2	117.2
4/29/2015	102.3	111.5	111.1	111.9	111.9	117.3	117.9	113.9	112.1	116.4	116.3	106.7	111.9	111.9	109.9	113.8	115	112.8	117.1	117
4/30/2015	102.5	111.5	109.7	111.8	112.3	117.8	117.8	113.9	111.5	117.3	117.3	106.7	113.2	112.2	108.7	114.5	114.5	111.1	117.1	117.1
5/1/2015	104.8	111.4	110.7	112.5	112.9	118.5	118.1	114.6	111.8	116.3	117.3	108.6	113.6	113.3	112.4	116.9	116.9	111.9	117.1	117.2
5/2/2015	104.8	111.1	110.8	112.1	112.8	118	117.5	114.8	111.5	115.9	116	110.3	114.6	114.5	112.2	116.2	116.5	111.8	117	117.1
5/3/2015	103.5	110.5	110.8	112.5	112.6	117.7	117.4	114.9	111.9	115.6	115.6	111.3	114.6	114.6	112.3	117.2	117.2	113.8	116.5	116.5
5/4/2015	104.2	110.8	112.1	112.7	112.8	117.3	118.1	115	111.9	114.8	114.9	111.5	114.3	114.2	112.3	117	117.2	114.3	117.1	117.1
5/5/2015	104.1	110.7	112.1	112.4	112.6	117.1	117.9	115.4	111.9	114.1	114.1	110.4	113.8	112.2	111.3	115.4	115.9	112.6	116.1	116.7
5/6/2015	102.7	109.9	111.2	111.2	111.9	116.8	116.3	115.8	109.7	114.4	114.4	109.8	114.6	114.6	109.9	116	116	110.2	116.2	116.1
5/7/2015	102.6	109.9	110.7	110.9	111.6	117.2	114.5	115.7	109.4	115.6	115.6	110.2	114.7	114.7	110.9	116.6	116.6	111.9	116.2	116.2
5/8/2015	102.5	109.9	110.4	110.9	111.9	117.3	114.8	115.7	111.3	117.2	117.2	110.8	112	113.9	112.4	117.4	117.4	114.2	116.4	116.4
5/9/2015	102.4	110.3	109.8	111.7	111.9	117.3	115.1	115.6	112.9	116.9	117.2	110.9	112.6	112.5	112.9	117.9	117.9	115.6	117.1	117.1
5/10/2015	103.5	111	111.3	112.1	112.1	117.3	115.7	113.8	113.3	116.7	116.7	110.4	112.1	112.1	113.4	117.9	117.9	115.8	117.2	117.2
5/11/2015	104.1	111.3	111.5	112	112.4	117.2	116.4	113.5	113.8	116.5	116.6	110.4	111	111.6	113	115.6	117.5	115.3	117	117.1
5/12/2015	104.4	111.3	111	112	112.5	116.8	116.4	114	113	116	116.1	108.9	110.2	110.7	108.6	114.8	114.9	111	116.8	117
5/13/2015	104.4	111.2	109.9	111.8	112.7	116.3	116.3	113.9	112	114.3	114.7	109	113.7	113.6	109.4	116	116	109.4	116.4	116.3
5/14/2015	103.9	110.9	109.9	111.6	111.3	117.2	113.5	115	108.3	114.9	114.7	109.9	114.4	114.3	112.7	118.2	118.2	112.5	116.8	116.8
5/15/2015	103.5	110.6	110.2	111.6	111.2	117.1	113	114.4	108.3	114.2	114.3	110.1	114.3	114.4	112.7	117.1	118.1	113.5	117.1	117
5/16/2015	102.6	111	110	111.4	111.2	118	113.4	114.9	109.9	116.4	116.4	109.8	112.5	113.3	109.6	114.6	115.7	111.7	116.1	116.7
5/17/2015	102.8	109.8	109.1	110.9	110.8	118.1	113.6	115.5	109.8	116.9	116.9	107.7	110.3	110.1	110.2	115.8	115.8	109.6	116.6	116.5
5/18/2015	102.8	109.9	109.5	110.7	110.7	119	114.4	115.7	109.7	114.8	116.5	109	110.8	110.8	112.2	118	118	112.9	117.3	117.3
5/19/2015	103.1	110	109.7	110.9	112.2	118.9	115.8	115.4	111.9	114.8	114.6	109.5	113.6	112.6	111.7	116.8	117.7	113.3	117.1	117.3
5/20/2015	104.3	110.1	110.5	111.3	113	119.1	116.6	116	112.7	115.6	115.5	109.5	114.6	114.6	111.4	117.3	117.3	113.2	117.3	117.3
5/21/2015	105	110.5	110.6	111.2	113	118.6	117.7	116	113	114.8	114.8	109.5	115.4	115.4	112.9	118.6	118.6	114.8	117.6	117.6
5/22/2015	105.1	110.6	110.4	111	113.2	118.2	118	115.6	113.3	114.7	114.6	110.9	115.2	115.1	112.9	117.3	118.3	114.8	117.2	117.4
5/23/2015	104.4	110.2	109.9	111.5	113.1	114.4	117.7	115.6	112.2	114.5	114.5	110.9	115.4	115.4	109.4	115.2	115.9	111.5	117.1	117.1
5/24/2015	103.4	110.3	111.1	111.5	112.4	113.8	116.3	116	110.8	115.1	115.1	110.5	116.6	116.6	109.7	115.9	115.9	108.4	117.5	117.5
5/25/2015	103.5	110.2	111.3	111.4	112.4	113.7	115.7	115.9	110.9	114.8	114.8	110.2	115.4	116.2	110.3	116	115.9	109	117.5	117.5
5/26/2015	103.4	110.3	110.9	111.2	112.5	114.3	115.5	115.8	111	114.6	114.6	109.5	114.2	114.6	110.1	116.4	116.4	109.8	117.4	117.4
5/27/2015	103.3	110.4	110.2	111.1	112.2	116.3	115.2	115.7	110.4	114.8	114.8	108.6	113.4	112.2	110.9	116.6	116.6	112.3	117.6	117.5
5/28/2015	102.9	110.1	110.1	111.1	111.8	116.8	115	115.8	111	114.9	114.8	110.7	115.6	115.6	112.2	117.4	117.4	115	117.7	117.7
5/29/2015	103	110.3	111.6	111.6	112.3	117.8	116.4	115.8	113.3	115.6	115.6	111.7	115.5	115.5	113.5	118.5	118.5	115.5	117.6	117.7
5/30/2015	103.5	110.7	111.7	112.1	113	117.3	117.1	115.7	113.1	114.9	114.8	112.1	115.2	115.2	113.2	117.1	118.1	115.4	117.1	117.5
5/31/2015	104	110.5	112.2	112.3	113.6	117.5	117.5	116	113.2	115	115	112.9	116	116	112.3	116.9	116.9	113.9	117.3	117.4

Note: The Oregon TDG standard modification (OR) and the Washington TDG criteria adjustments (WA) have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard. TDG values are presented in Table 1 by displaying the highest value %TDG (more stringent), and the lower value is displayed with a strikethrough.

Total Dissolved Gas Monitoring Stations

Code	Station Name
LWG	Lower Granite Forebay
LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay
LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay
LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay
IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay
MCPW	McNary Tailwater
JDY	John Day Forebay
JHAW	John Day Tailwater
TDA	The Dalles Forebay
TDDO	The Dalles Tailwater
BON	Bonneville Forebay
CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal

FISH OPERATIONS PLAN IMPLEMENTATION REPORT

June 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' June 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in June 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in June displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

The weekly figures begin on June 1 and end on June 28 for the following lower Snake River and

¹ Averages reported are consistent with the current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and the Washington TDG criteria adjustments have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented from Monday through Sunday.

lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on June 1 for the lower Snake River and the lower Columbia River projects.

June 1 – June 7	Figures 1 – 8
June 8 – June 14	Figures 9 – 16
June 15 – June 21	Figures 17 – 24
June 22 – June 28	Figures 25 – 32

A. Upper Figure: Displays the daily average %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the observed percent TDG in the tailwater of the dam using the Oregon 120 %TDG standard calculated with the high 12-hour average.¹ Applies only to figures which include the lower Columbia dams.
2. The blue dot-dash line represents the observed percent TDG in the tailwater of the dam using the Washington 120 %TDG standard calculated with the high 12-hour average.¹³
3. The black solid line represents the observed percent TDG in the forebay of the next dam downstream using the Washington 115 %TDG standard calculated with the high 12-hour average.¹

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

³ From June 23 at 1000 through June 24 at 1000, the Lower Monumental tailwater percent TDG data was erroneous due to a ruptured membrane in the sensor. This erroneous data is evident in Figure 27 for the high 12-hour averages.

II. A table is included at the end of the figures that lists the daily average of high %TDG values for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects, tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the June 2015 Spill Variance Table.⁴ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour (except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams⁵, which may

⁴ Involuntary spill conditions appear in the figures, but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

⁵ As specified in the 2015 FOP (p. 14), this applies when the spill level is below 40% of total flow at The Dalles Dam.

range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

June 2015 Operations

The month of June was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the June 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 2.4 MAF (Million Acre Feet) or 39% of average as measured at Lower Granite Dam. For the lower Columbia, the Runoff Processor indicated the June 2015 adjusted volume runoff was below the 30 year average (1981-2010): 15.8 MAF or 61% of average as measured at The Dalles. The monthly precipitation summary for June was well below average at 32% on the Snake River above Ice Harbor Dam and also well below average on the Columbia River above The Dalles Dam at 44%.

During the June 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 20 kcfs, 24 hours/day through June 20. The operation transitioned to the summer hourly target spill level of 18 kcfs, 24 hours/day on June 21.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24

hours/day. Due to flow conditions, the operation transitioned to an hourly constant spill target⁶ of 11 kcfs, 24 hours/day on June 16, 9 kcfs, 24 hours/day on June 22, and then on June 23, to the variable 7/9/11 kcfs operation, depending on the previous day's outflow.

- Lower Monumental Dam - The hourly target spill level was the %TDG cap, 24 hours/day. The operation transitioned to the summer hourly target spill level of 17 kcfs, 24 hours/day on June 21.
- Ice Harbor Dam - The hourly target spill level alternated in 2-day blocks between 30% of total project outflow, 24 hours/day and 45 kcfs during the day and the %TDG cap during the nighttime spill hours (1800-0500).⁷
- McNary Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day. The operation transitioned to the summer hourly target spill level of 50%, 24 hours/day on June 16.
- John Day Dam - The hourly target spill level alternated in 2-day blocks between 40% and 30% of total project outflow, 24 hours/day⁸. Spill level changes occurred at 2000 hours.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level was 100 kcfs, 24 hours/day. The operation transitioned to the summer hourly target spill level alternating in 2-day blocks between 95 kcfs, 24 hours/day vs. 85 kcfs during the day and 121 kcfs during the nighttime on June 16.

Operational Adjustments

No Operational Adjustments to report.

⁶ Low flow operations for Little Goose Dam are described in the 2015 FOP (see p. 6). This operation was coordinated with TMT via email on June 16 and discussed during TMT meetings on June 17, 24, and 25.

⁷ In accordance with the 2015 FOP (see p. 12), the Ice Harbor spill operation on June 27 was changed from 45 kcfs day/TDG cap night to 30% of total project outflow during a period of higher power demand. This operation was discontinued on July 3, with the resumption of the alternating 2-day block operation (30% to 45 kcfs day/TDG cap at night).

⁸ In accordance with the 2015 FOP (see p. 12), on June 24 and June 28, the John Day spill operation was changed from 40% to 30% during a period of higher power demand. On June 30 and July 4, the within week changes to operations were from 30% to 40%.

June 2015 Spill Variance Table

Project	Parameter	Date	Time ⁹	Hours	Type	Reason
Little Goose	Reduced Spill	6/8/15	0800	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.8%.
Little Goose	Reduced Spill	6/11/15	0300	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.9%.
Little Goose	Reduced Spill	6/12/15	0700	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.9%.
Little Goose	Reduced Spill	6/14/15	0400	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock. 24 hr avg. spill was 29.9%.
Little Goose	Reduced Spill	6/15/15	1000-1300	4	Operational Limitation	Hourly spill decreased to 26.5, 27.4; 27.4, 27.4 % (below 30.0% ±1% range). Percent spill fluctuated due to low inflows and physical limits of spill gate settings. See p. 3 of FOP. 24 hr avg. spill was 29.4%.
Lower Monumental	Reduced Spill	6/1/15	1700-1800	2	Navigation	Hourly spill decreased to 12.2 and 18.5 kcfs (below 23 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/3/15	1700-1800	2	Navigation	Hourly spill decreased to 14.3 and 19.1 kcfs (below 23 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/5/15	1800-1900	2	Navigation	Hourly spill decreased to 16.4 and 21.7 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/7/15	1800	1	Navigation	Hourly spill decreased to 14.0 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/8/15	0400	1	Navigation	Hourly spill decreased to 20.9 kcfs (below 24 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/9/15	1800-1900	2	Navigation	Hourly spill decreased to 14.2 kcfs and 15.5 (below 20 kcfs ±2 kcfs range). Reduced spill for safe passage of fish barge.

⁹ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Project	Parameter	Date	Time⁹	Hours	Type	Reason
Lower Monumental	Reduced Spill	6/11/15	1700-1800	2	Navigation	Hourly spill decreased to 10.8 kcfs and 15.3 kcfs (below 20 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/13/15	1800-1900	2	Navigation	Hourly spill decreased to 13.9 kcfs and 17.4 kcfs (below 20 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/21/15	1700-1800	2	Navigation	Hourly spill decreased to 11.6 kcfs and 13.9 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/23/15	1800-1900	2	Navigation	Hourly spill decreased to 9.7 kcfs and 14.0 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/25/15	1700-1800	2	Navigation	Hourly spill decreased to 10.3 kcfs and 12.5 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	6/27/15	2300-2400	2	Navigation	Hourly spill decreased to 11.3 kcfs and 14.6 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Ice Harbor	Reduced Spill	6/13/15	1000	1	Navigation	Hourly spill decreased to 28.6% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/14/15	0200	1	Navigation	Hourly spill decreased to 28.5% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/14/15	0700	1	Operational Limitation	Hourly spill decreased to 25% (below 30.0% \pm 1% range). Percent spill fluctuated due to low inflows and physical limits of spill gate settings. See p. 3 of FOP.
Ice Harbor	Reduced Spill	6/17/15	2200	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/18/15	0900	1	Navigation	Hourly spill decreased to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/22/15	0000	1	Navigation	Hourly spill decreased to 28.7% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/22/15	0600	1	Navigation	Hourly spill decreased to 28.9% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.

Project	Parameter	Date	Time⁹	Hours	Type	Reason
Ice Harbor	Reduced Spill	6/22/15	1600	1	Navigation	Hourly spill decreased to 28.3% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock
Ice Harbor	Reduced Spill	6/23/15	0800-1000	3	Maintenance	Hourly spill remained at 11.6 kcfs while generation increased to 11.5 kcfs (above 8.2 to 10.0 kcfs minimum generation range for units 1 and 2) due to switching units for fish screen maintenance.
Ice Harbor	Reduced Spill	6/25/15	1100	1	Navigation	Hourly spill decreased to 28.5% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/25/15	2100-2200	2	Navigation	Hourly spill decreased to 28.6% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/26/15	0500	1	Navigation	Hourly spill decreased to 28.5% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/26/15	0900	1	Navigation	Hourly spill decreased to 28.5% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/26/15	1500	1	Navigation	Hourly spill decreased to 28.6% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/27/15	0500	1	Navigation	Hourly spill decreased to 28.6% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/27/15	1600	1	Navigation	Hourly spill decreased to 28.5% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/27/15	2200	1	Navigation	Hourly spill decreased to 28.7% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	6/28/15	1200	1	Navigation	Hourly spill decreased to 28.6% (below 30.0% ±1% range) due to volume of water needed to empty the navigation lock.

Figure 1

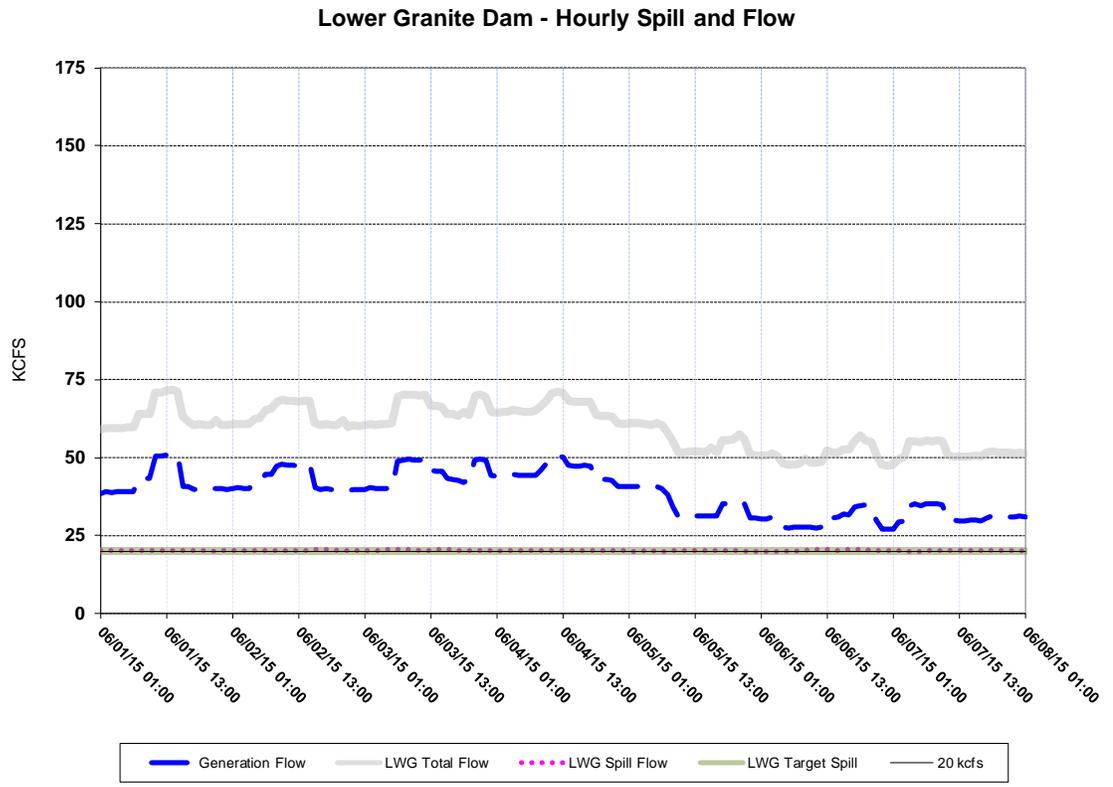
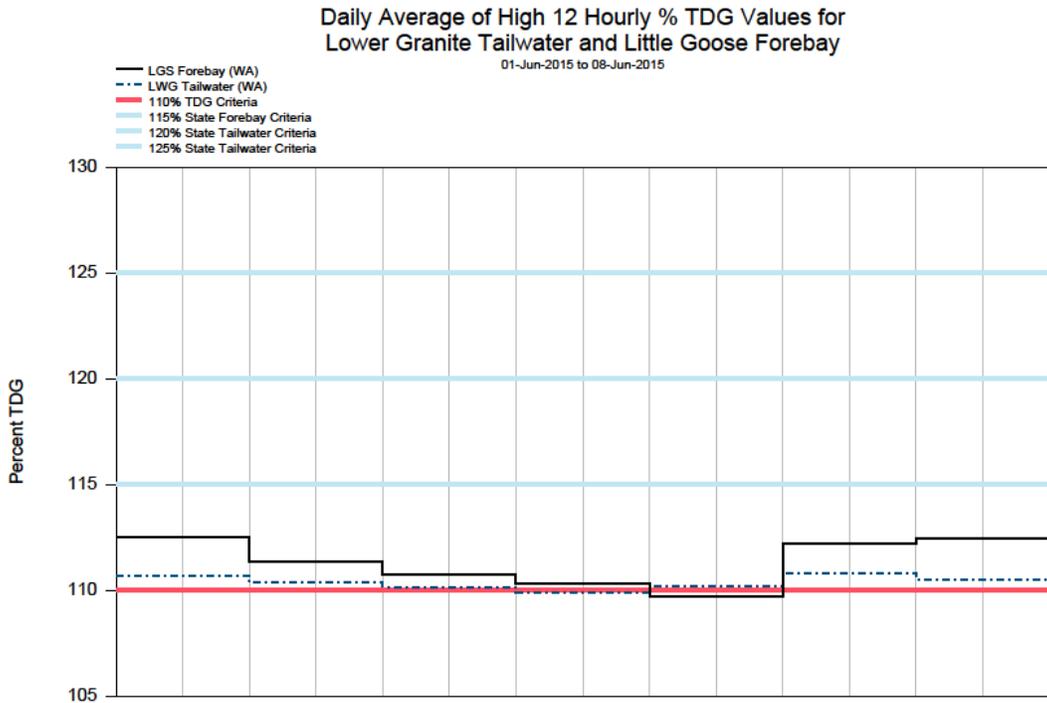


Figure 2

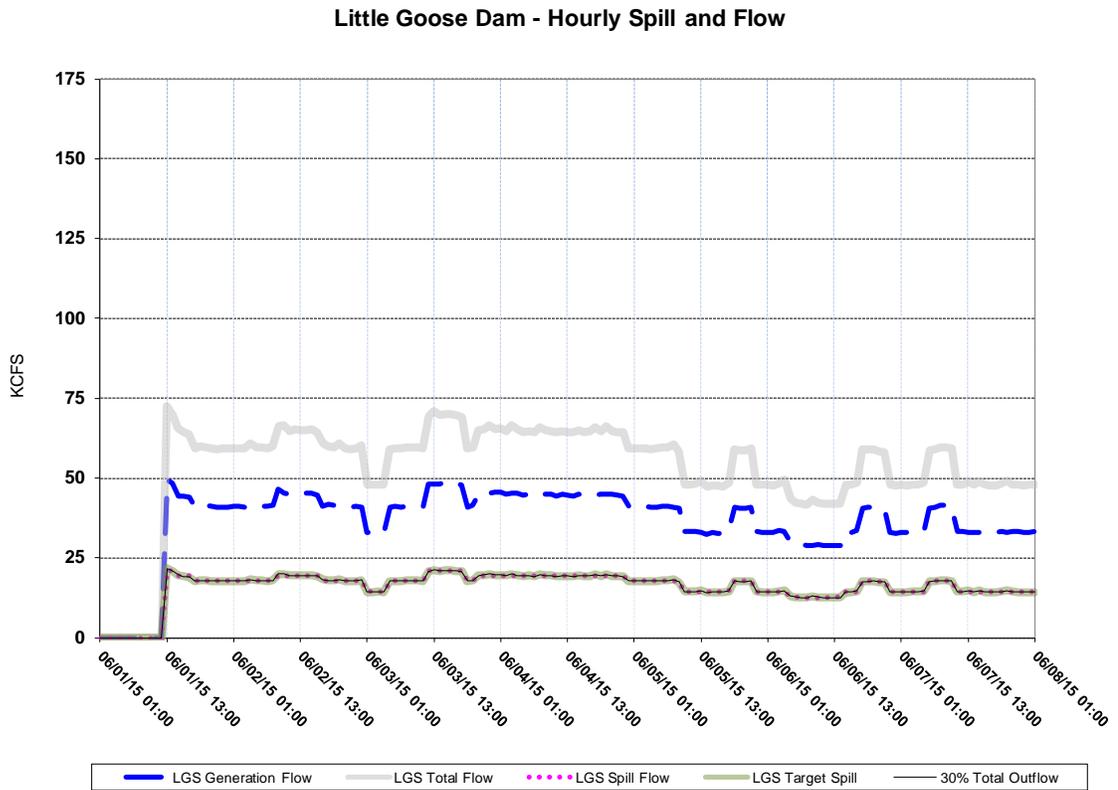
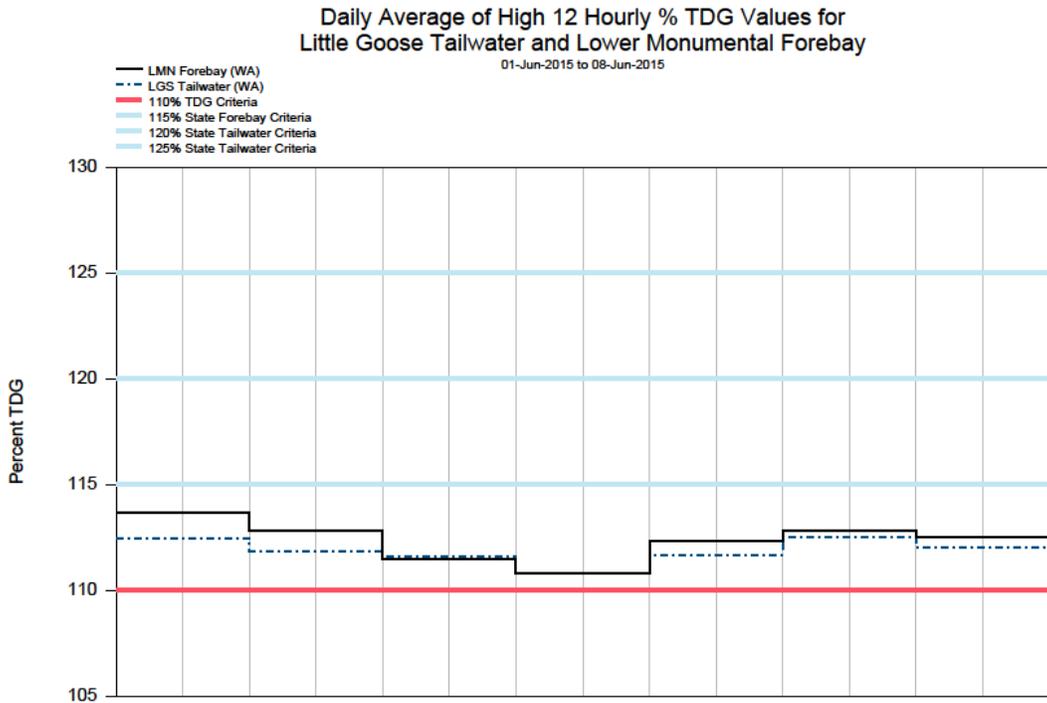


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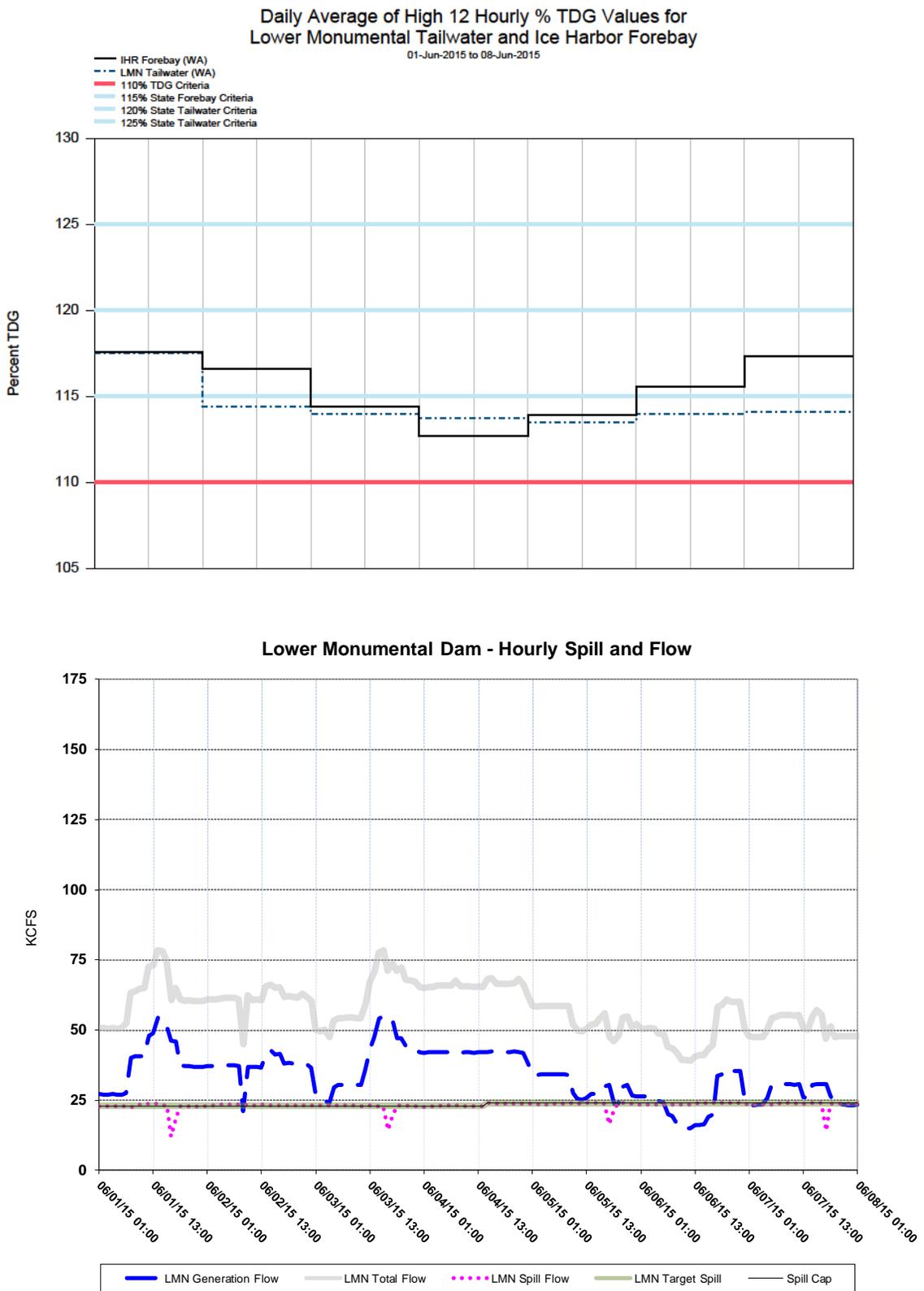


Figure 4

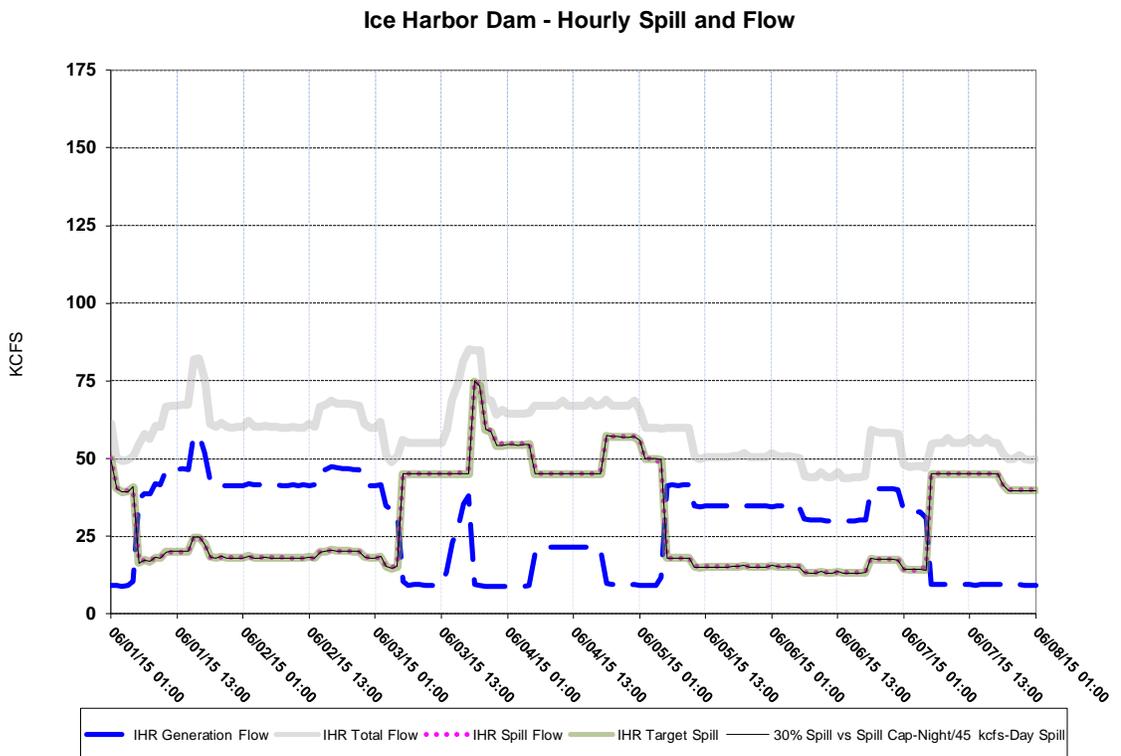
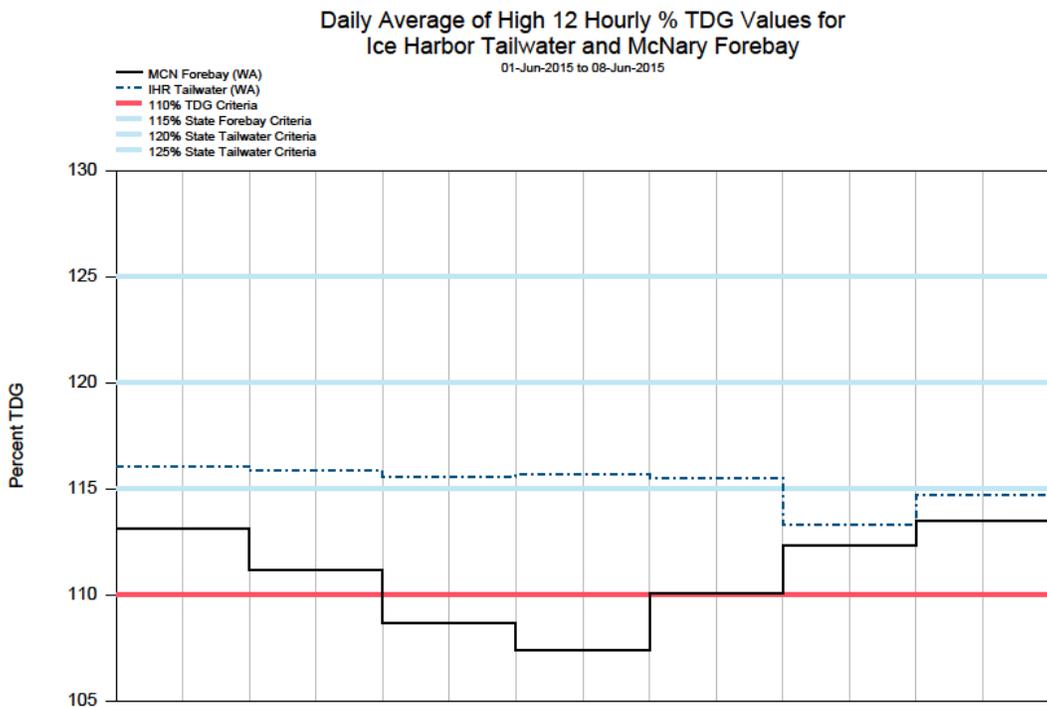


Figure 5

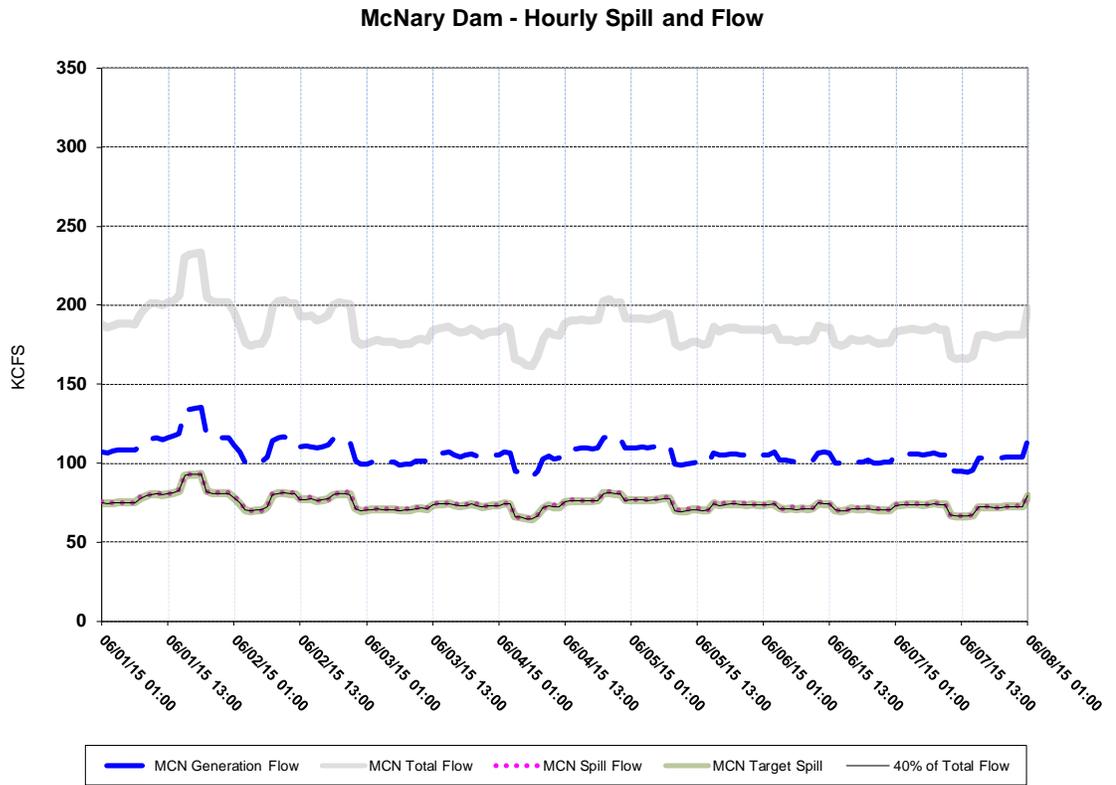
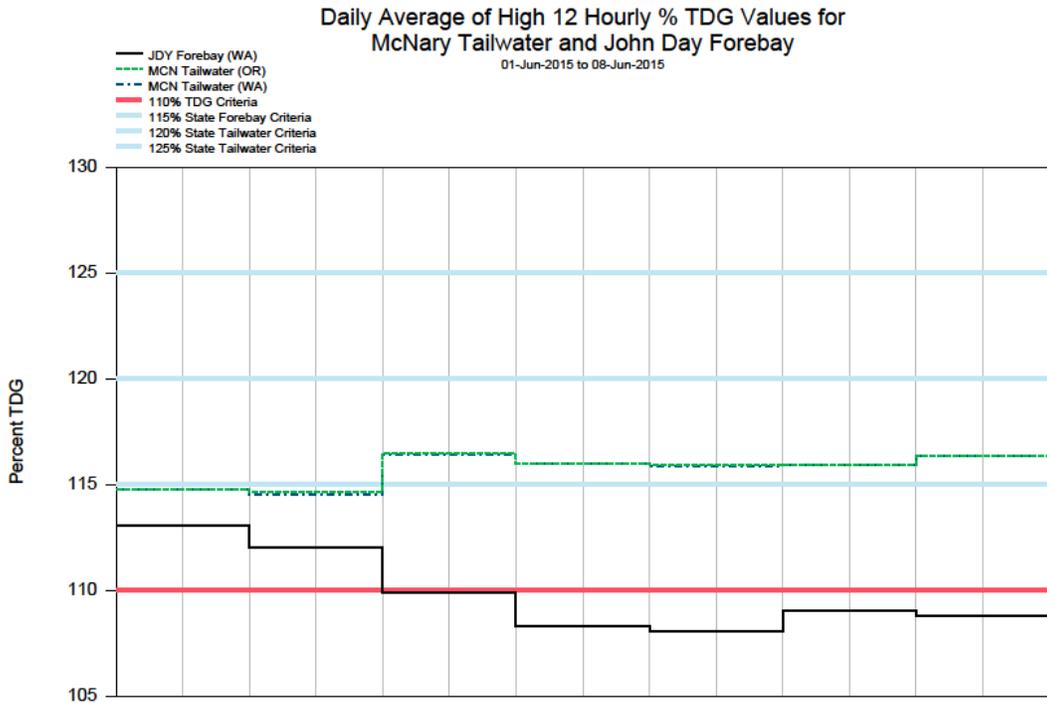


Figure 6

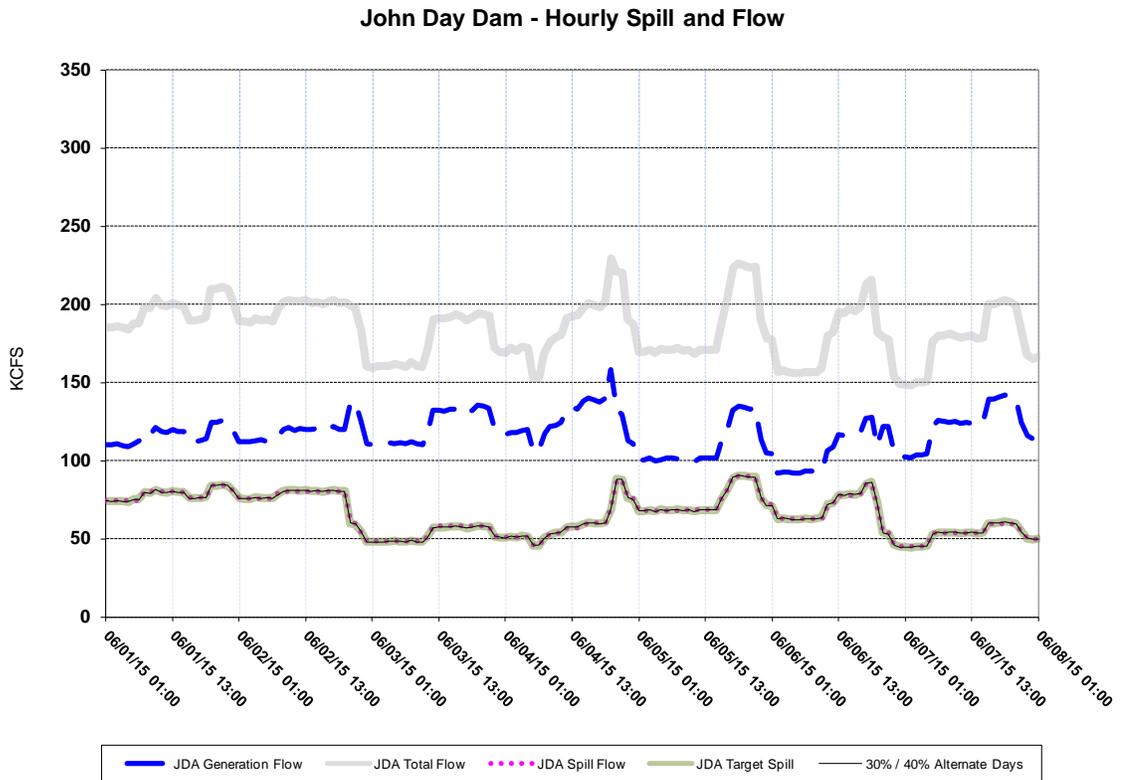
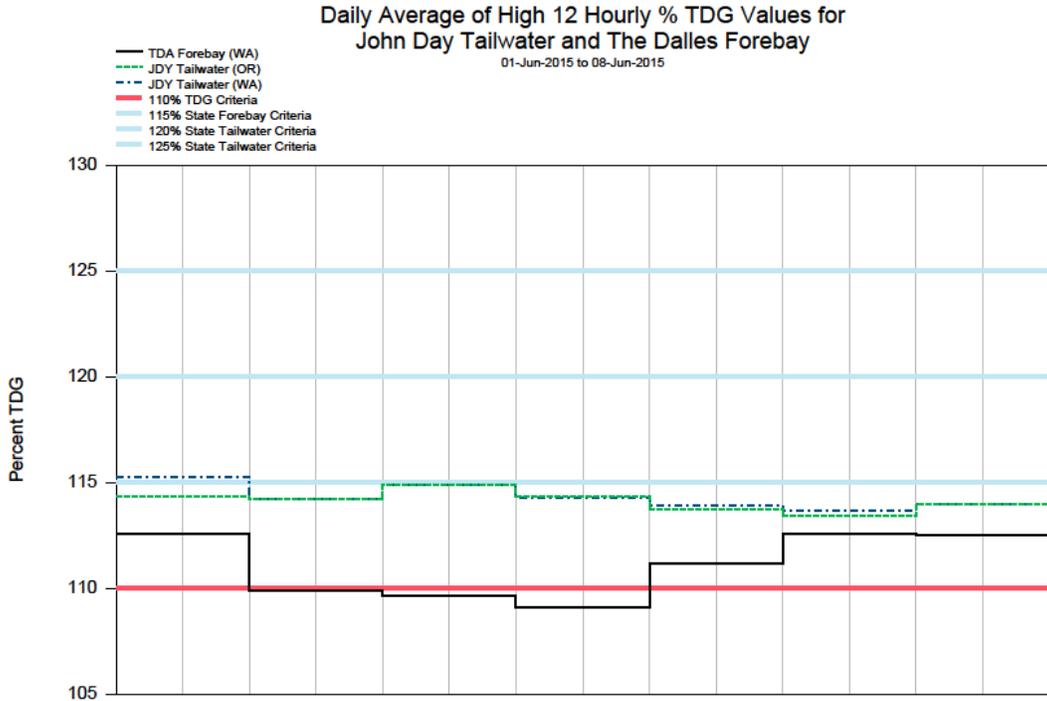


Figure 7

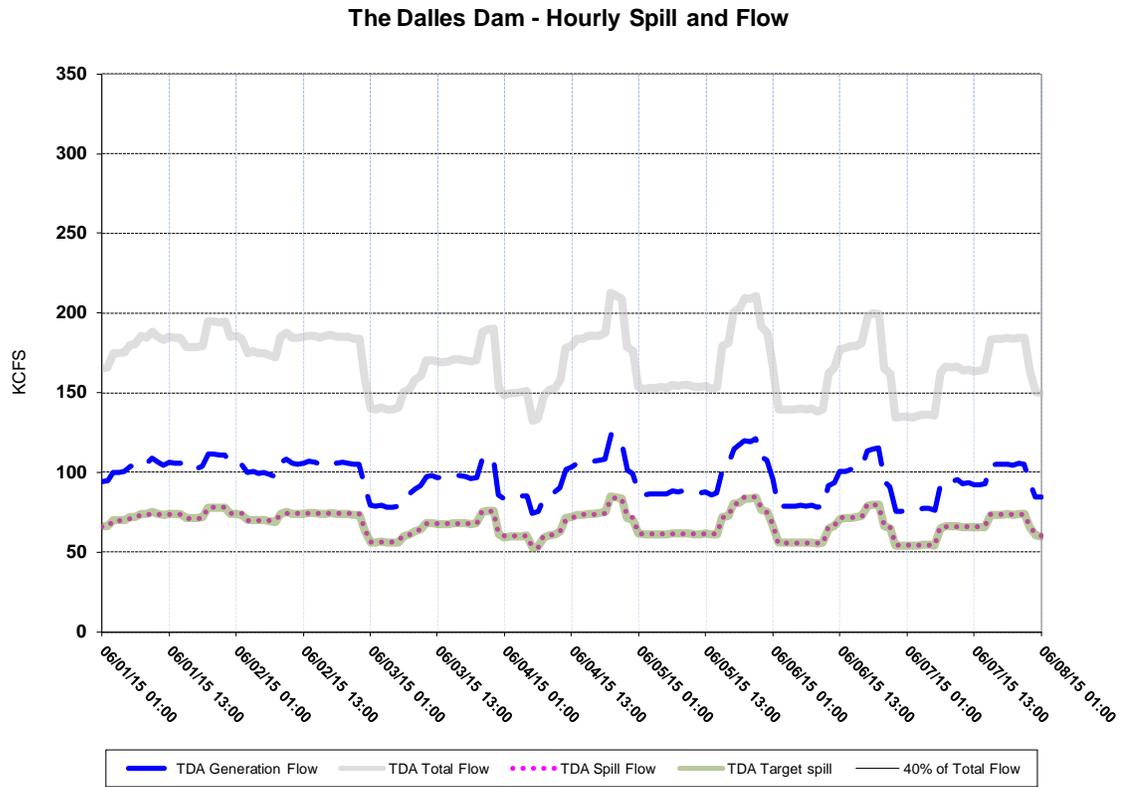
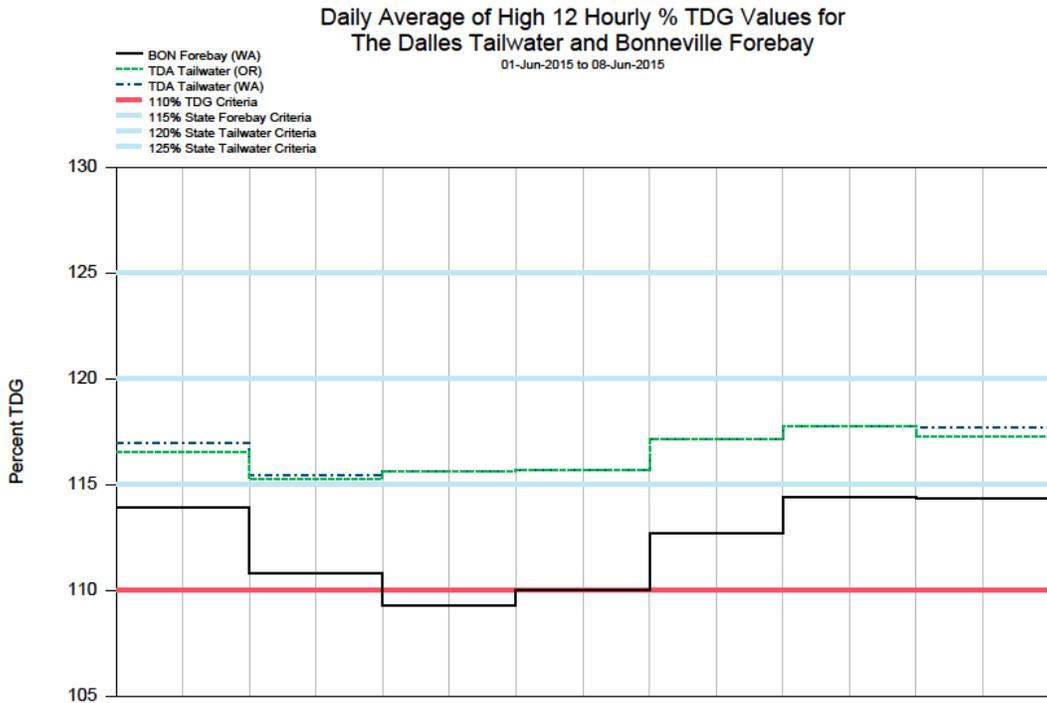


Figure 8

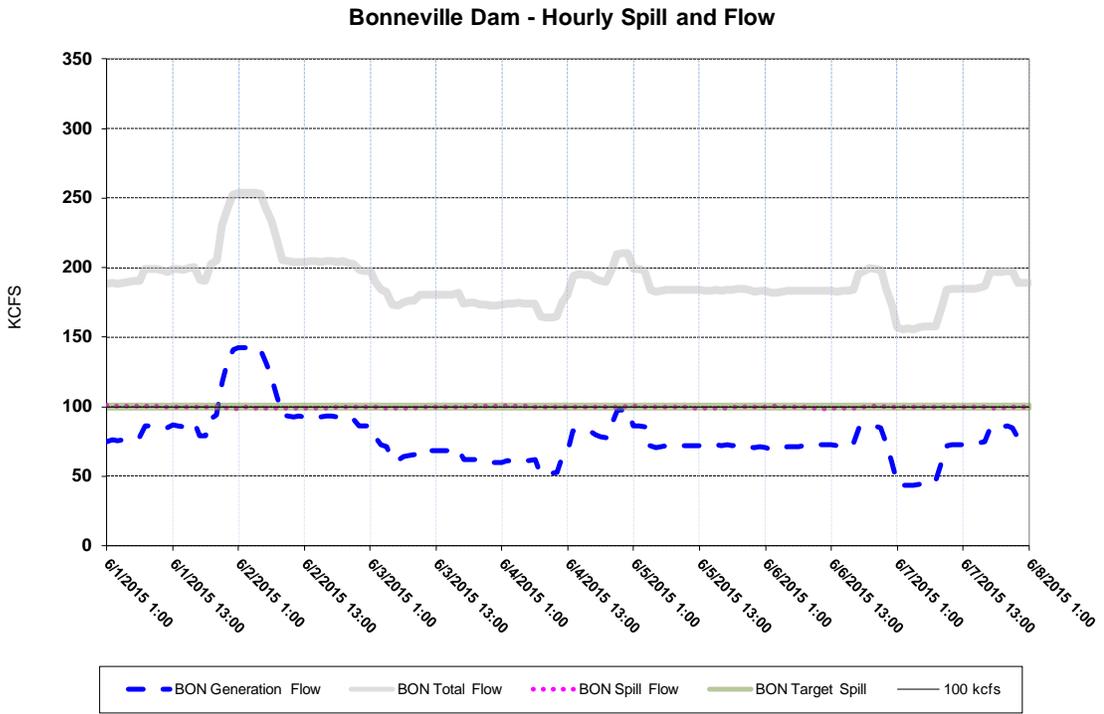
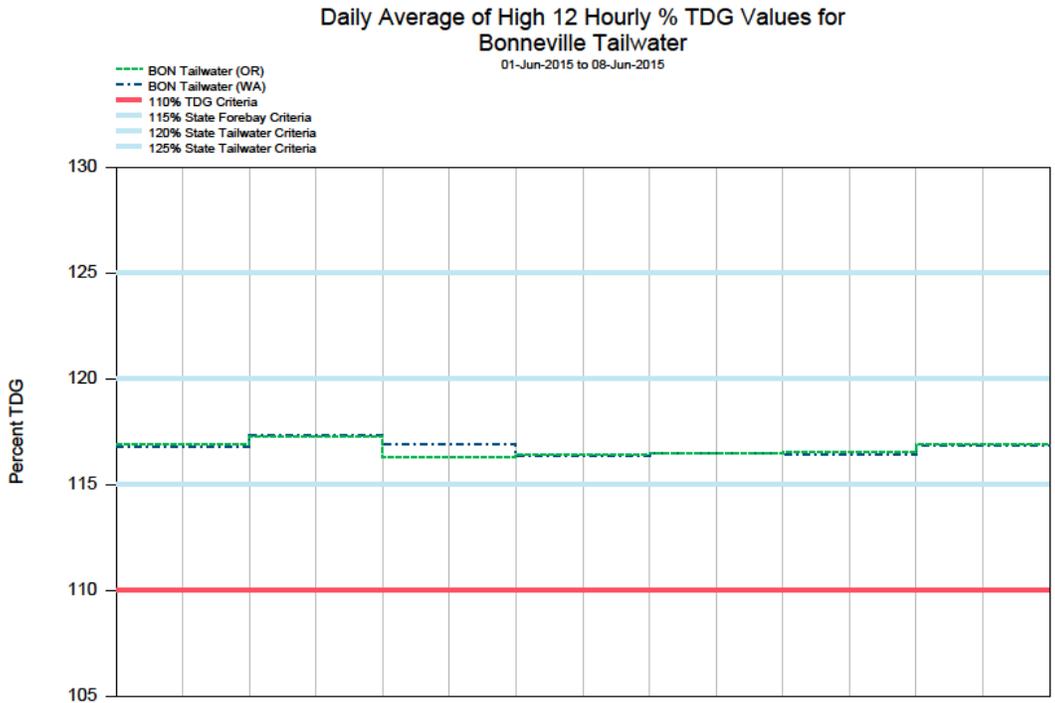


Figure 9

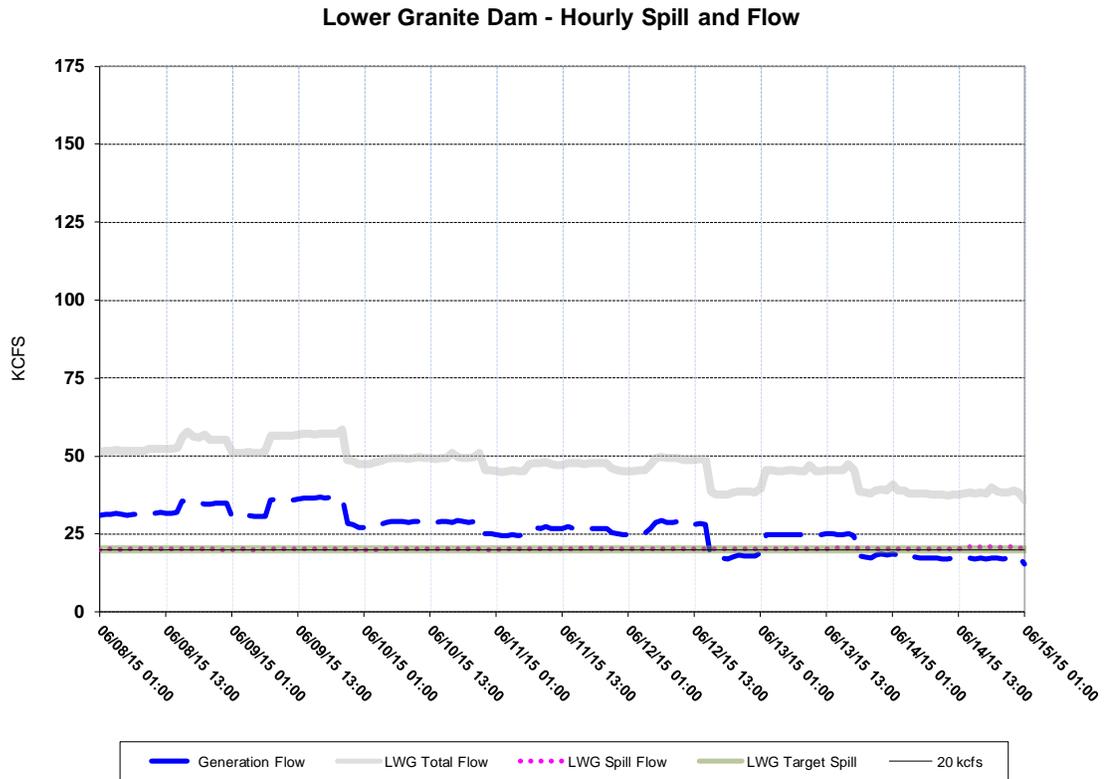
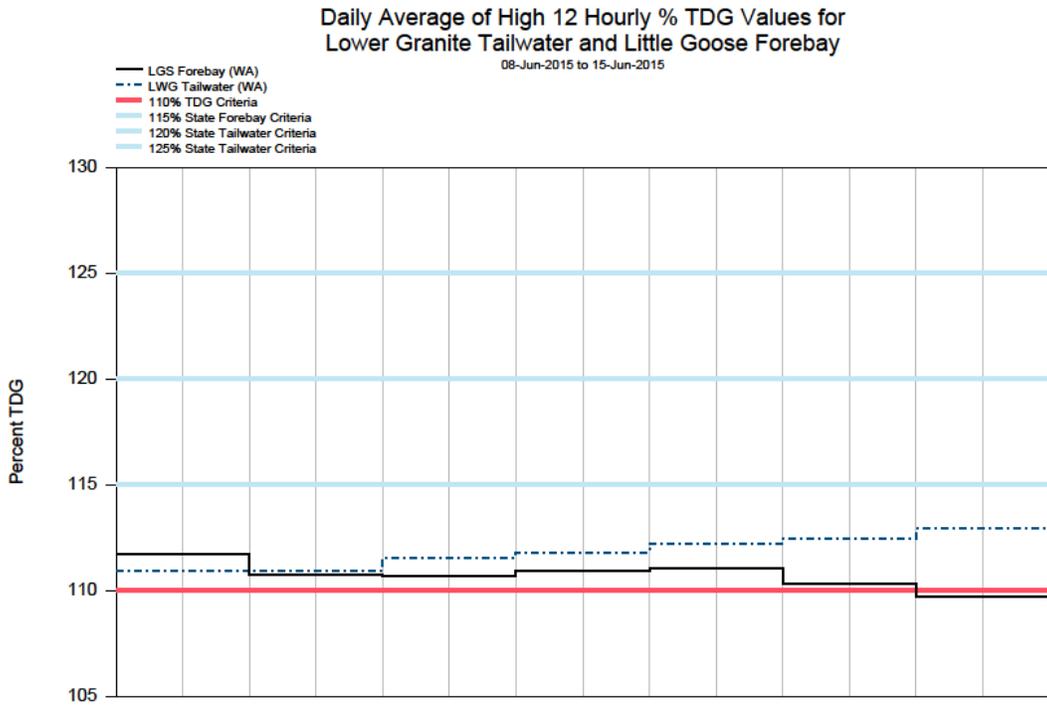


Figure 10

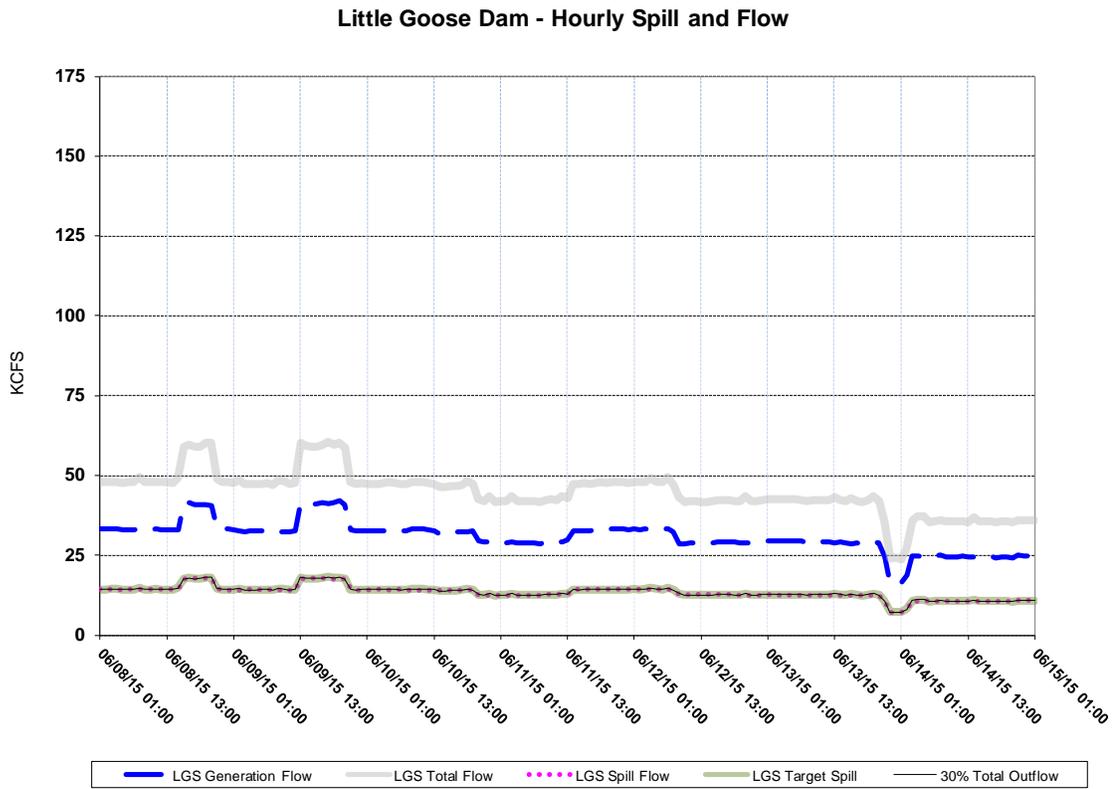
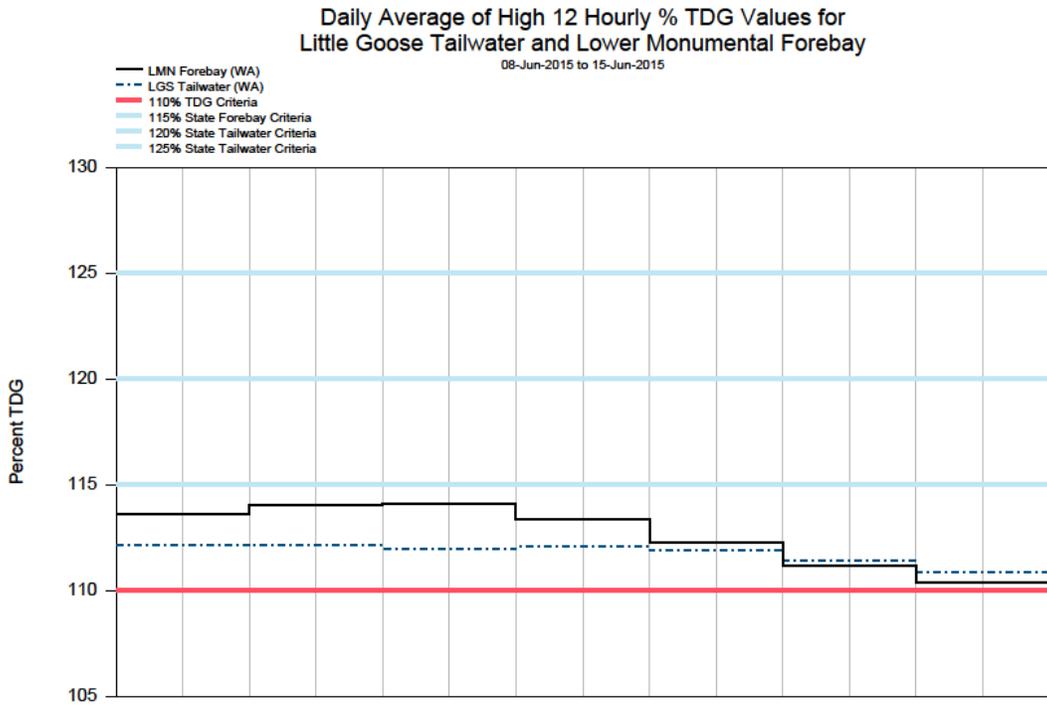


Figure 11

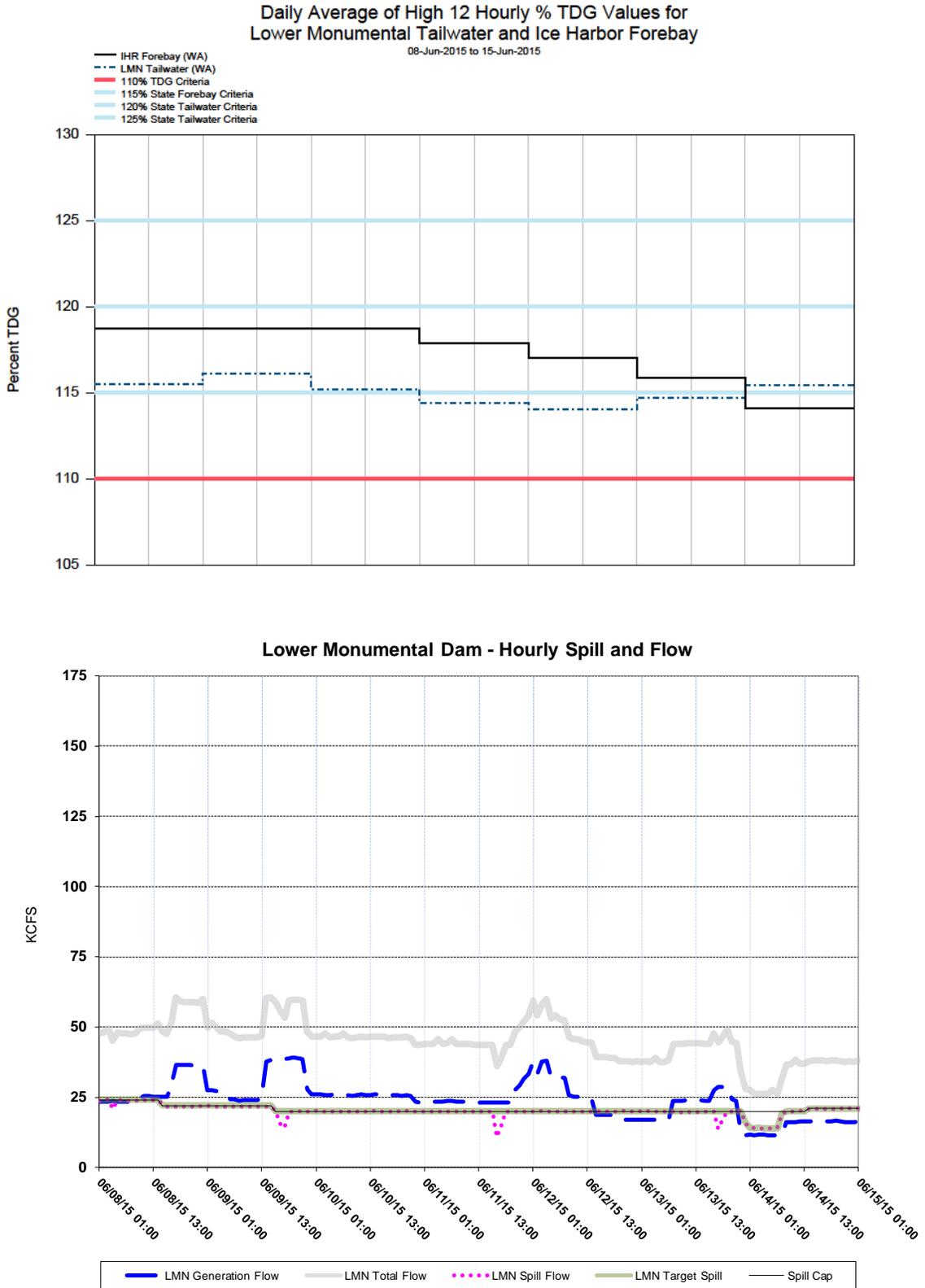


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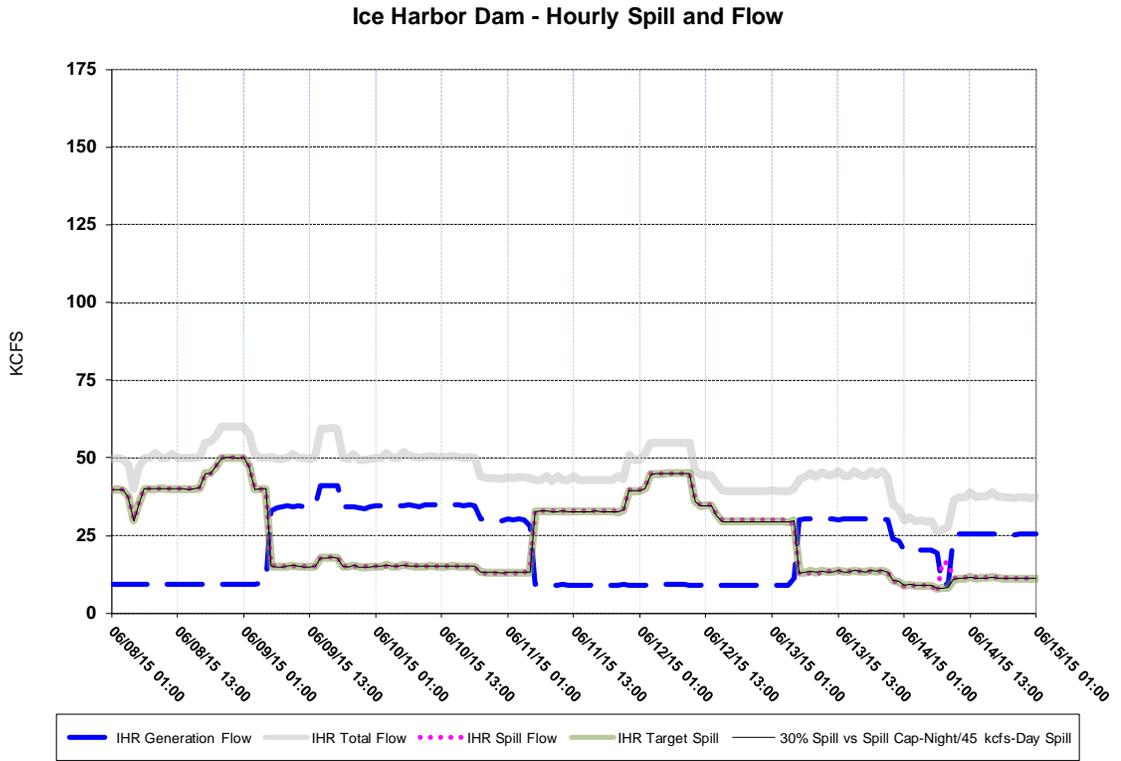
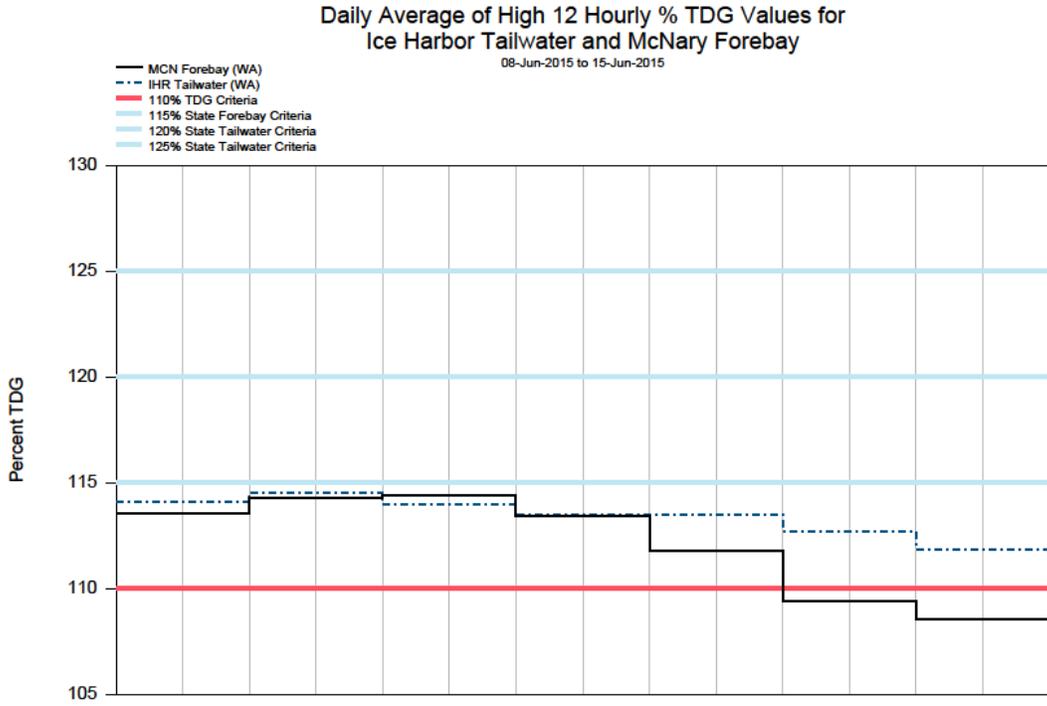


Figure 13

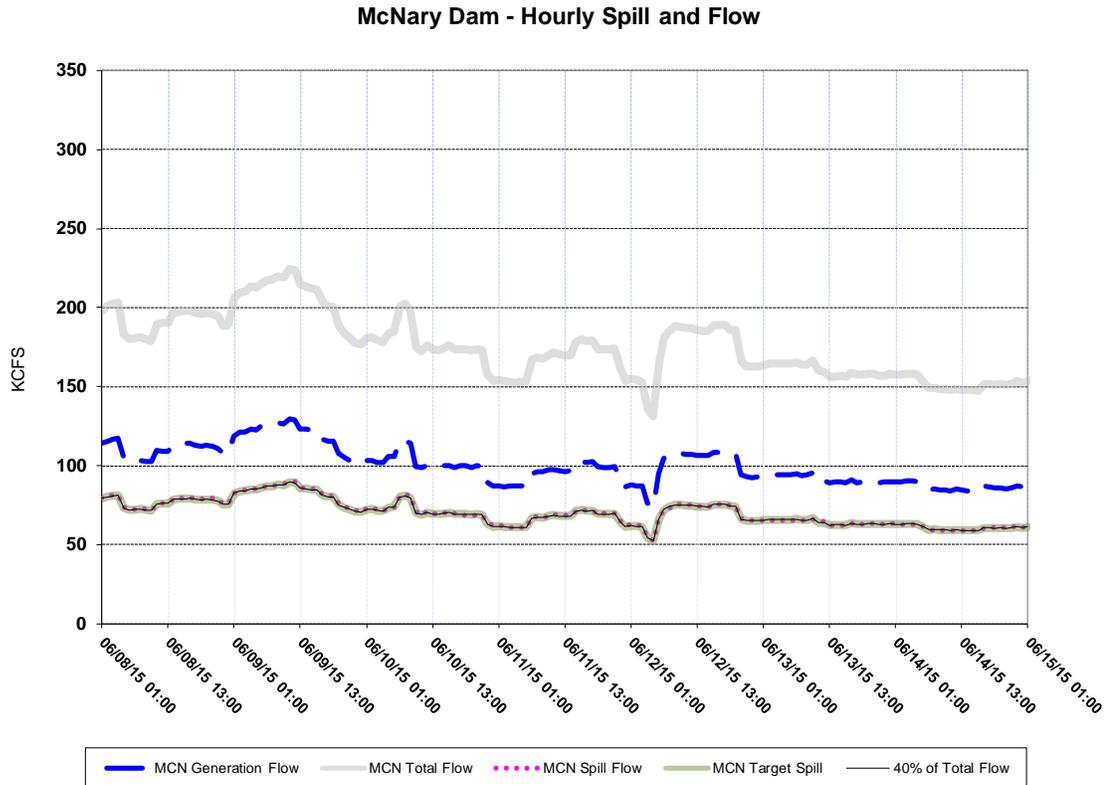
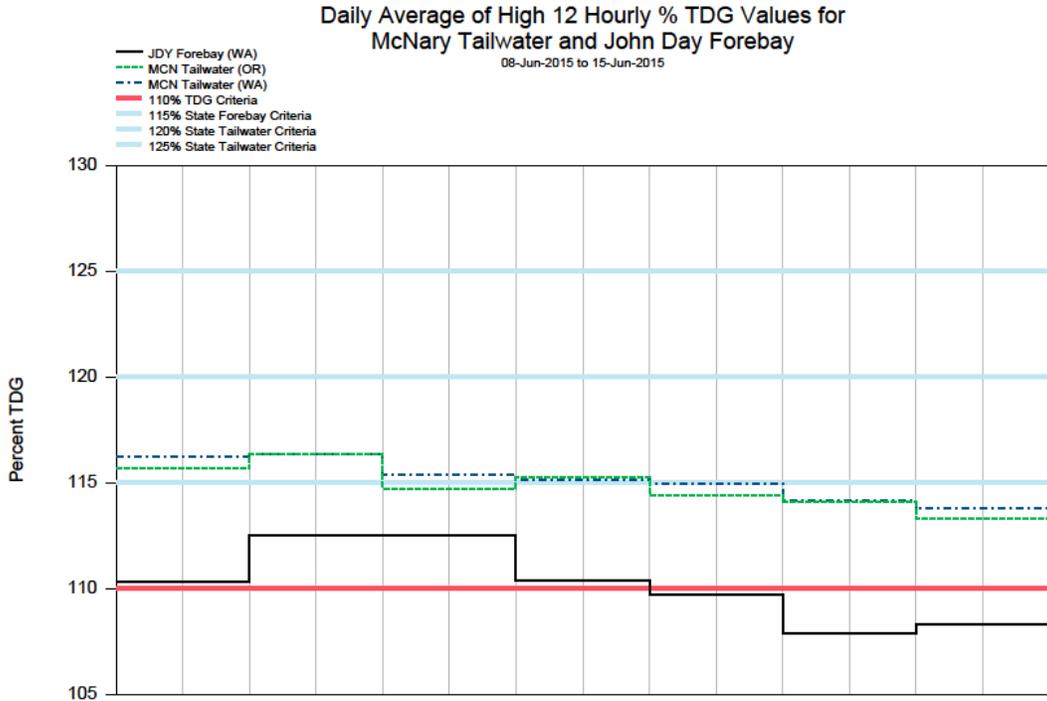


Figure 14

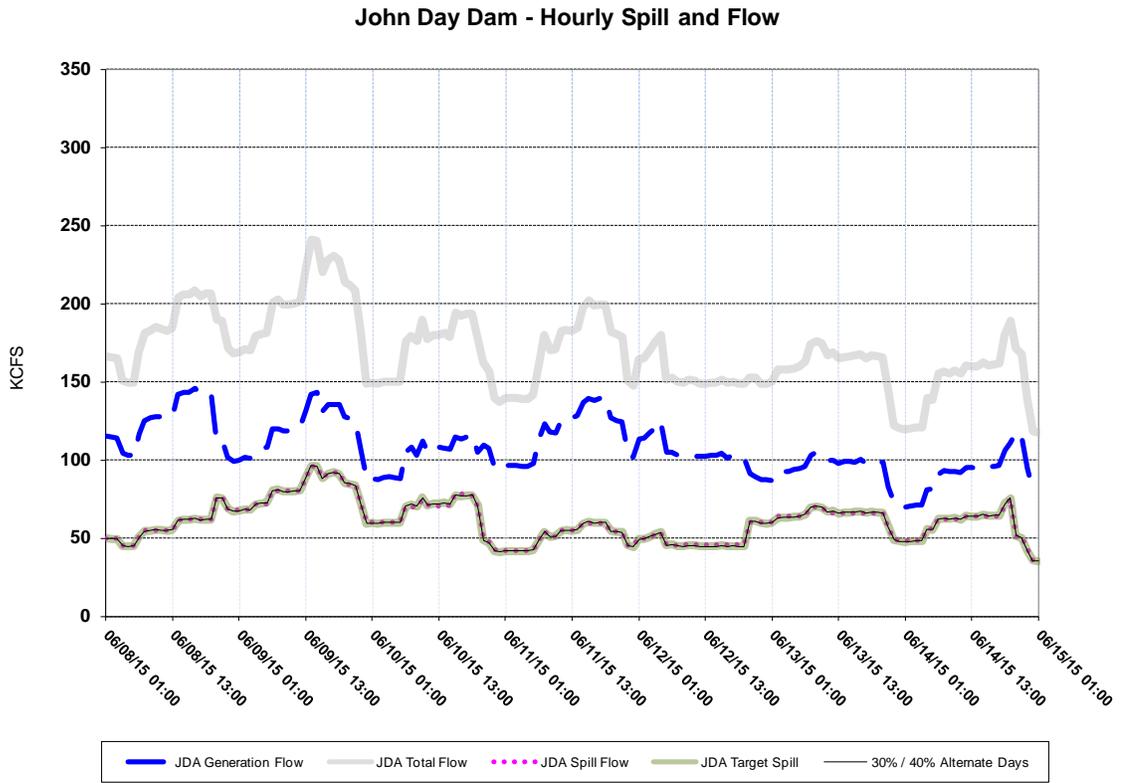
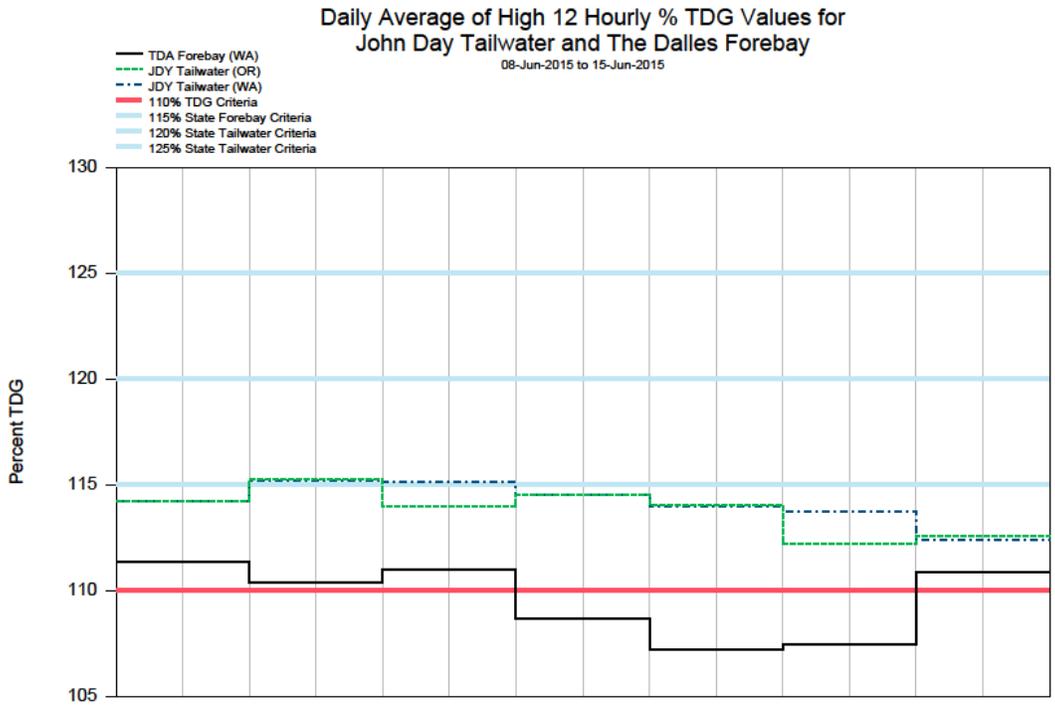
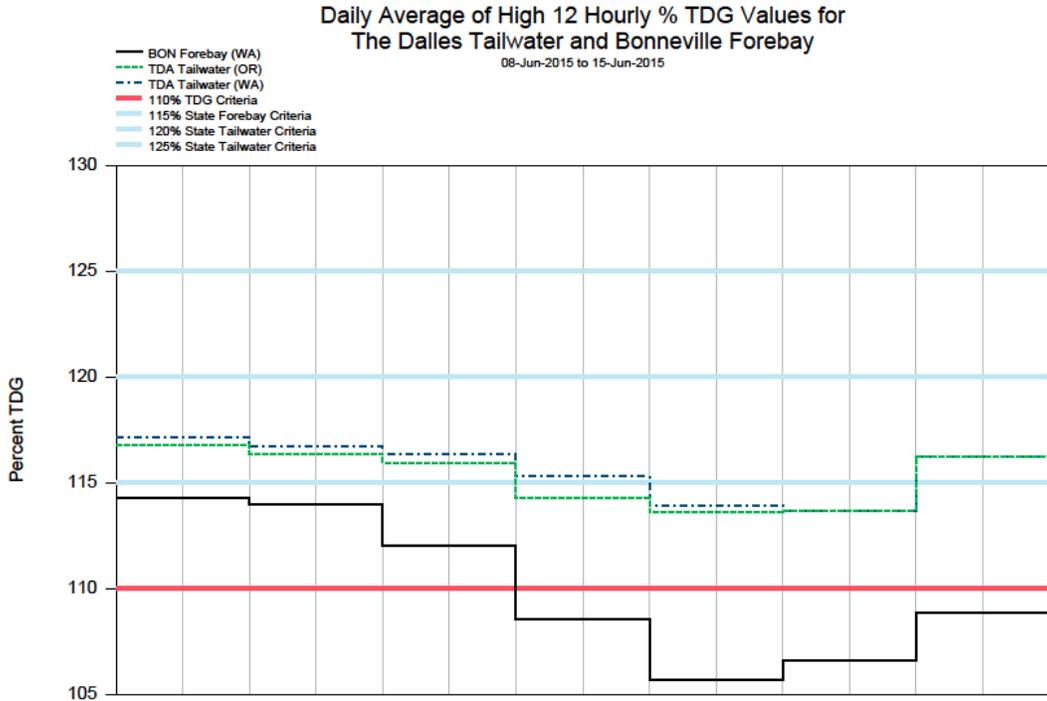


Figure 15



The Dalles Dam - Hourly Spill and Flow

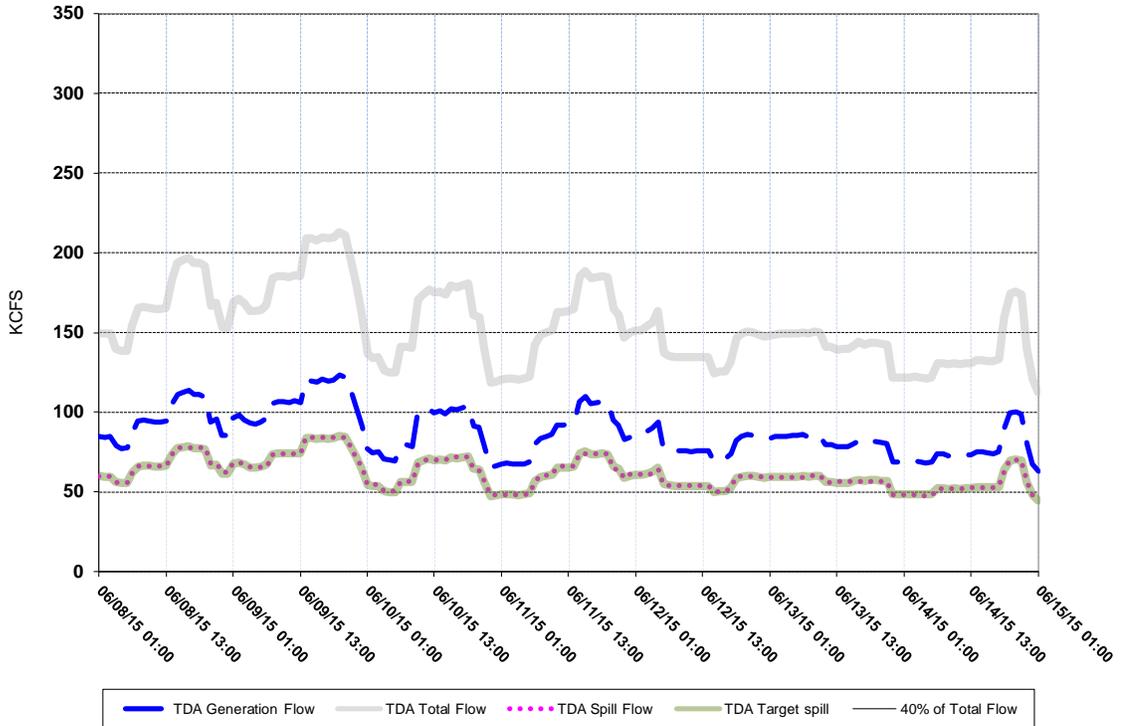


Figure 16

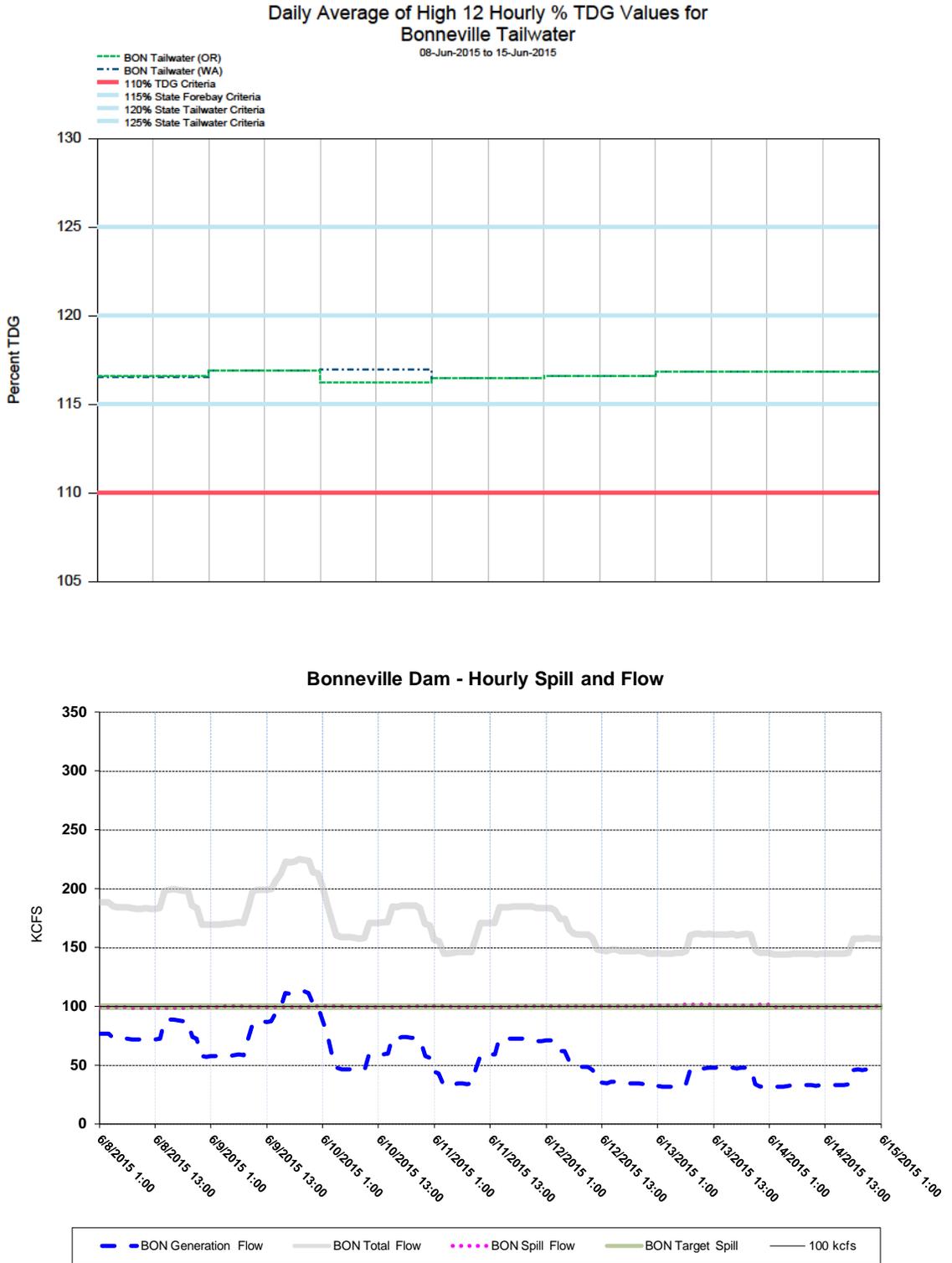


Figure 17

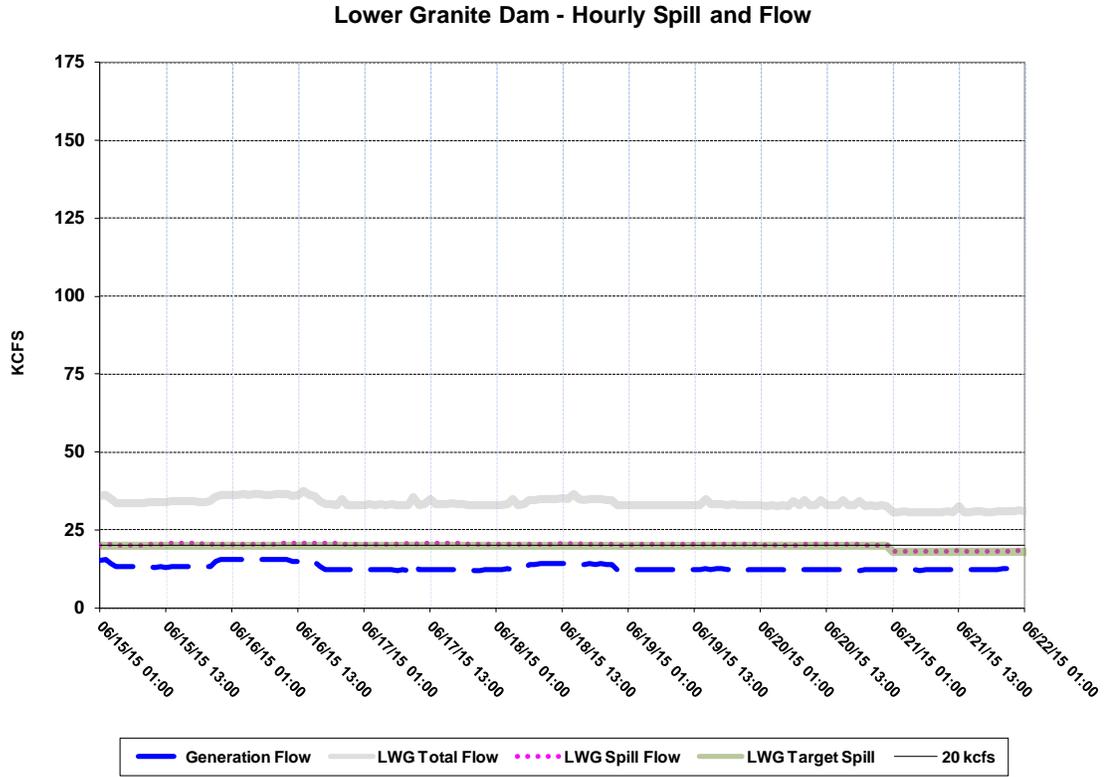
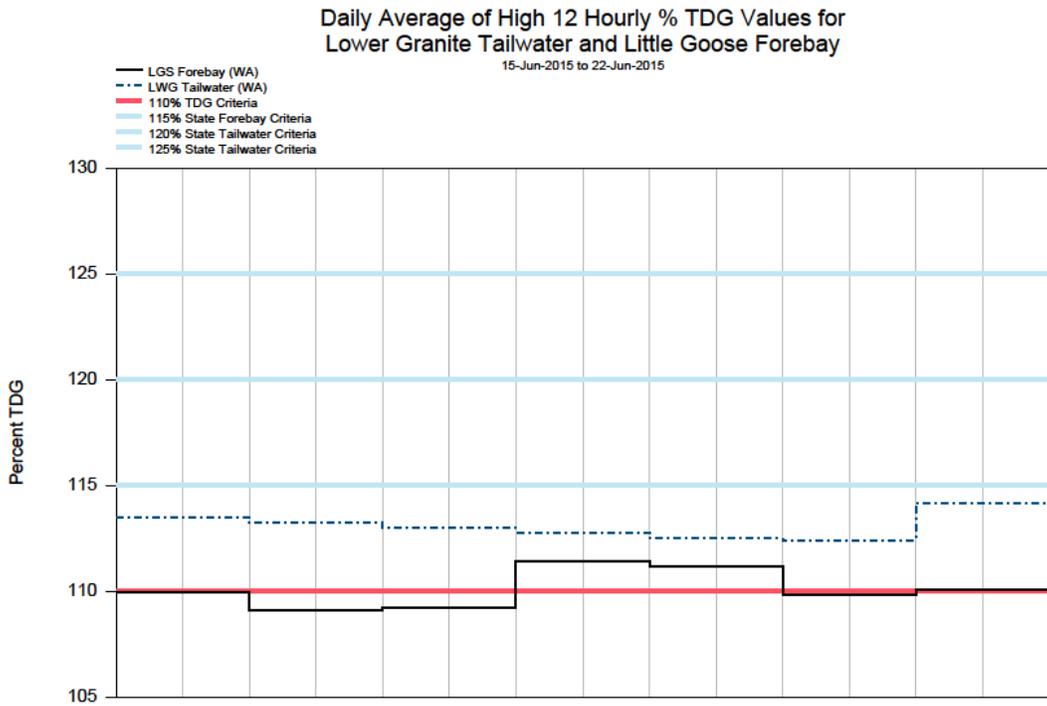


Figure 18

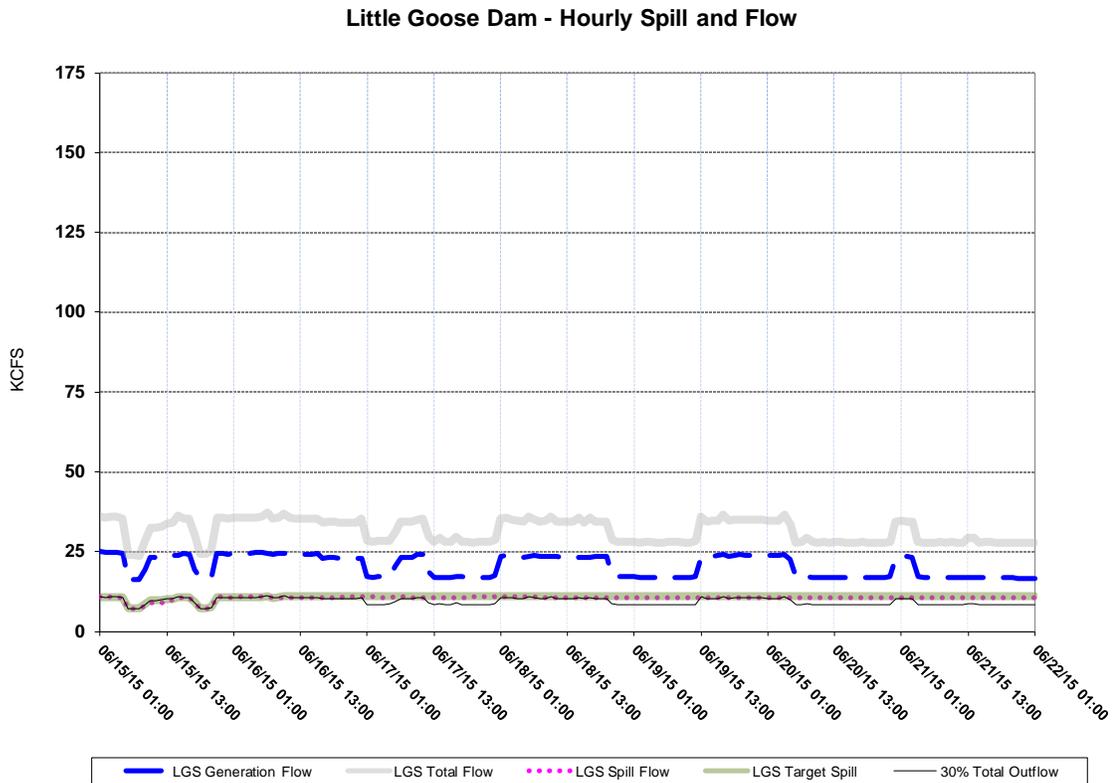
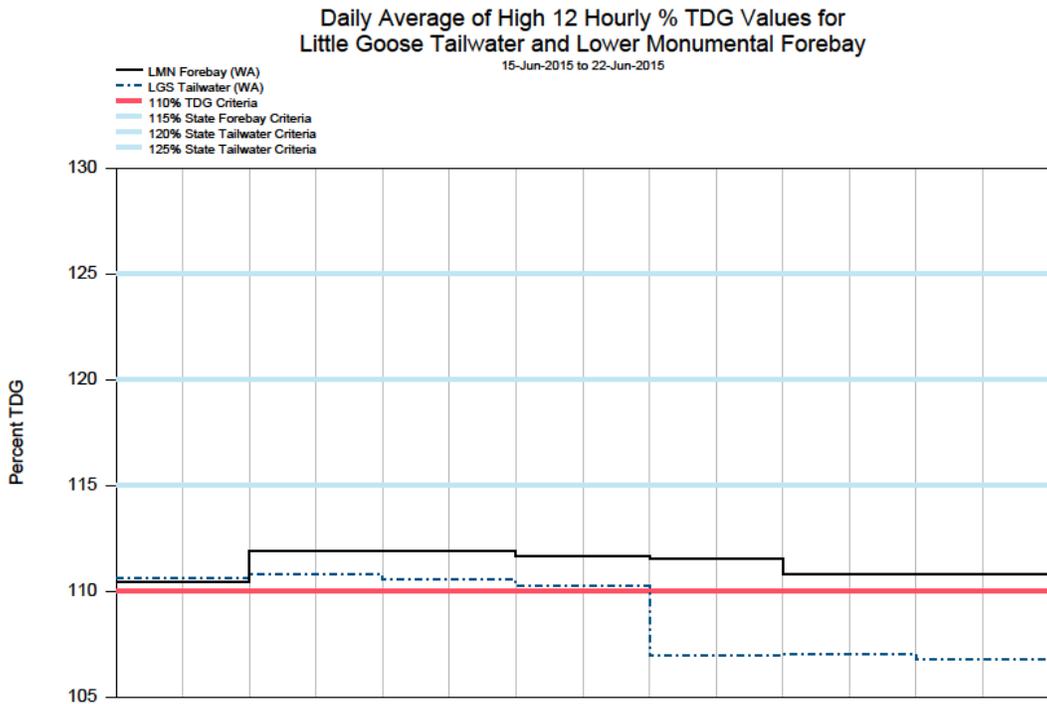


Figure 19

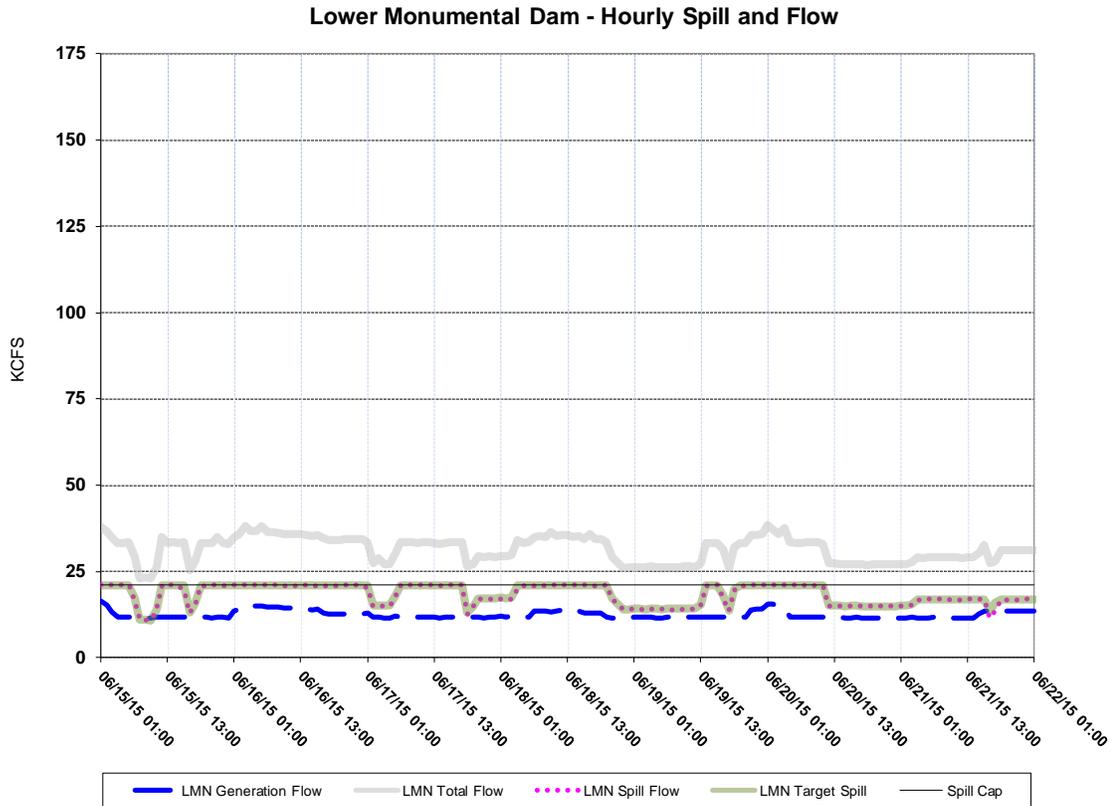
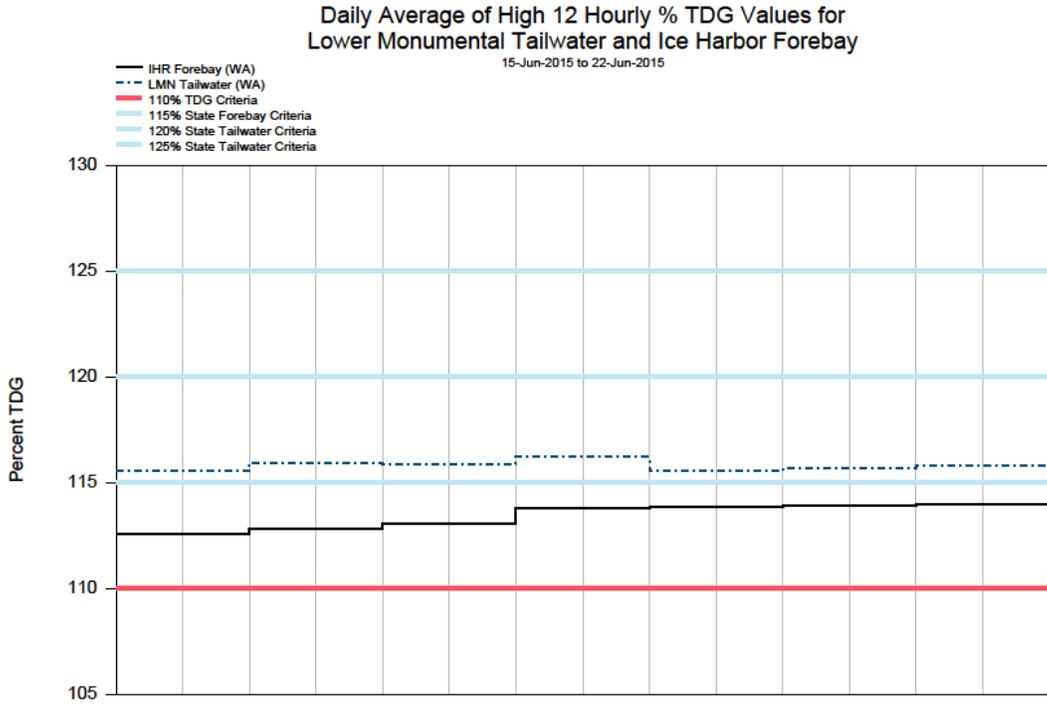


Figure 20

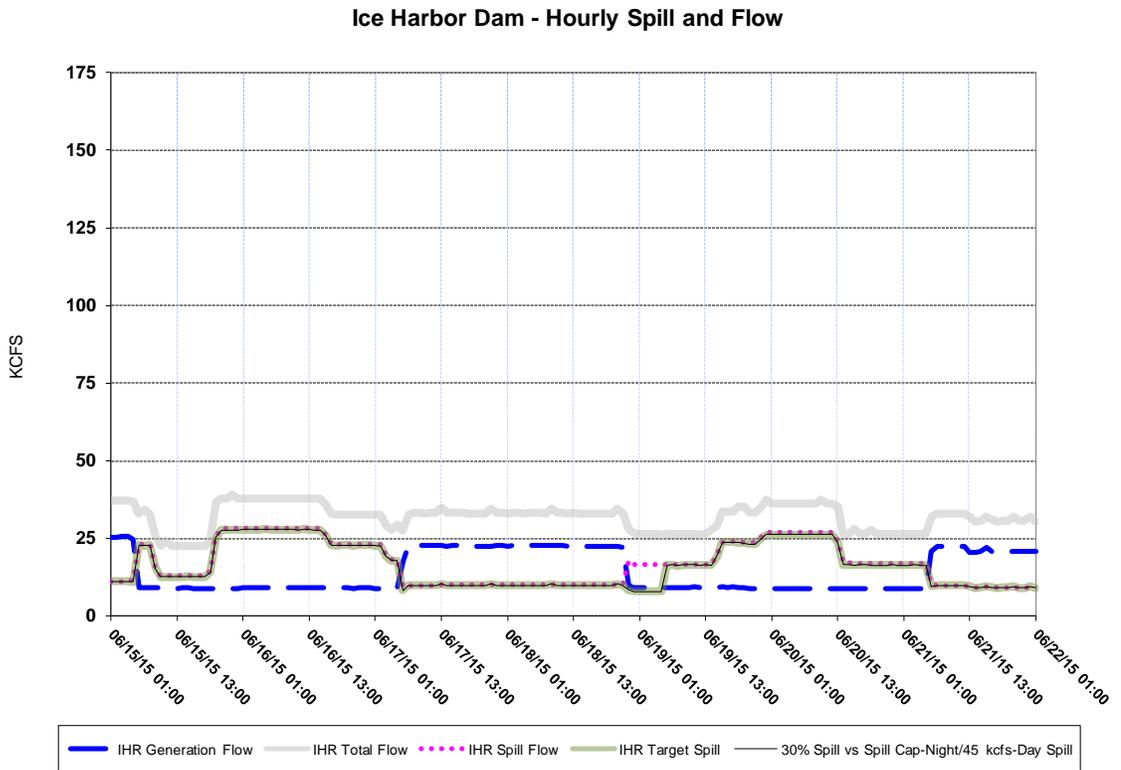
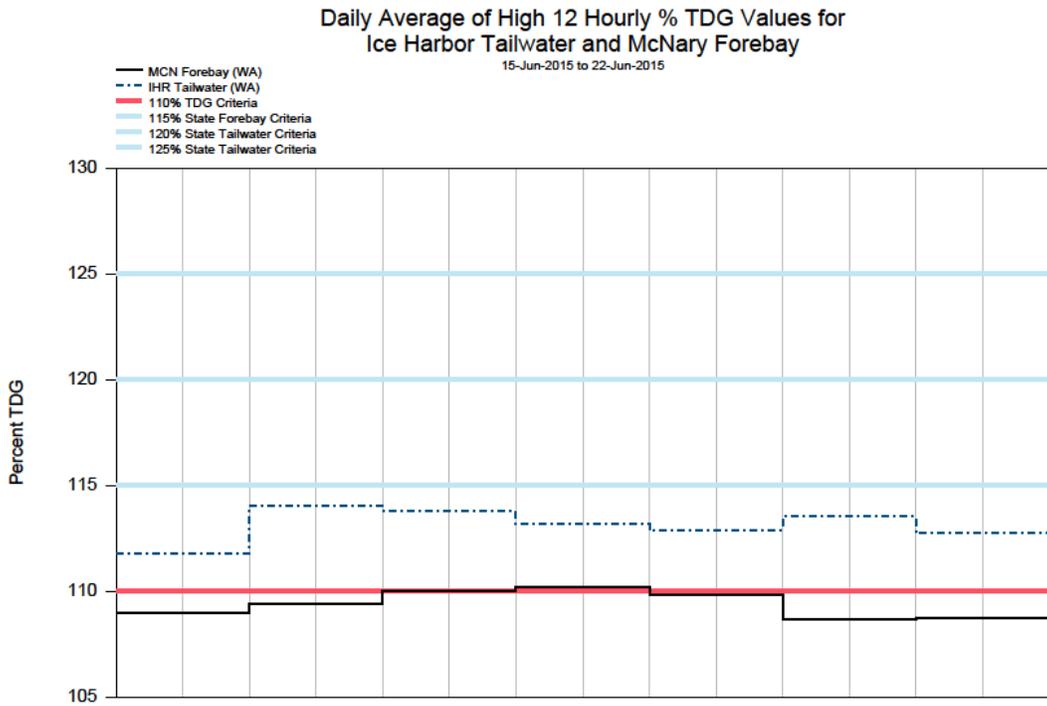


Figure 21

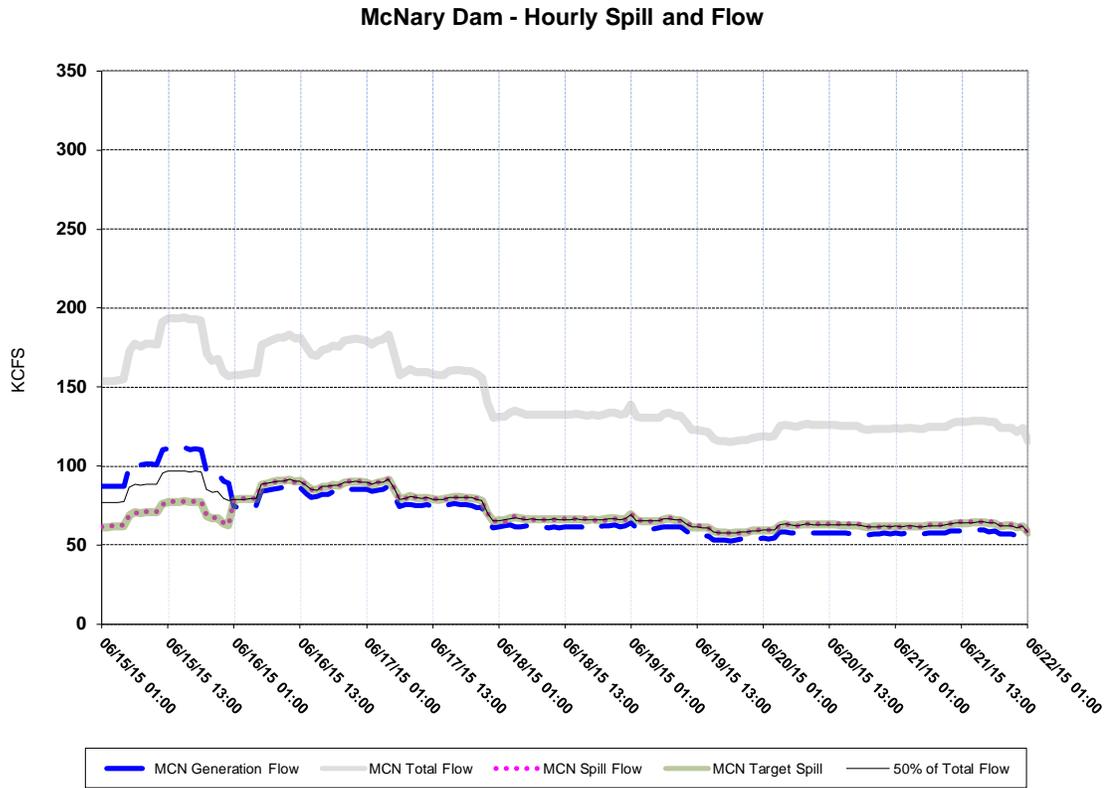
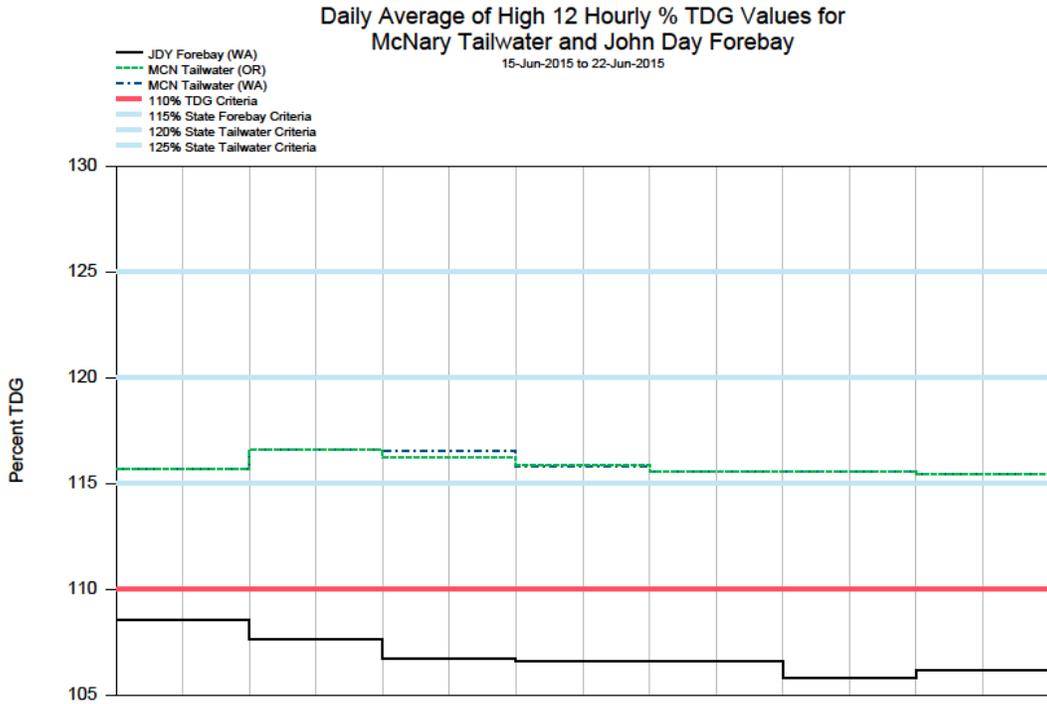
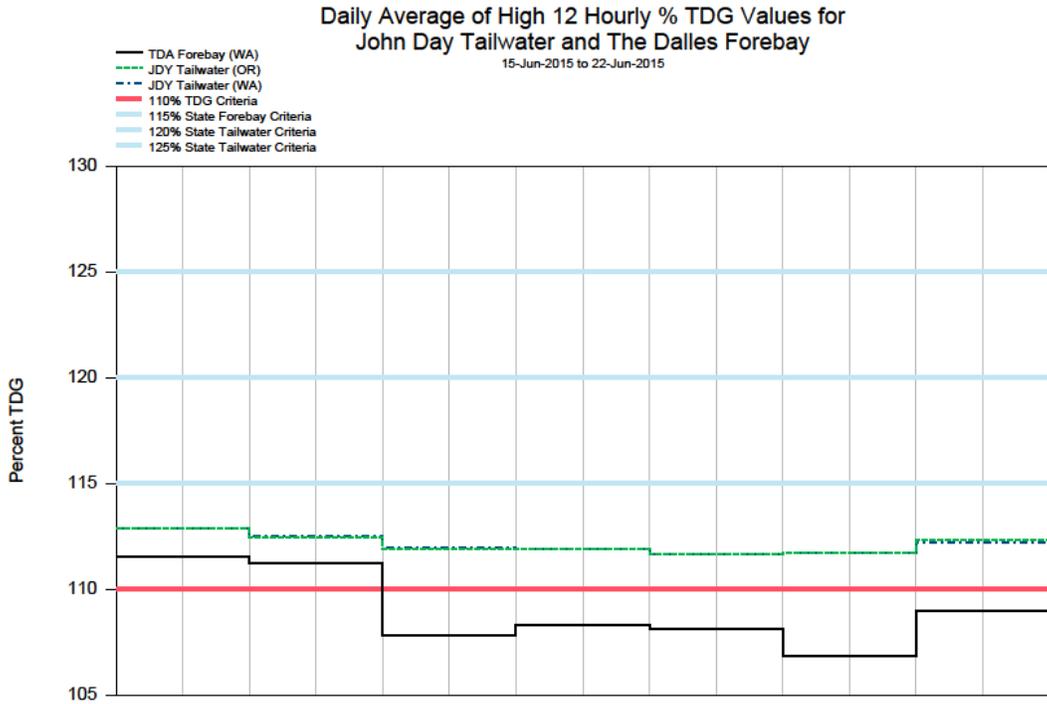


Figure 22



John Day Dam - Hourly Spill and Flow

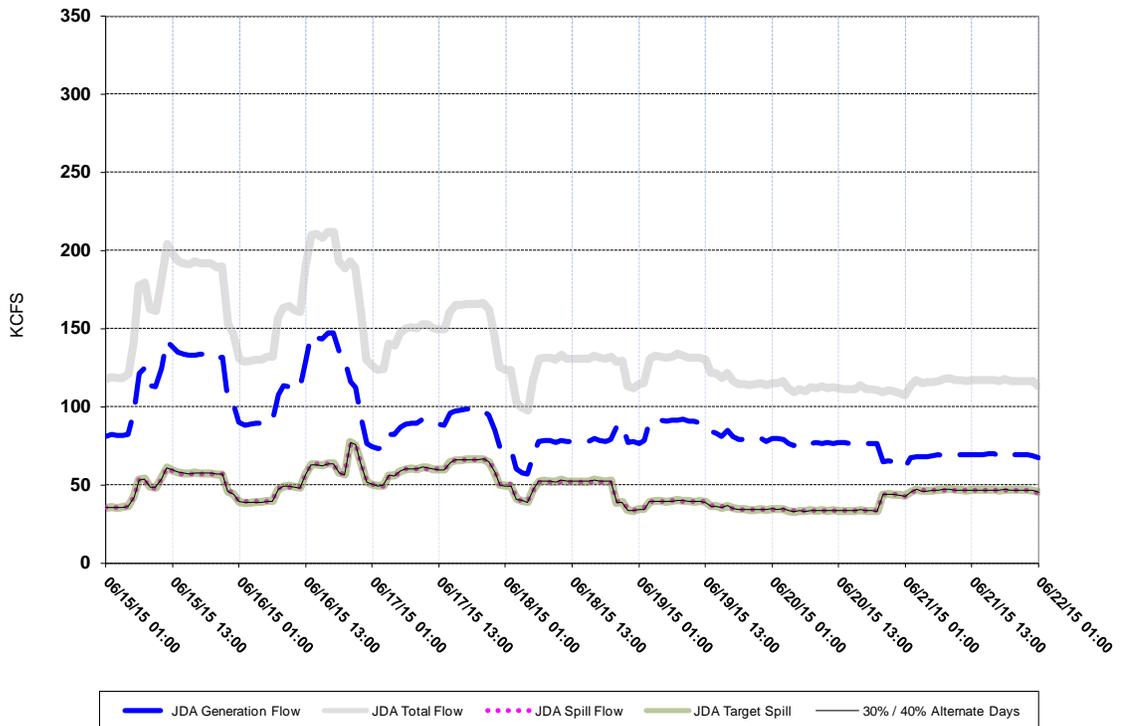
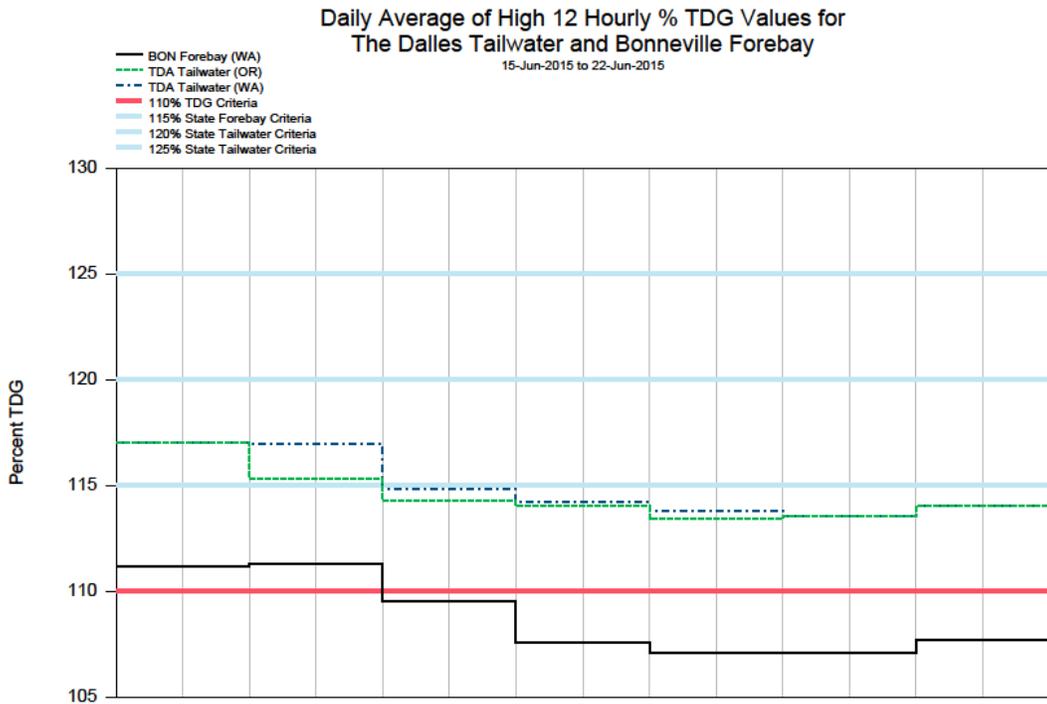


Figure 23



The Dalles Dam - Hourly Spill and Flow

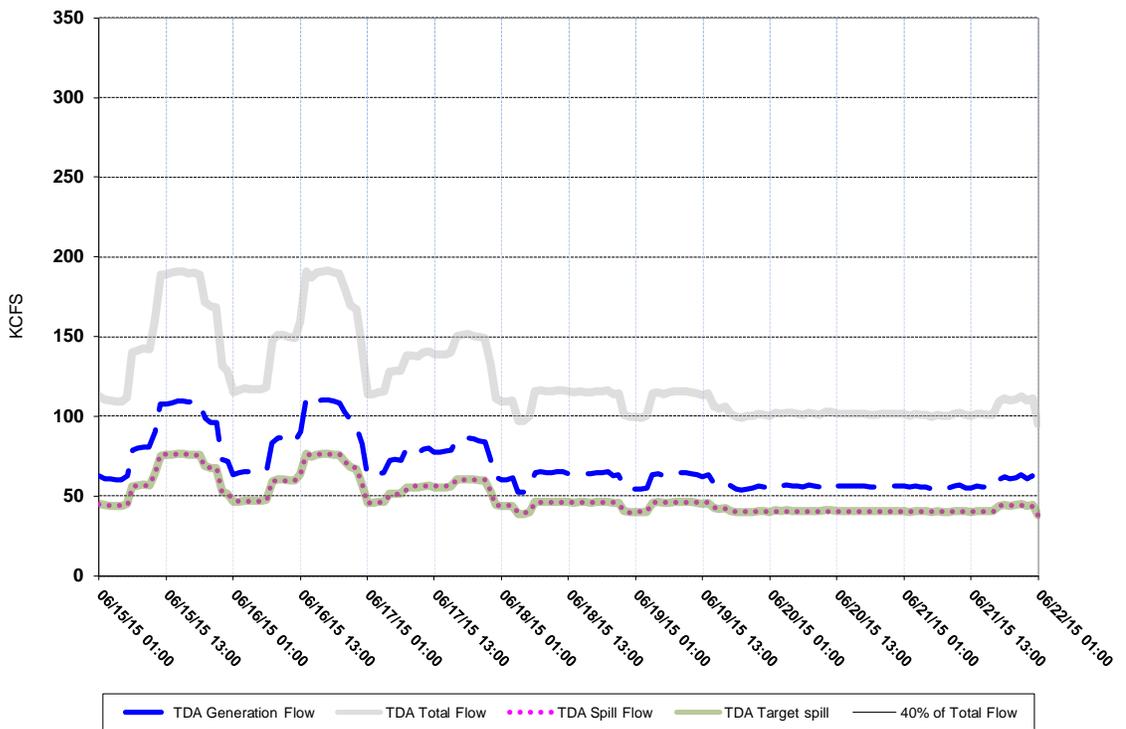
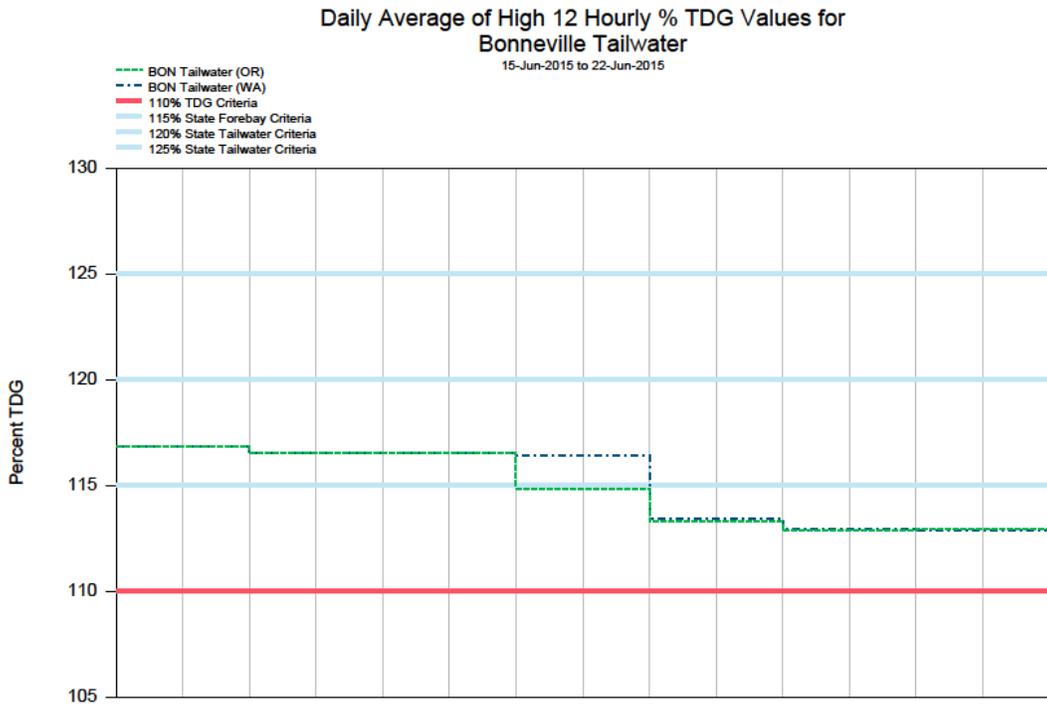


Figure 24



Bonneville Dam - Hourly Spill and Flow

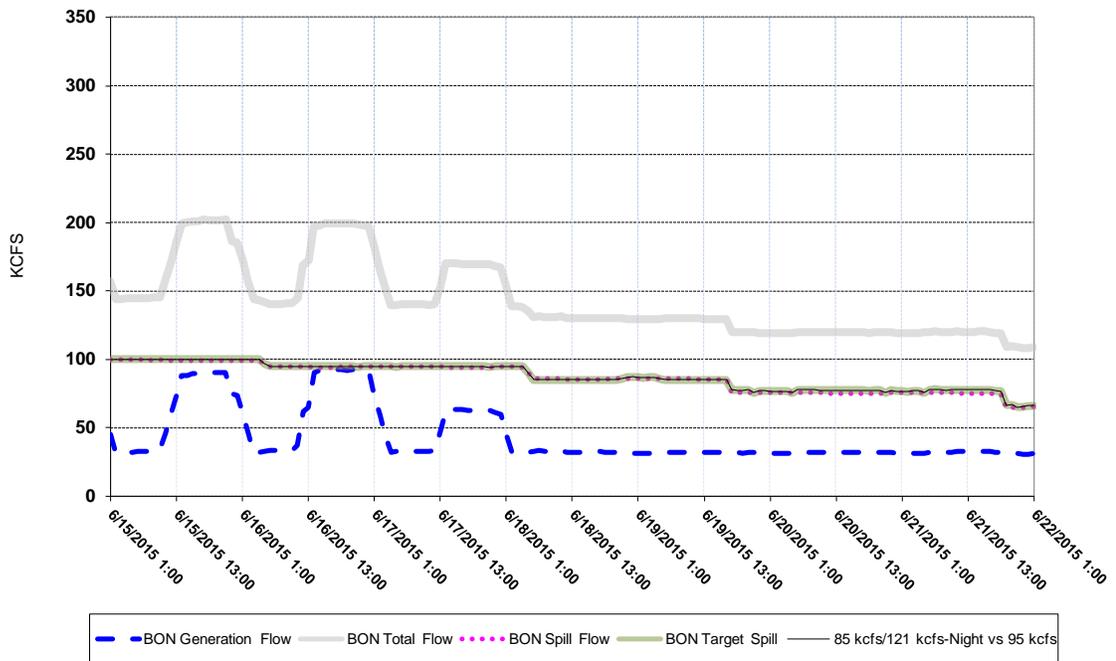


Figure 25

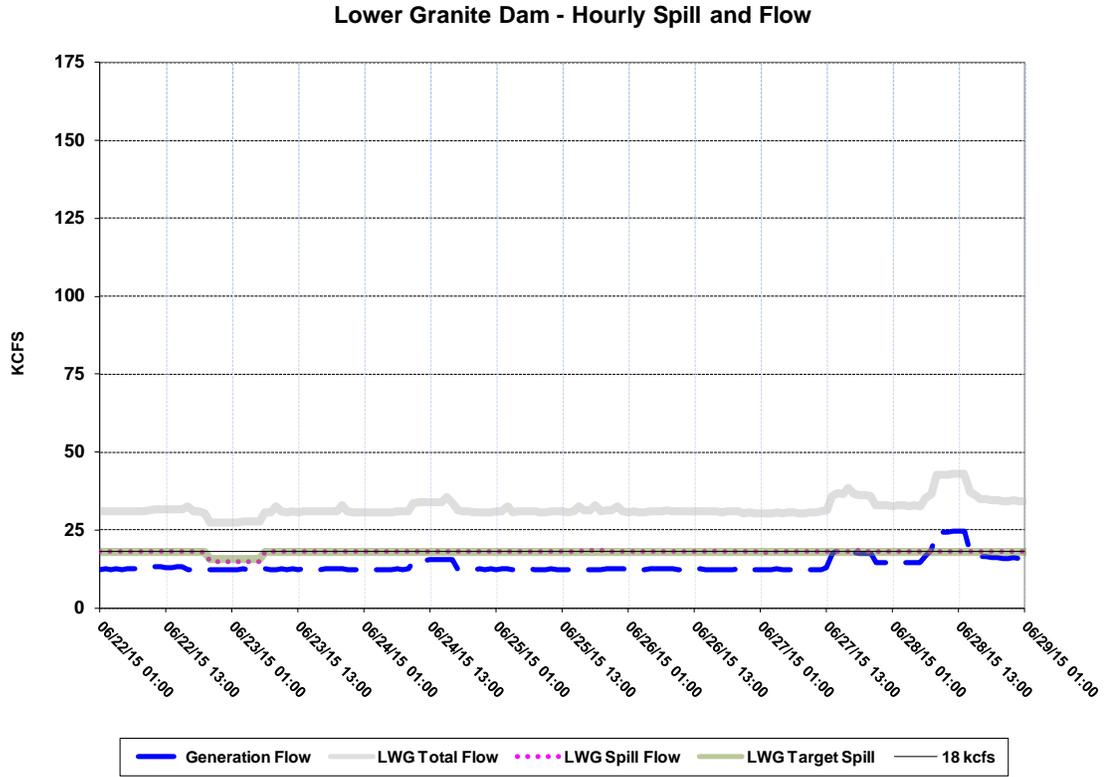
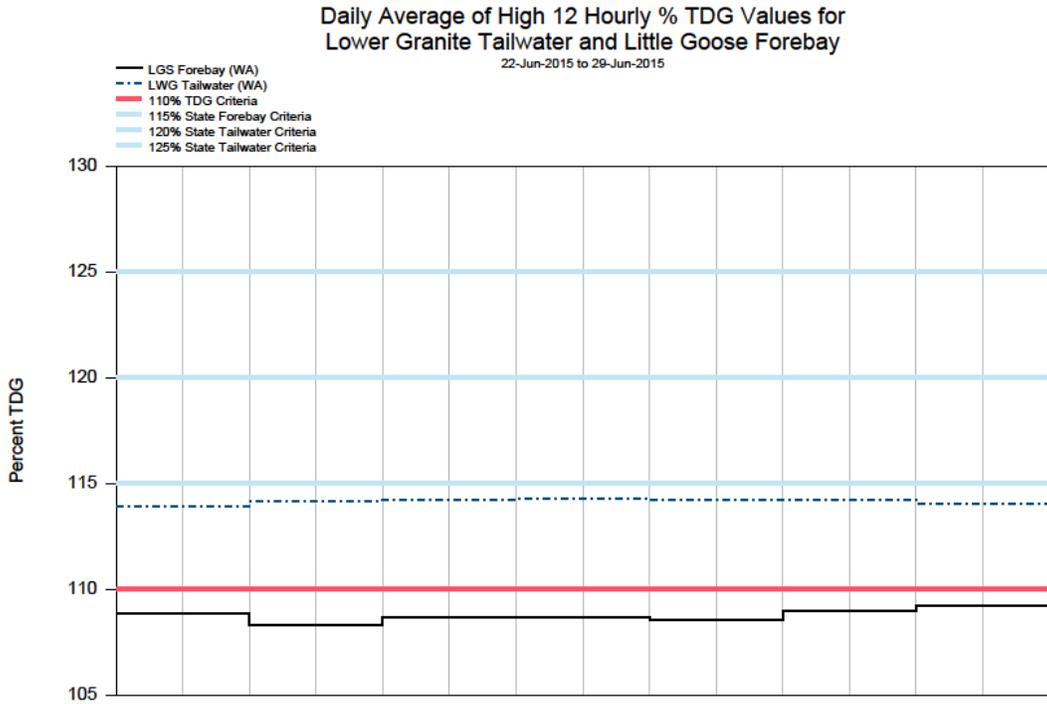


Figure 26

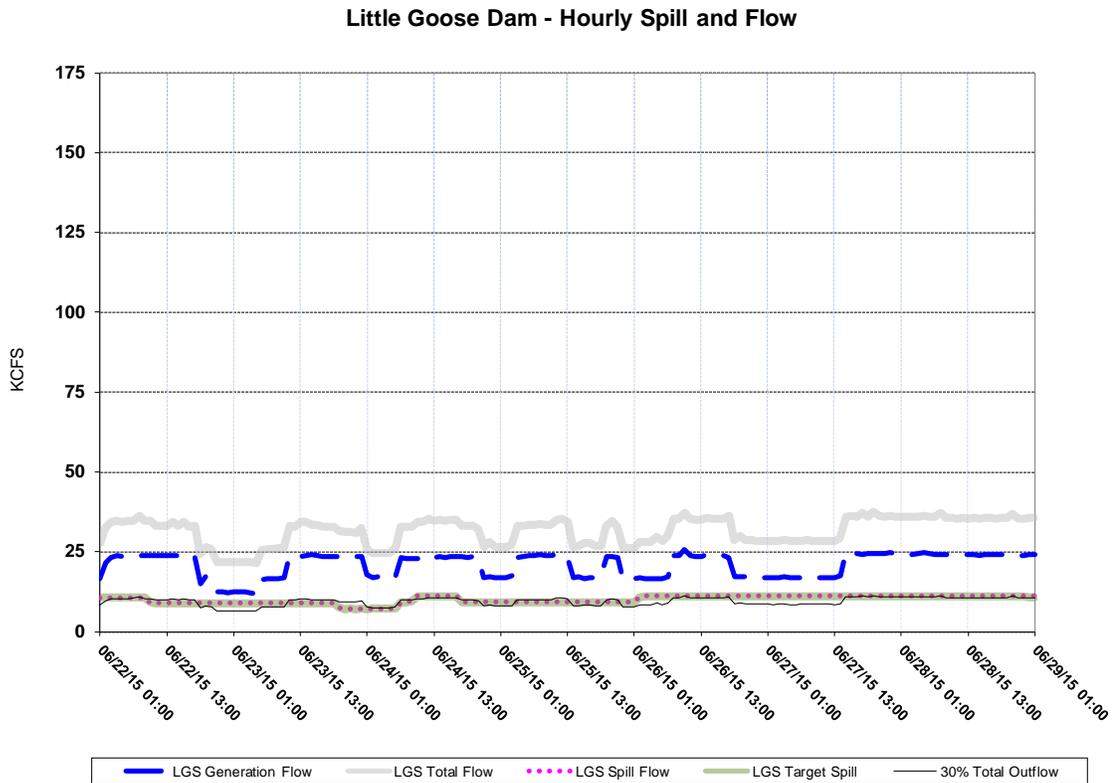
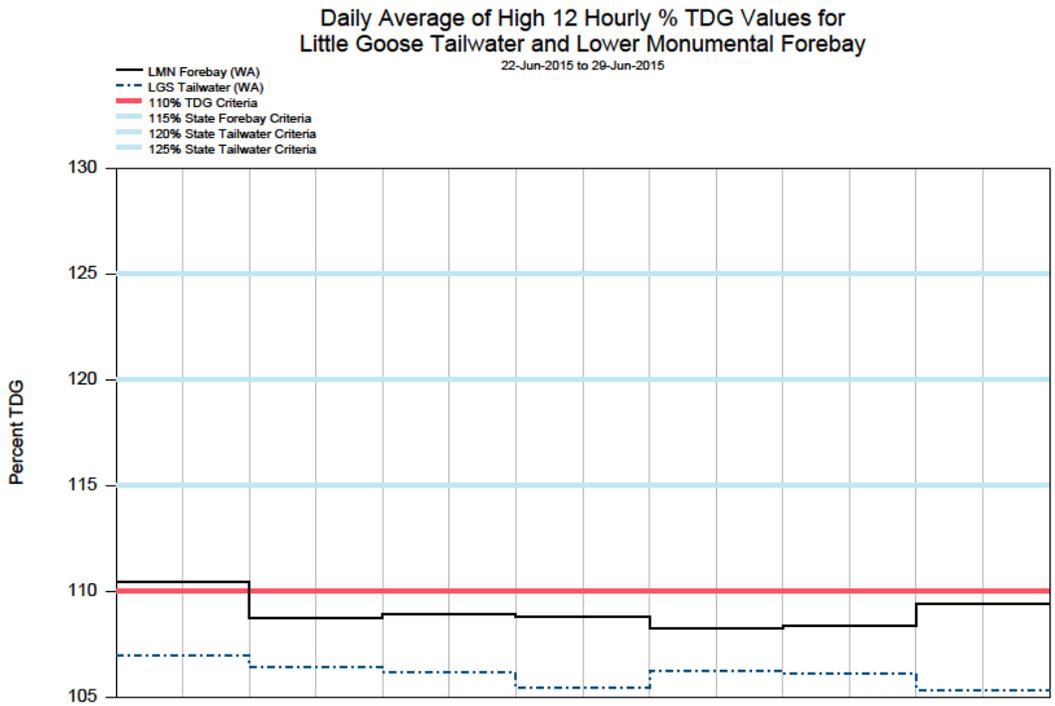


Figure 27

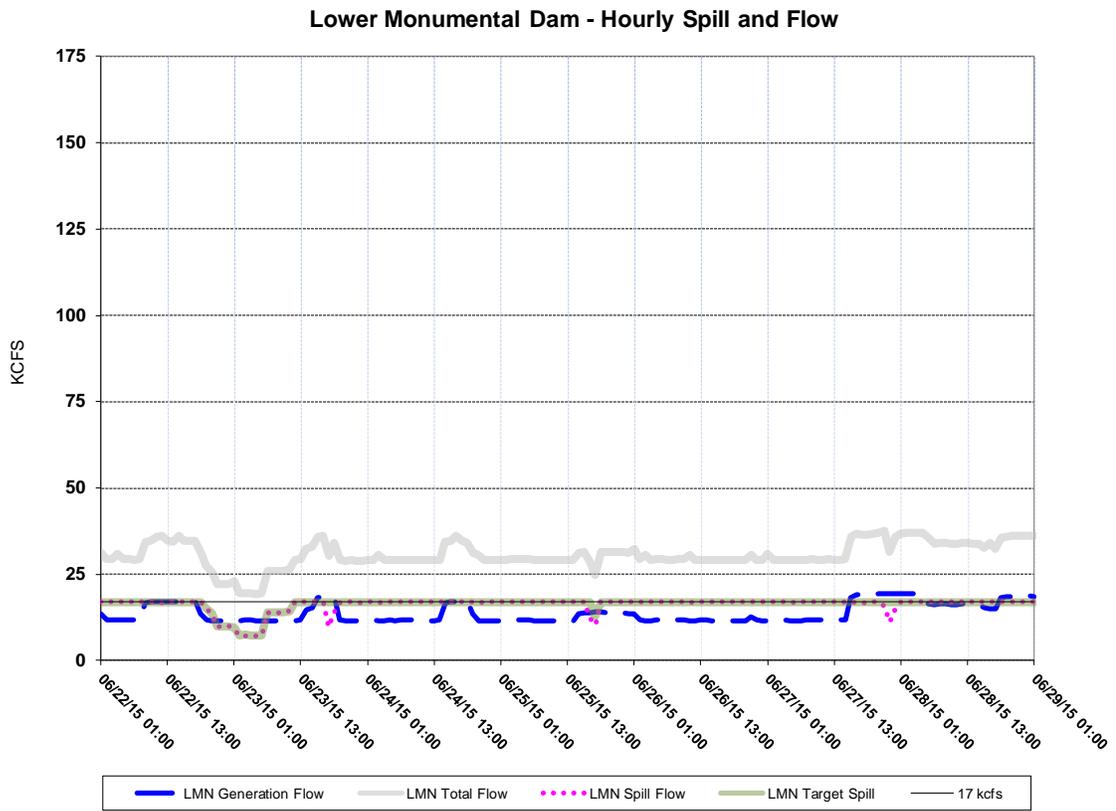
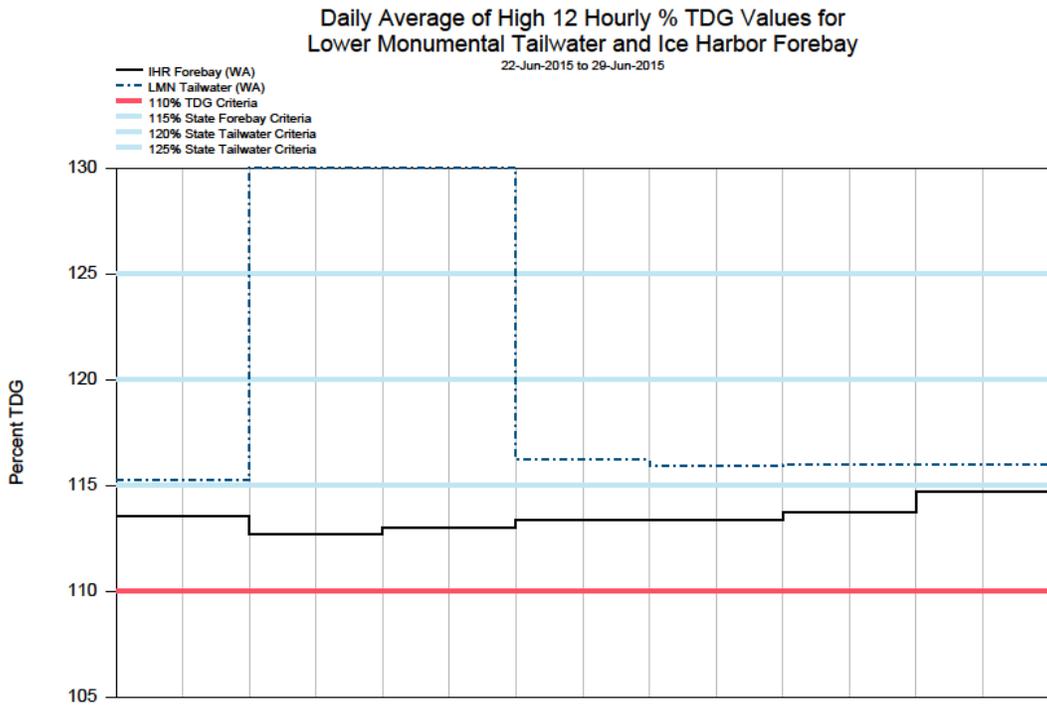


Figure 28

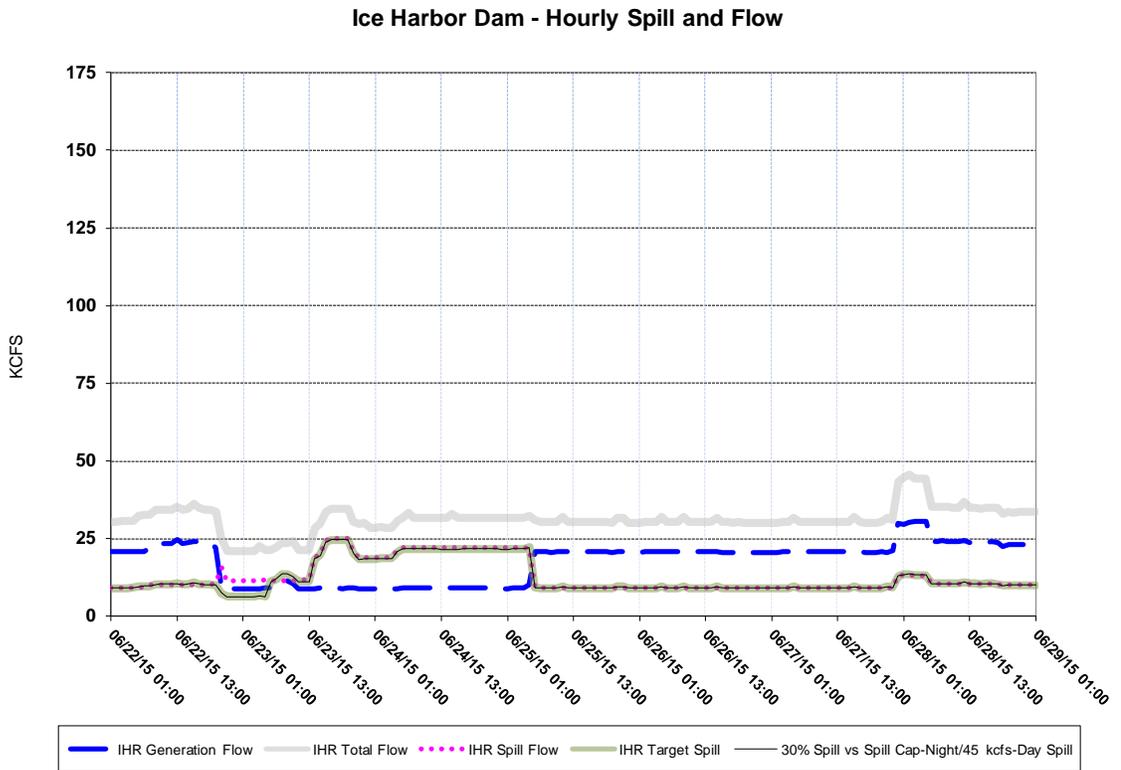
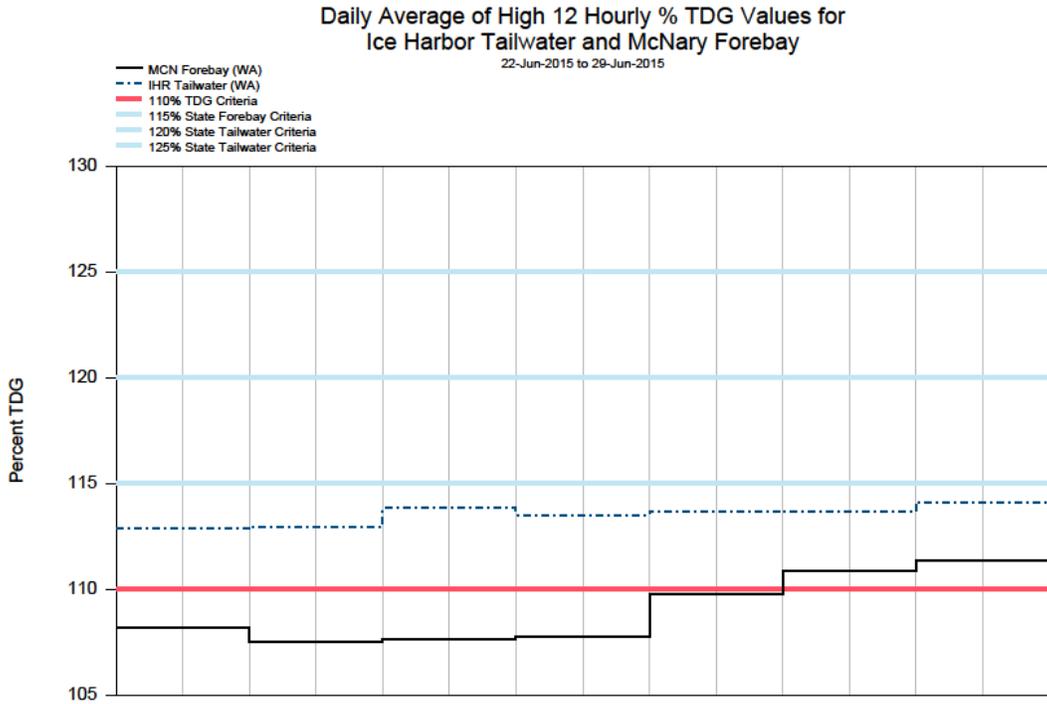


Figure 29

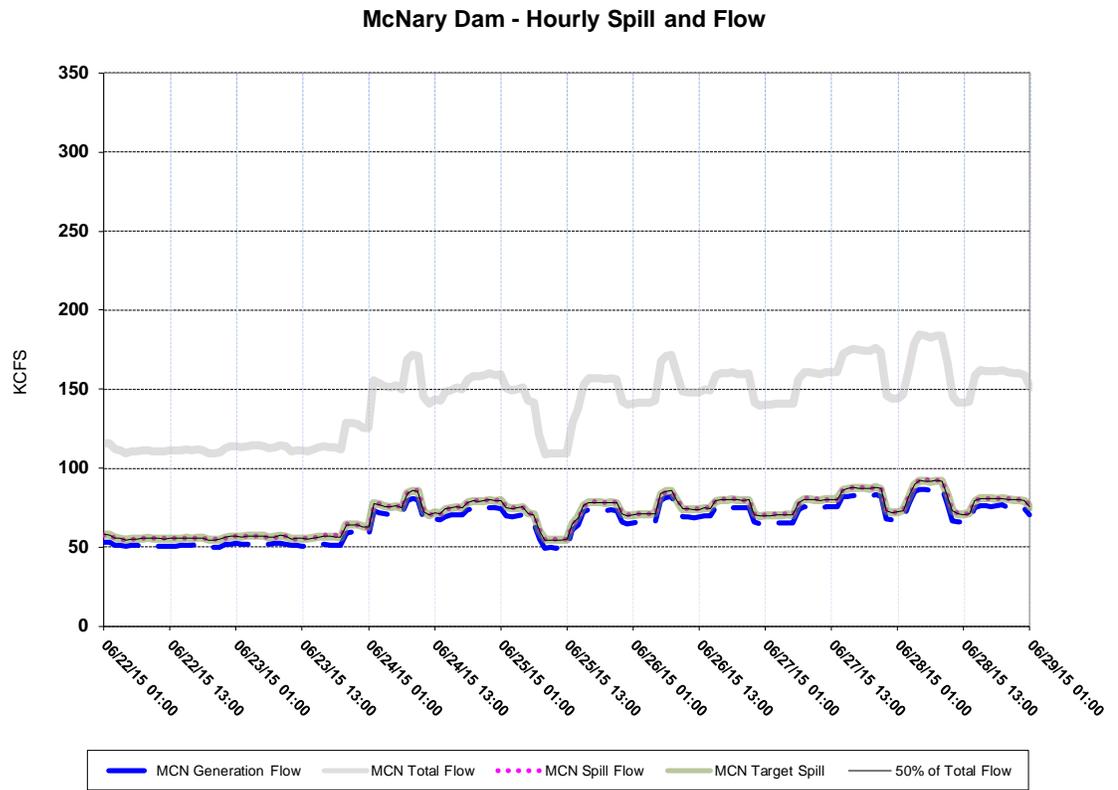
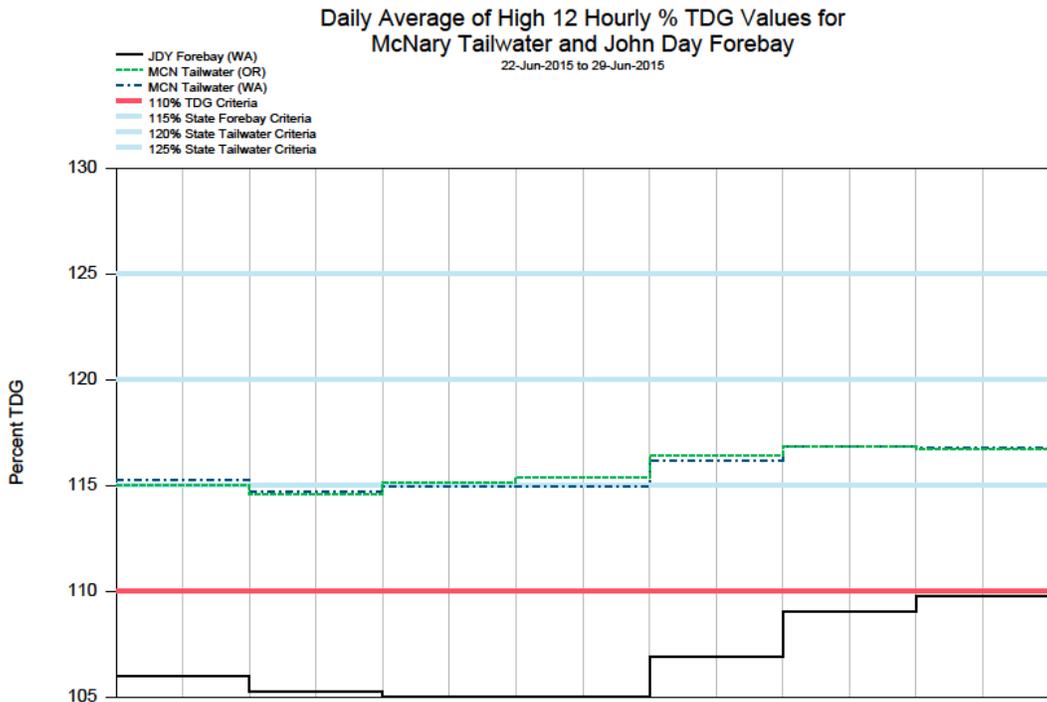
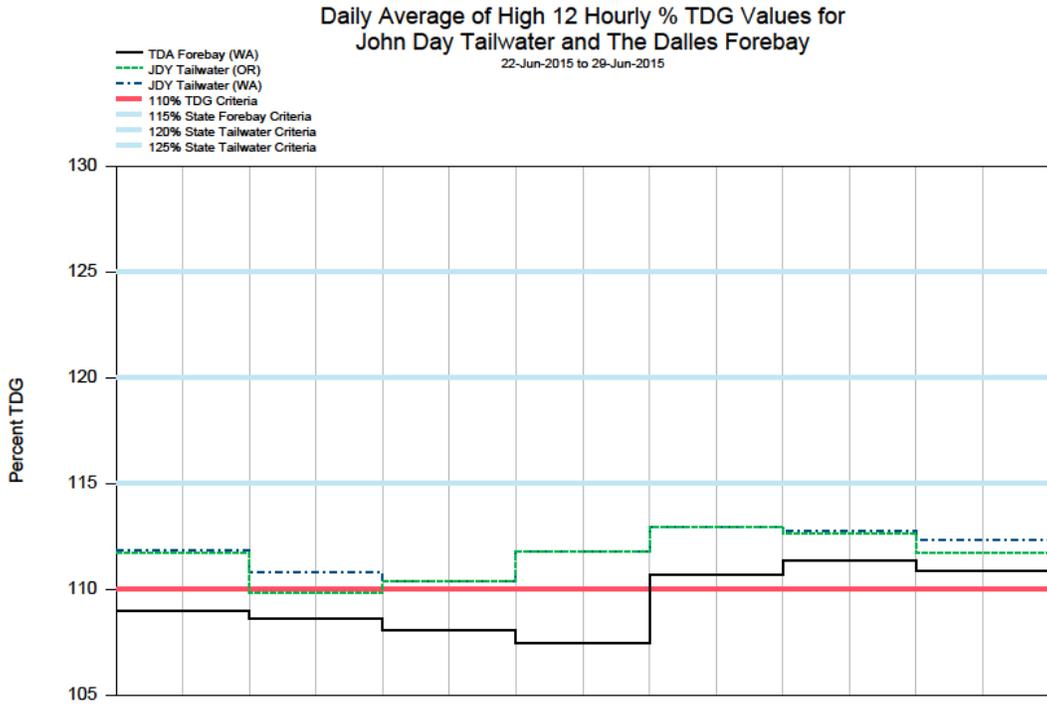


Figure 30



John Day Dam - Hourly Spill and Flow

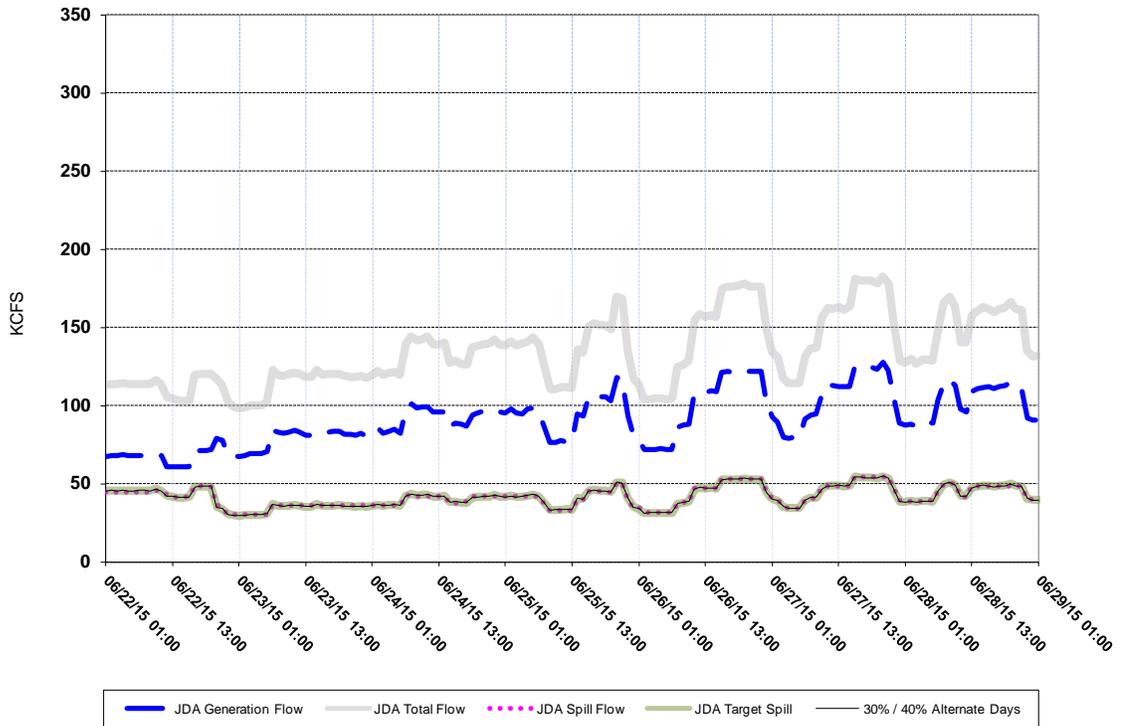


Figure 31

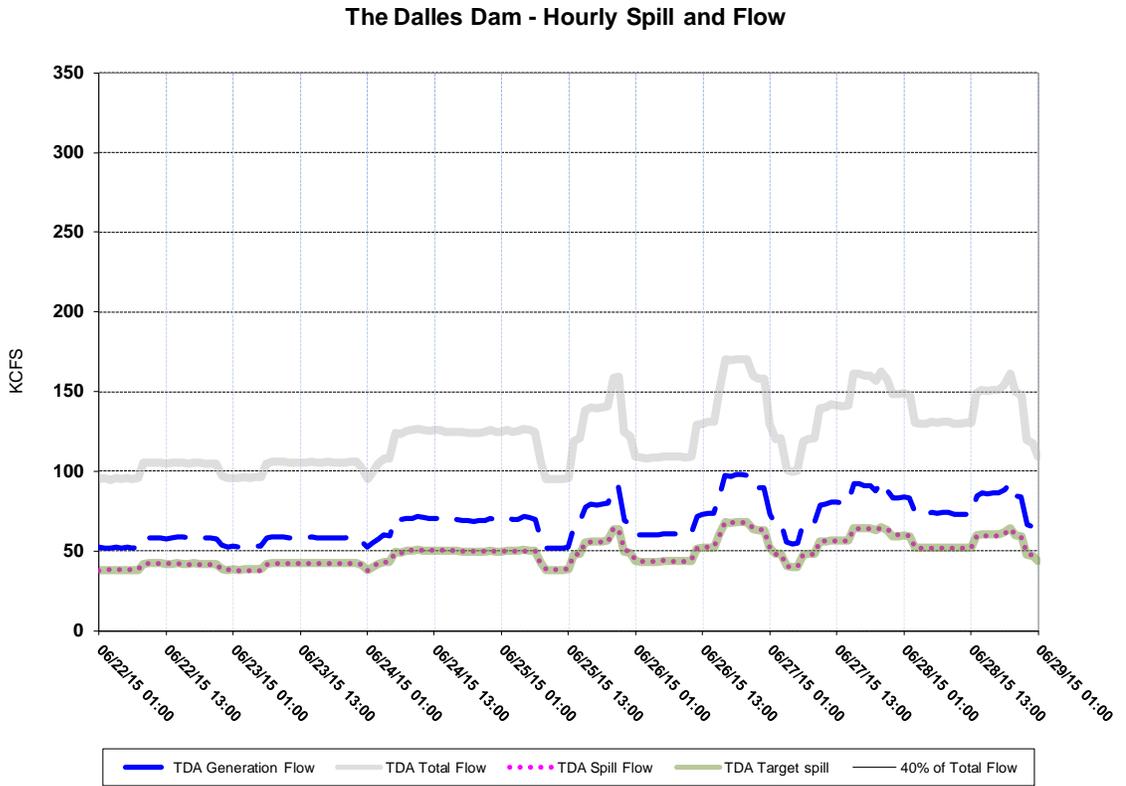
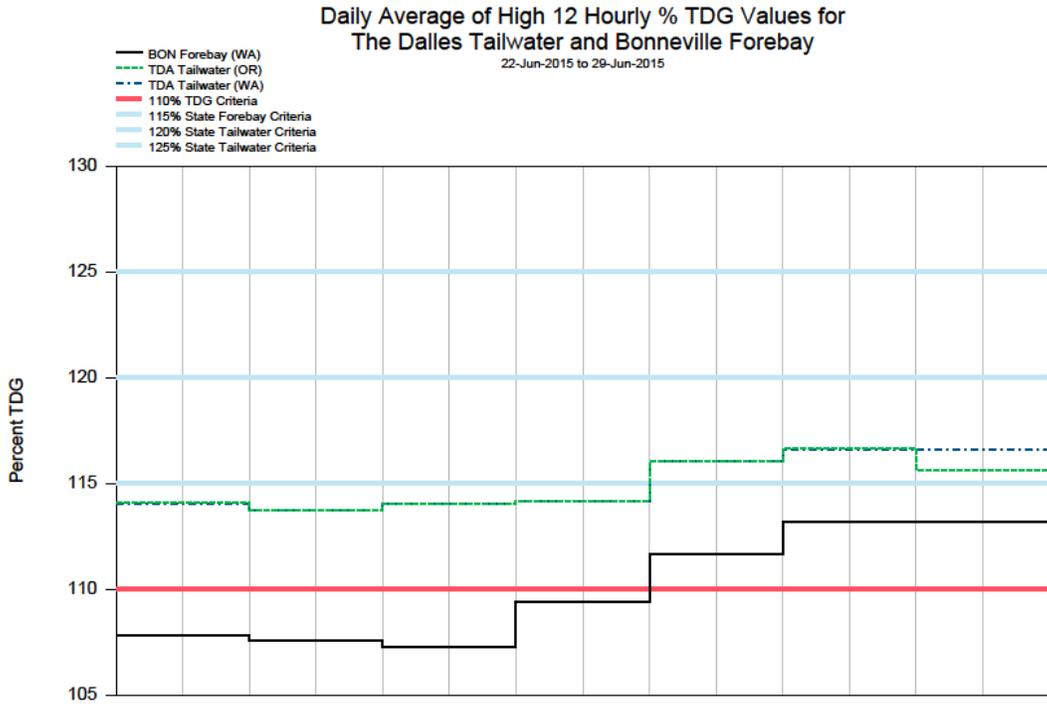


Figure 32

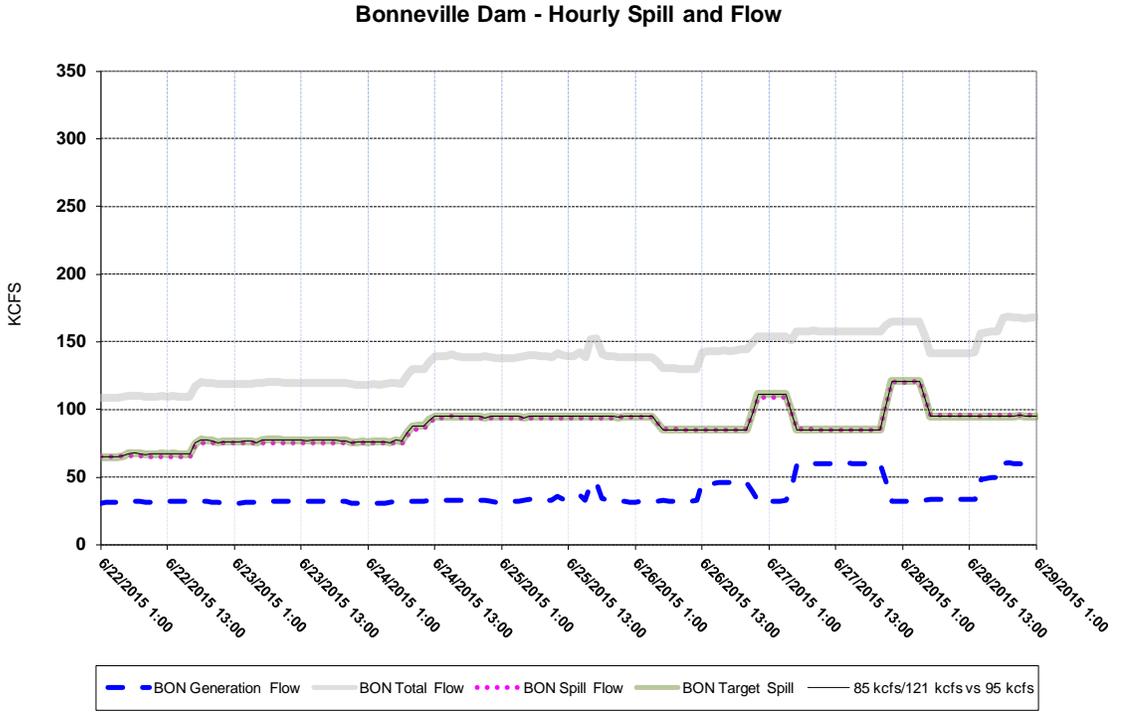
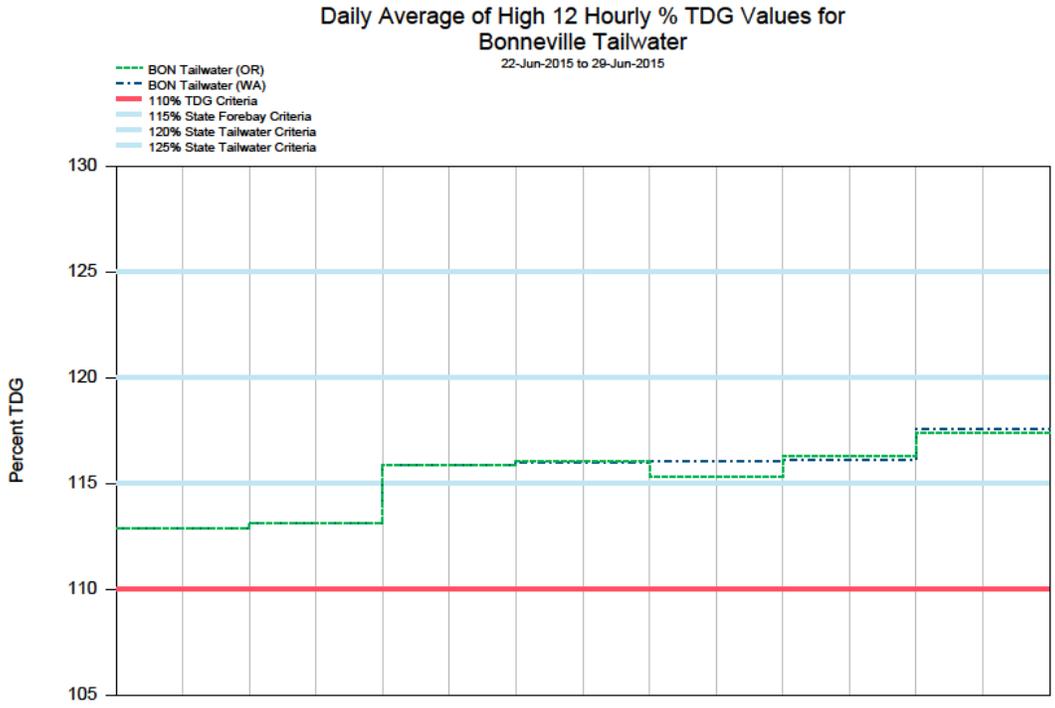


Table 2
Average Percent TDG Values For June 1 – June 28

Date	FIXED MONITORING STATIONS																			
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	ISDW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW	
Method:	WA	WA	WA	WA	WA	WA	WA	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120
6/1/2015	104.5	110.7	112.5	112.4	113.7	117.5	117.5	116	113.1	114.8	114.7	113	114.3	115	112.6	116.5	116.9	113.9	117.2	117.1
6/2/2015	103.8	110.3	111.3	111.8	112.8	114.3	116.5	115.7	111	114.7	114.5	111.9	114.2	114.2	109.8	115.3	115.3	110.7	117.4	117.5
6/3/2015	102.4	110.1	110.7	111.6	111.4	113.9	114.3	115.6	108.6	116.4	116.4	109.8	114.9	114.9	109.6	115.6	115.6	109.3	116.5	117.1
6/4/2015	101.7	109.9	110.3	110.8	110.8	113.7	112.6	115.6	107.5	116	116	108.2	114.3	114.3	109	115.7	115.7	110.1	116.6	116.6
6/5/2015	100.8	110.2	109.8	111.7	112.3	113.4	114	115.5	110.2	115.9	115.9	108.3	113.7	113.7	111.3	117.2	117.2	112.8	116.7	116.7
6/6/2015	101.3	110.8	112.2	112.5	112.8	114	115.6	113.3	112.4	115.9	115.9	109	113.4	113.6	112.6	117.7	117.7	114.4	116.7	116.7
6/7/2015	102.3	110.5	112.4	112	112.6	114.1	117.4	114.7	113.5	116.3	116.3	108.6	114	114	112.5	117.2	117.6	114.3	117.1	117.1
6/8/2015	103.9	110.9	111.7	112.1	113.7	115.7	118.7	114.2	113.5	115.6	116.1	110.4	114.2	114.2	111.3	116.8	117.1	114.3	116.8	116.8
6/9/2015	103.9	111	110.8	112.1	114.1	116.1	118.7	114.5	114.3	116.4	116.4	112.5	115.2	115.2	110.5	116.4	116.6	113.8	117.2	117.2
6/10/2015	104	111.6	110.7	112	114.1	115	118.7	113.9	114.4	114.7	115.1	112.5	114	115	111	115.9	116.3	111.8	116.4	117.2
6/11/2015	103.8	111.8	111	112.1	113.3	114.3	117.8	113.5	113.3	115.2	115.1	110.4	114.5	114.5	108.5	114.2	115.1	108.4	116.7	116.7
6/12/2015	103.6	112.3	111.1	111.7	112.2	114.1	117	113.5	111.7	114.4	114.7	109.7	114	114	107.2	113.6	113.8	105.7	116.9	116.9
6/13/2015	103.1	112.4	110.2	111.3	111.1	114.7	115.8	112.6	109.3	114.1	114.1	107.9	112.2	113.6	107.7	113.7	113.7	106.6	117.1	117.1
6/14/2015	103	112.9	109.8	110.9	110.3	115.4	114	111.8	108.5	113.3	113.7	108.4	112.5	112.4	110.9	116.2	116.2	109	117.1	117
6/15/2015	102	113.5	110	110.5	110.5	115.6	112.5	111.7	109.1	115.7	115.7	108.5	112.9	112.9	111.5	117	117	111.2	117	117
6/16/2015	101.2	113.1	109.1	110.8	111.9	115.9	112.9	114	109.5	116.6	116.6	107.6	112.5	112.5	111.1	115.2	116.8	111.3	116.8	116.8
6/17/2015	100.6	113	109.2	110.5	111.8	115.9	113	113.7	110.1	116.2	116.5	106.6	111.9	111.9	107.8	114.3	114.7	109.3	116.7	116.7
6/18/2015	101.6	112.8	111.4	110.1	111.6	116.2	113.8	113.2	110.2	115.8	115.8	106.6	111.9	111.9	108.3	114	114.1	107.6	114.8	116.7
6/19/2015	101.6	112.5	111.1	106.7	111.5	115.5	113.8	112.7	109.8	115.6	115.5	106.6	111.7	111.6	108	113.4	113.7	107.1	113.5	113.6
6/20/2015	101.9	112.4	109.9	107	110.8	115.7	114	113.5	108.7	115.5	115.5	105.9	111.8	111.7	106.8	113.6	113.5	107.2	113.1	113.1
6/21/2015	102.1	114.2	110.1	106.7	110.8	115.8	114	112.7	108.7	115.4	115.4	106.2	112.3	112.2	109	114	114	107.7	113.1	113.1
6/22/2015	101.5	113.9	108.7	106.9	110.4	115.2	113.5	112.9	108.2	115	115.1	105.8	111.7	111.7	109	114	114	107.8	113.2	113.1
6/23/2015	101.2	114.1	108.3	106.4	108.6	138.6	112.6	113	107.6	114.7	114.6	105.2	109.8	110.6	108.5	113.7	113.7	107.6	113.4	113.3
6/24/2015	101.5	114.2	108.6	106.2	108.9	138.7	113	113.8	107.6	115.1	115	104.9	110.4	110.3	108	114.1	114.1	107.3	116.1	116.1
6/25/2015	102.1	114.3	108.6	105.5	108.8	116.2	113.4	113.5	107.9	115.4	115.1	105.1	111.8	111.8	107.5	114.2	114.2	109.5	116.3	116.2
6/26/2015	103.7	114.2	108.5	106.2	108.3	115.9	113.4	113.7	109.8	116.4	116.2	107	112.9	112.9	110.7	116.2	116.2	111.8	115.7	116.2
6/27/2015	105	114.2	109.1	106	108.4	116	113.8	113.6	111	116.8	116.8	109.2	112.6	112.6	111.3	116.6	116.6	113.2	116.6	116.3
6/28/2015	106.3	114	109.2	105.3	109.4	116	114.7	114.1	111.3	116.7	116.7	109.7	111.7	112.1	110.7	115.6	116.5	113.1	117.5	117.8

Note: The Oregon TDG standard modification (OR) and the Washington TDG criteria adjustments (WA) have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard. TDG values are presented in Table 1 by displaying the highest value %TDG (more stringent), and the lower value is displayed with a strikethrough.

Total Dissolved Gas Monitoring Stations

Code	Station Name
LWG	Lower Granite Forebay
LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay
LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay
LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay
IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay
MCPW	McNary Tailwater
JDY	John Day Forebay
JHAW	John Day Tailwater
TDA	The Dalles Forebay
TDDO	The Dalles Tailwater
BON	Bonneville Forebay
CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal

FISH OPERATIONS PLAN IMPLEMENTATION REPORT

July 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' July 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in July 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in July displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

¹ Averages reported are consistent with current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and Washington TDG criteria adjustments have different methodologies for calculating TDG. When standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented Monday through Sunday.

The weekly figures begin on June 29 and end on August 2 for the following lower Snake River and lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on June 29 for the lower Snake River and the lower Columbia River projects.

June 29 – July 5	Figures 1 – 8
July 6 – July 12	Figures 9 – 16
July 13 – July 19	Figures 17 – 24
July 20 – July 26	Figures 25 – 32
July 27 – August 2	Figures 33 – 40

A. Upper Figure: Displays the daily average %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the observed percent TDG in the tailwater of the dam using the Oregon 120 %TDG standard calculated with the high 12-hour average.¹ Applies only to figures which include the lower Columbia dams.
2. The blue dot-dash line represents the observed percent TDG in the tailwater of the dam using the Washington 120 %TDG standard calculated with the high 12-hour average.¹
3. The black solid line represents the observed percent TDG in the forebay of the next dam downstream using the Washington 115 %TDG standard calculated with the high 12-hour average.¹

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

II. A table is included at the end of the figures that lists the daily average of high %TDG values for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects, tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the July 2015 Spill Variance Table.³ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour (except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams,⁴ which may

³ Involuntary spill conditions appear in the figures but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

⁴ As specified in the 2015 FOP (p. 14), this applies when spill is below 40% of total outflow at The Dalles Dam.

range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

July 2015 Operations

The month of July was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the July 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 1.1 MAF (Million Acre Feet) or 48% of average as measured at Lower Granite Dam. For the lower Columbia, the Runoff Processor indicated the July 2015 adjusted volume runoff was below the 30 year average (1981-2010): 7.6 MAF or 52% of average as measured at The Dalles. The monthly precipitation summary for July was above average at 128% (1.29 inches) on the Snake River above Ice Harbor Dam but below average on the Columbia River above The Dalles Dam at 83%.

During the July 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 18 kcfs, 24 hours/day.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day. Due to low flow conditions, the operation transitioned to an hourly constant spill

target of 7/9/11 kcfs operation⁵, depending on the previous day's outflow as coordinated with TMT on June 25.

- Lower Monumental Dam - The hourly target spill level was 17 kcfs, 24 hours/day.
- Ice Harbor Dam - The hourly target spill level alternated in 2-day blocks between 30% of total project outflow, 24 hours/day and 45 kcfs during the day and the %TDG cap during the nighttime (gas cap range ~75 – 95 kcfs) until July 13 when the operation transitioned to 45 kcfs spill during the daytime and the %TDG cap spill during the nighttime. Nighttime spill hours (1800-0500).
- McNary Dam - The hourly target spill level was 50% of total project outflow, 24 hours/day.
- John Day Dam - The hourly target spill level alternated in 2-day blocks between 40% and 30% of total project outflow, 24 hours/day until July 20 when the operation transitioned to 30% of total river flow for 24 hours/day. Spill level changes occurred at 2000 hours.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level alternated in 2-day blocks between 95 kcfs, 24 hours/day vs. 85 kcfs during the day and 121 kcfs during the nighttime.

Operational Adjustments

1. Lower Granite Dam.

Beginning at 1210 hours on July 8, the Corps implemented the FPOM recommended operation intended to improve tailrace hydraulics and temperature conditions for the benefit of adult sockeye passage. The spillway weir was closed and spill was distributed uniformly across the spillway as described in the 2015 Fish Passage Plan, Table LWG-9. This operation did not alter FOP spill levels. The operation was coordinated to continue through 2400 hours on August 31.

Additionally, from 1500 hours on July 13 through 0500 hours on August 3, the Corps implemented the FPOM recommendation to change from operating Unit 2 to operating Unit 1 as the priority turbine unit to improve passage conditions for adult sockeye during emergency trap and haul operations implemented by the Idaho Department of Fish and Game. The operation of Unit 1 provides optimum attraction flow near the adult fish ladder, improves tailrace hydraulics near the ladder entrance by minimizing the eddy created by spill, and improves downstream temperature conditions by passing more cool water from deeper in the forebay to the tailrace. However, Unit 1 has fixed blades (non-adjustable) and operates at approximately 18.4 kcfs, compared to Unit 2 which can be adjusted as flow decreases down to minimum generation of approximately 12.4 kcfs. Consequently, during minimum generation operations, Unit 1 results in less spill (approximately 6 kcfs) than Unit 2.

The operations to improve Snake River sockeye passage conditions were discussed and coordinated with FPOM on several conference calls on July 6, 8, 9, 10, 13, 17, 20, 24, and 27; and with TMT at meetings on July 8, 15, 22, 27, 29, and 30. FPOM and TMT members either supported or did not object.

⁵ See FOP (p. 6) for low flow operations at Little Goose Dam.

2. Little Goose Dam.

From 0400 hours on July 23 through 0400 hours on July 25, and again at 0400 hours on July 28 through 0400 hours on July 30, the Corps implemented experimental emergency operations at Little Goose Dam as recommended by NOAA Fisheries and other regional sovereigns to improve passage conditions for adult sockeye. In conjunction with the Lower Granite operations described above, the goal was to assess whether these actions could improve temperature and hydraulic conditions at the two projects as a means of facilitating adult sockeye passage at both dams during the Idaho Department of Fish and Game's emergency trap and haul operations.

The two 2-day experimental emergency operations at Little Goose consisted of a period of no spill during daytime hours (0400-2000) and the operation of one unit at minimum generation and spilling the remainder of project outflow during nighttime hours (2000-0400). As a result, hourly average spill during these operations ranged from 0–16.9 kcfs, as compared to the 2015 FOP low flow spill operation that would have resulted in fixed spill of 9 or 11 kcfs as determined by the previous day's average outflow.

These operations were coordinated with FPOM during conference calls on July 21, 24, and 27; and with TMT at meetings on July 22, 27, 29, and 30. Consensus at TMT on the 2-day experimental operation was not reached. After conferring with NOAA and reviewing their recommendation and supporting documents, the Corps proceeded with implementation of the 2-day experimental operation. Oregon's representative for Regional Implementation Oversight Group (RIOG) requested a RIOG meeting to further discuss the operation. The RIOG was convened on July 28, and after discussing these experimental emergency operations, no further objections were raised by sovereign representatives.

July 2015 Spill Variance Table

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Lower Granite	Reduced Spill	7/30/15	1100	1	Maintenance	Hourly spill at 11.4 kcfs (below FOP 18 kcfs), while generation increased above the minimum range (16.4-19.5 kcfs) to 20.9 kcfs for testing necessary before planned annual maintenance.
Lower Monumental	Reduced Spill	6/29/15	1700-1800	2	Navigation	Hourly spill decreased to 7.1 kcfs and 11.6 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Lower Monumental	Reduced Spill	7/1/15	1700-1800	2	Navigation	Hourly spill decreased to 11.3 kcfs and 13.2 kcfs (below 17 kcfs \pm 2 kcfs range). Reduced spill for safe passage of fish barge.
Ice Harbor	Reduced Spill	6/29/15	1000	1	Navigation	Hourly spill reduced from minimum generation spill of 29.9% to 28.5% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill 29.8%.
Ice Harbor	Reduced Spill	6/29/15	1300	1	Navigation	Hourly spill reduced from minimum generation spill of 30.0% to 28.8% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill 29.8%.
Ice Harbor	Reduced Spill	6/29/15	1600	1	Navigation	Hourly spill reduced from minimum generation spill of 30.0% to 28.7% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill 29.8%.
Ice Harbor	Reduced Spill	6/29/15	2100	1	Navigation	Hourly spill reduced from minimum generation spill of 30.0% to 28.7% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock. 24-hr avg spill 29.8%.
Ice Harbor	Reduced Spill	6/30/15	0100	1	Navigation	Hourly spill reduced from minimum generation spill of 30.1% to 28.7% (below 30.0% \pm 1% range) due to volume of water needed to empty the navigation lock.
Ice Harbor	Reduced Spill	7/30/15	1700	1	Maintenance	Hourly spill at 25.2 kcfs (below FOP 45 kcfs) while generation increased above Unit 1 minimum range (8.2-10.0 kcfs) to 11.3 kcfs, for returning unit 5 to service after planned annual maintenance and testing.
John Day	Additional Spill	7/1/15	0000	1	Transmission Stability	Hourly spill increased to 41.4% (above 40.0% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill 40.0%.

⁶ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Project	Parameter	Date	Time⁶	Hours	Type	Reason
John Day	Reduced Spill	7/8/15	0900	1	Transmission Stability	Hourly spill decreased to 38.9% (below 40.0% ±1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill 38.2%.
John Day	Reduced Spill	7/11/15	1100	1	Transmission Stability	Hourly spill decreased to 38.7% (below 40.0% ±1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill 40.1%.
John Day	Reduced Spill	7/23/15	1600	1	Program Error	Hourly spill decreased to 28.9% (below 30.0% ±1% range). Computer program failed to display spill changes so duty schedulers were unaware of low percent spill. 24-hr avg spill 30.0%.
John Day	Reduced Spill	7/29/15	1400	1	Maintenance	Hourly spill decreased to 28.6% (below 30.0% ±1% range) due to installation and testing of a digital governor during planned annual maintenance on Unit 15. 24-hr avg spill 29.8%.
The Dalles	Reduced Spill	7/16/15	1300	1	Transmission Stability	Hourly spill decreased to 38.4% (below 38.6 to 41.4 %). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg spill 39.9%.

Figure 1

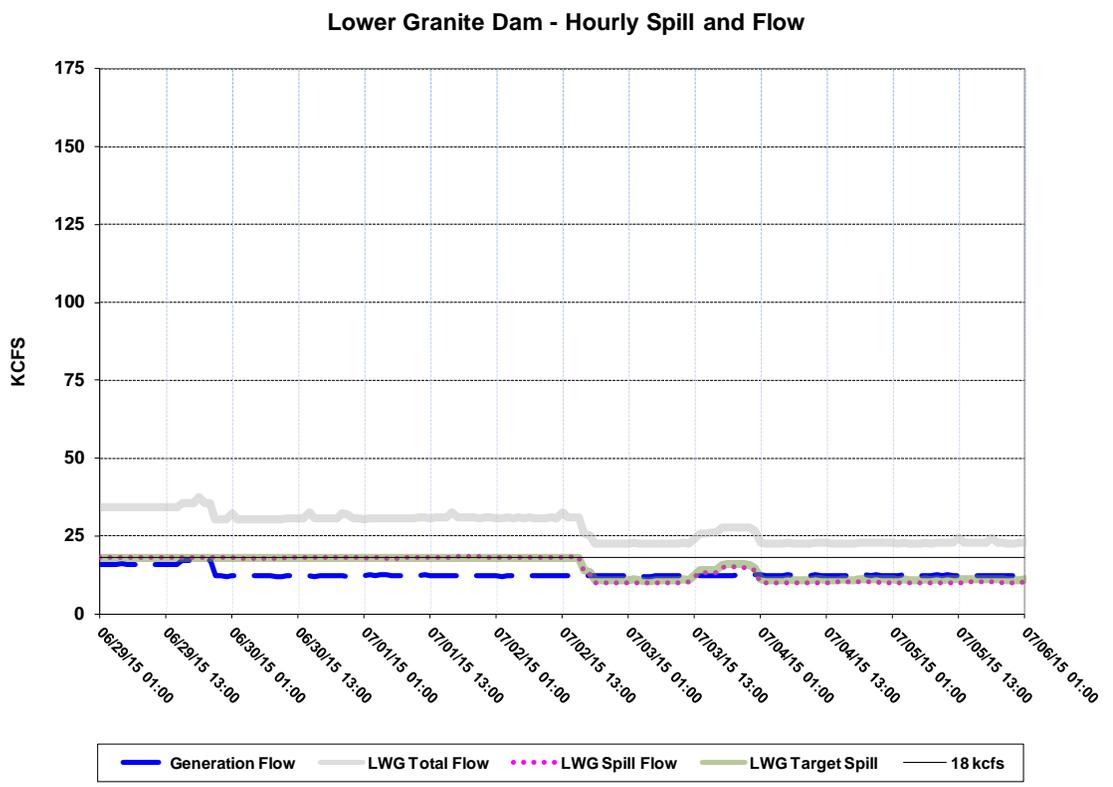
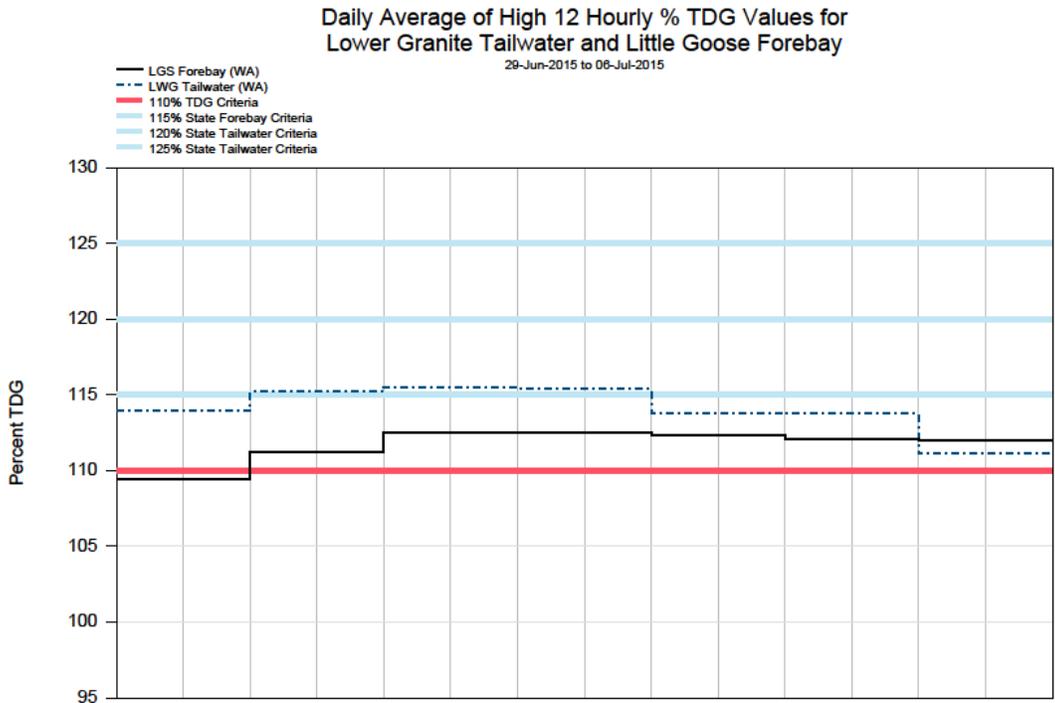
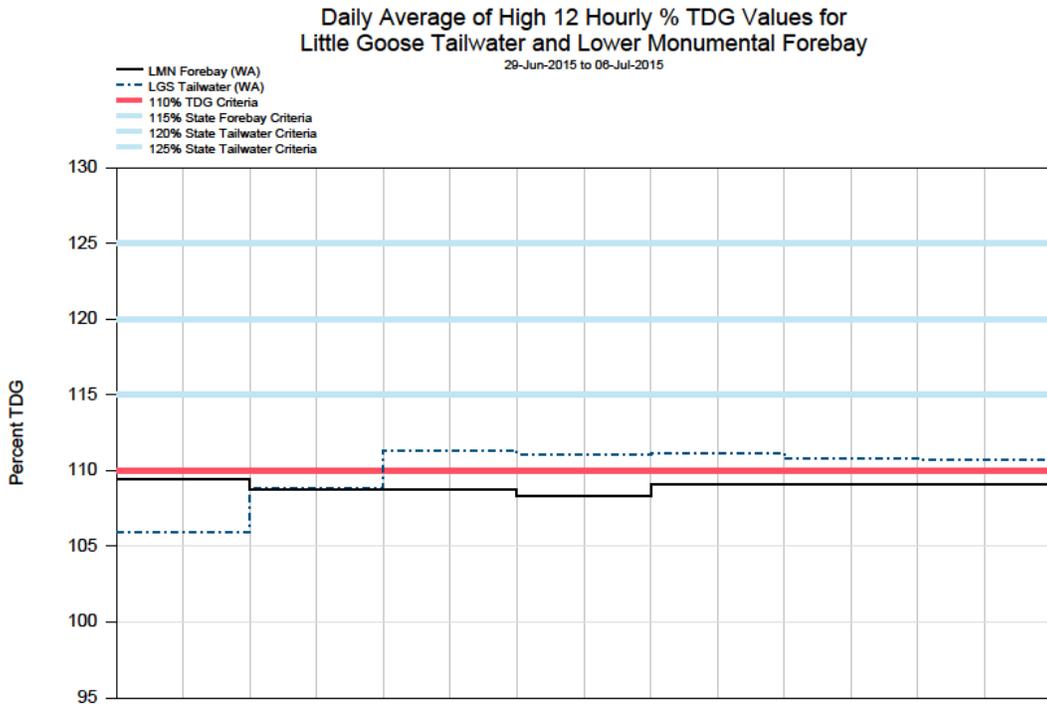


Figure 2



Little Goose Dam - Hourly Spill and Flow

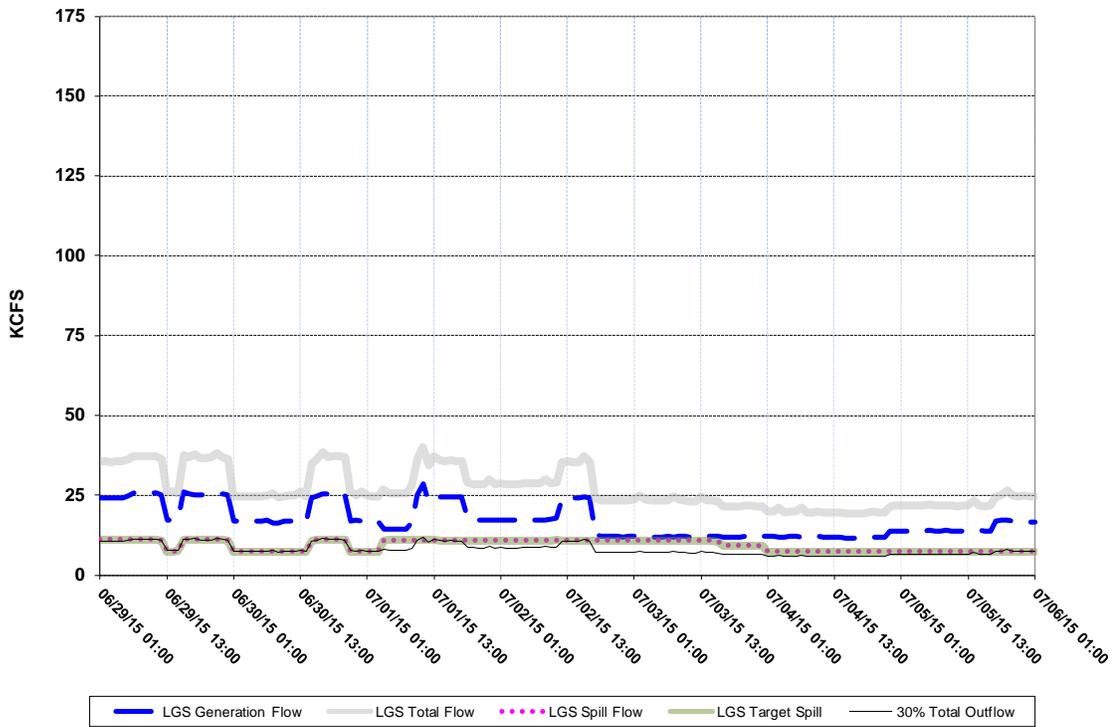


Figure 3

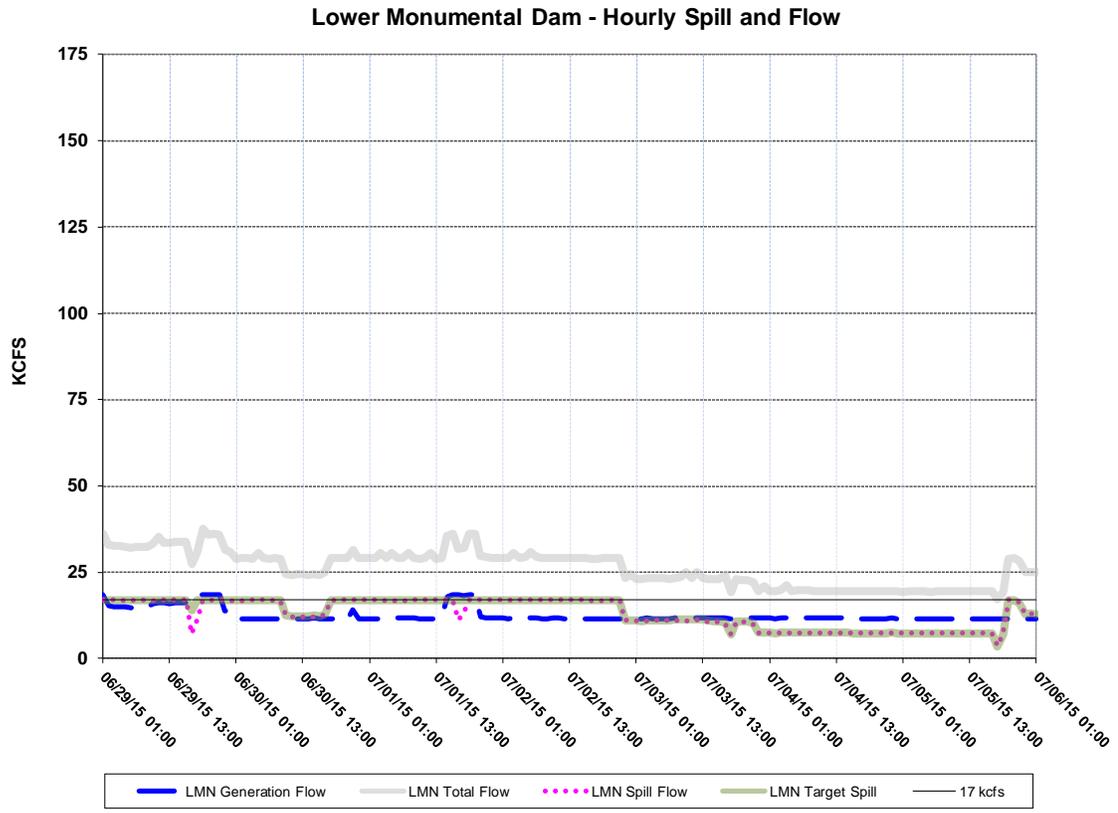
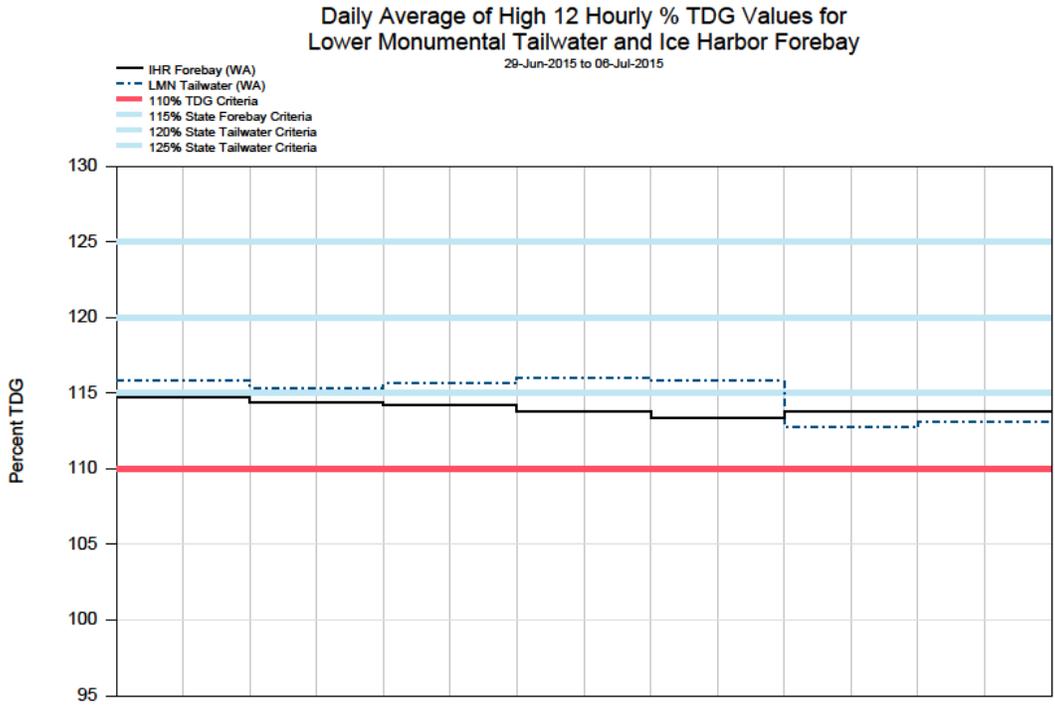


Figure 4

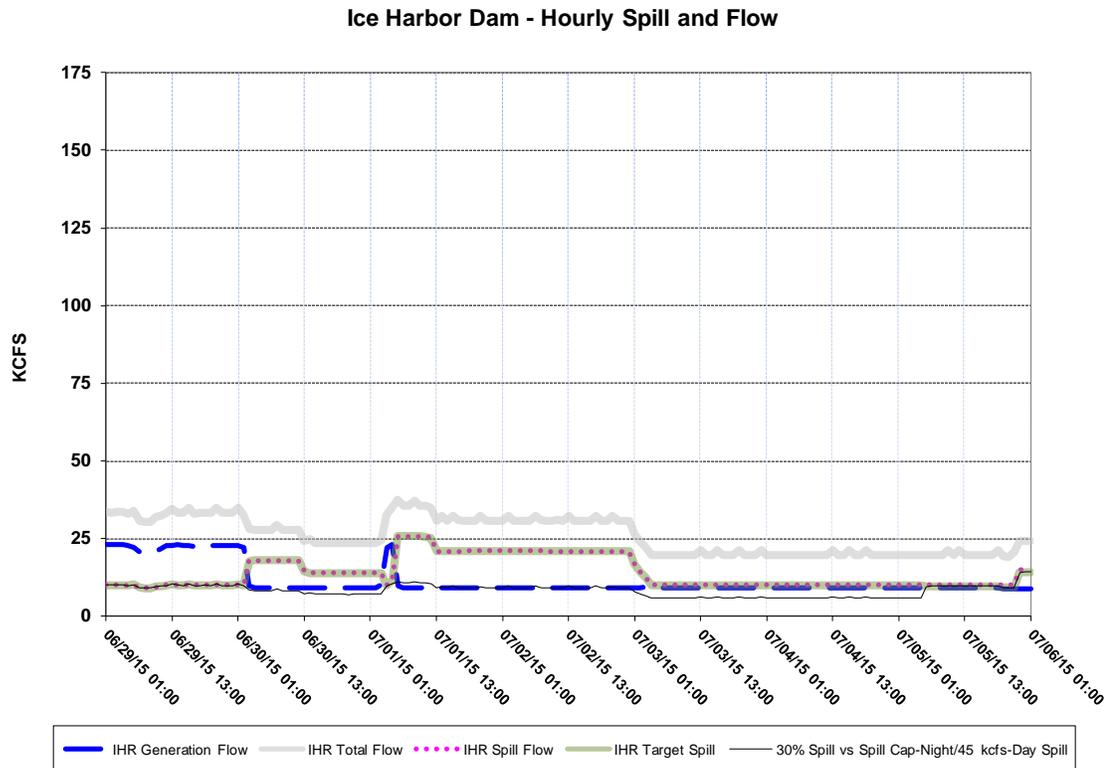
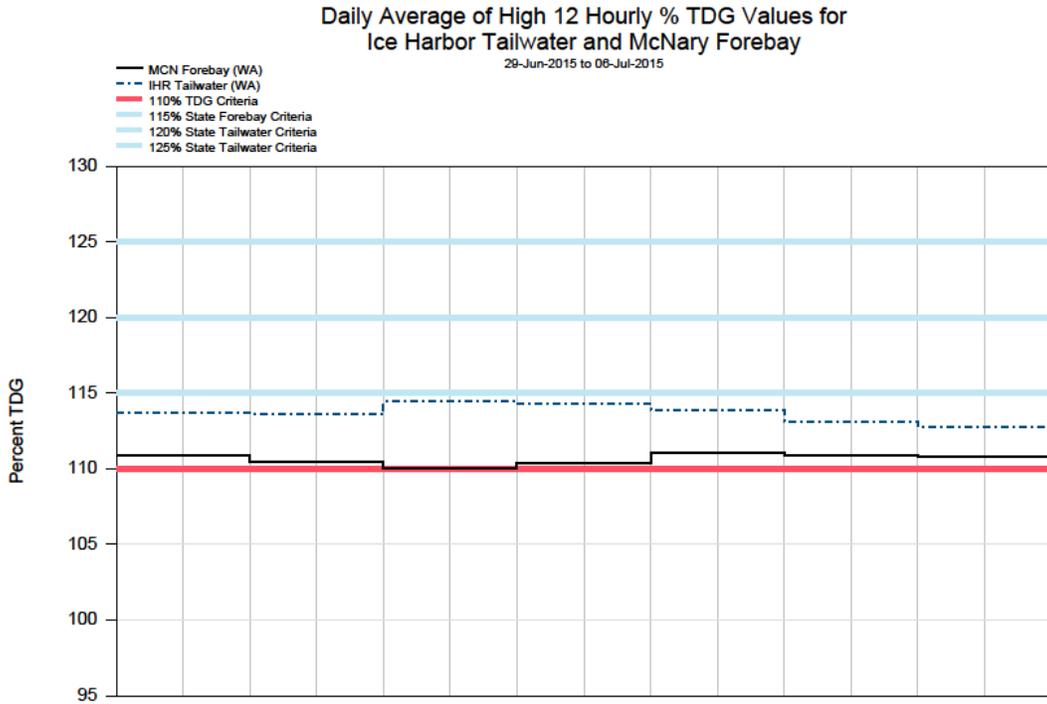


Figure 5

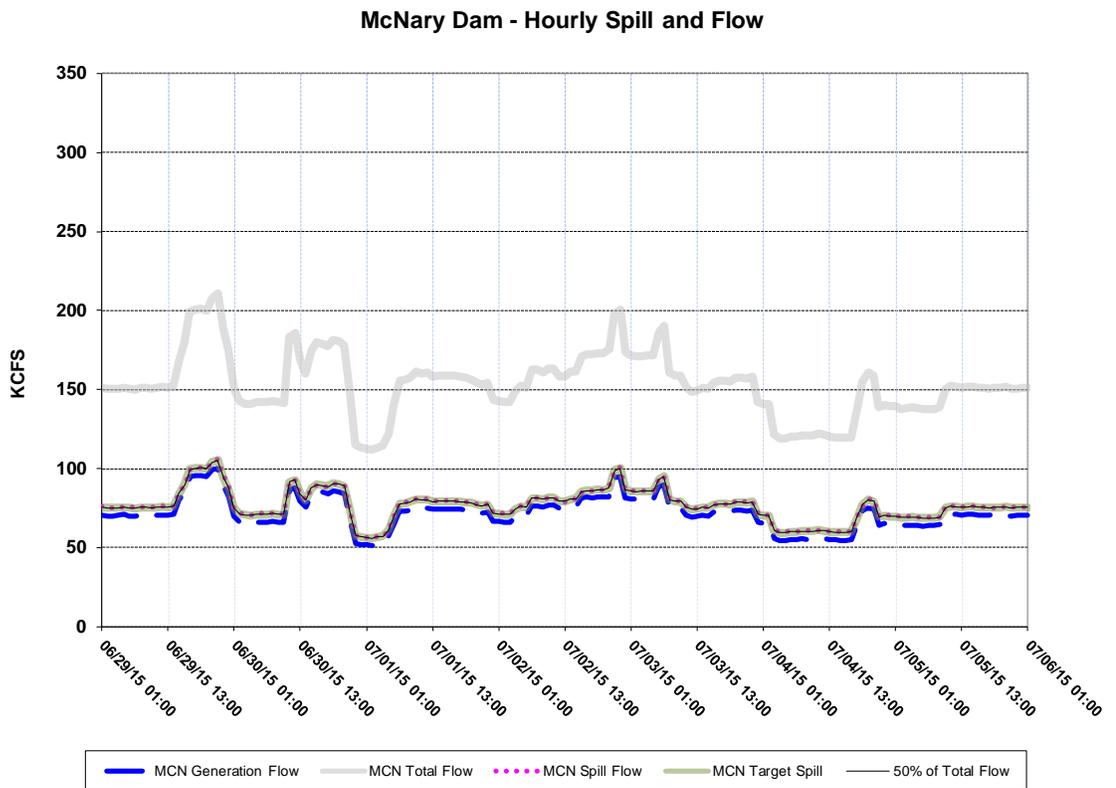
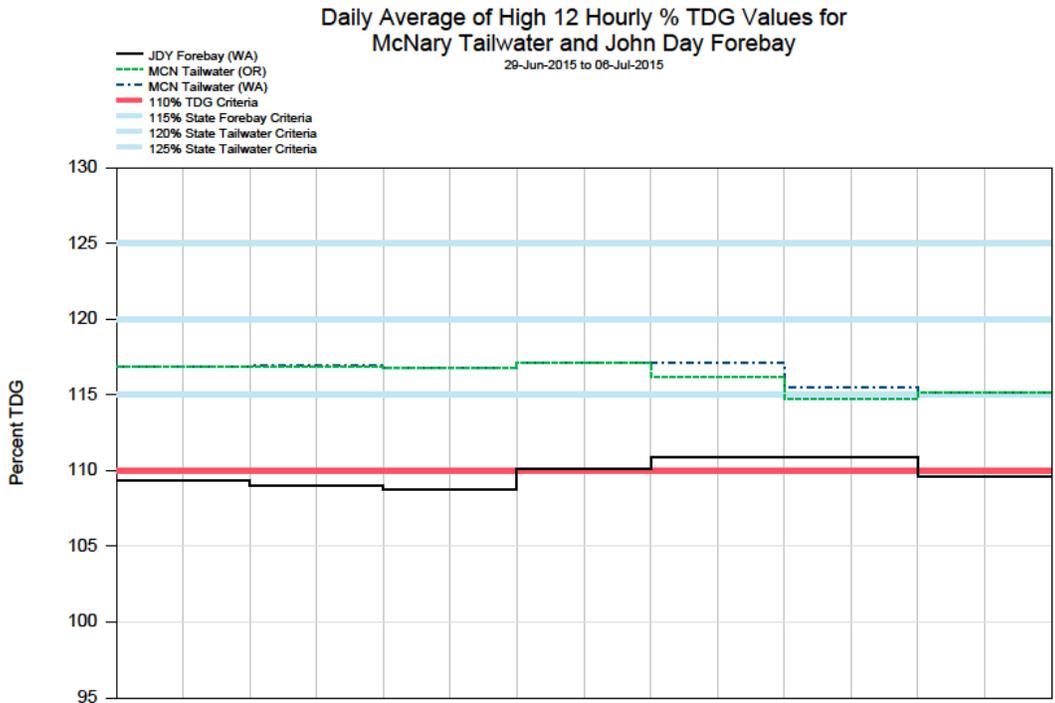
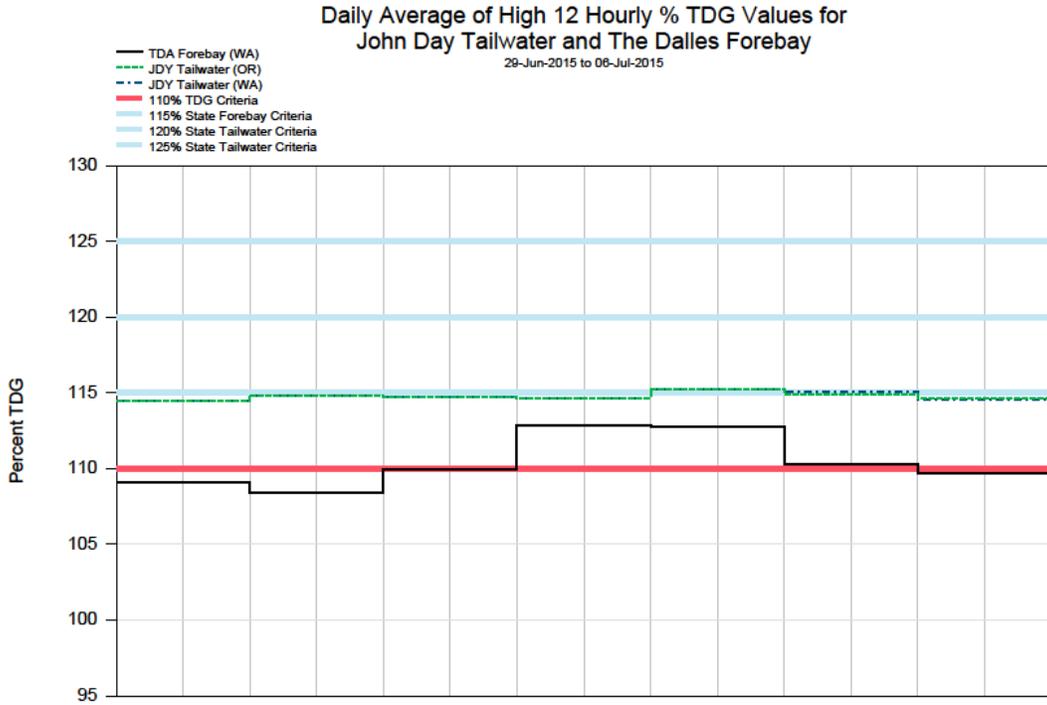


Figure 6



John Day Dam - Hourly Spill and Flow

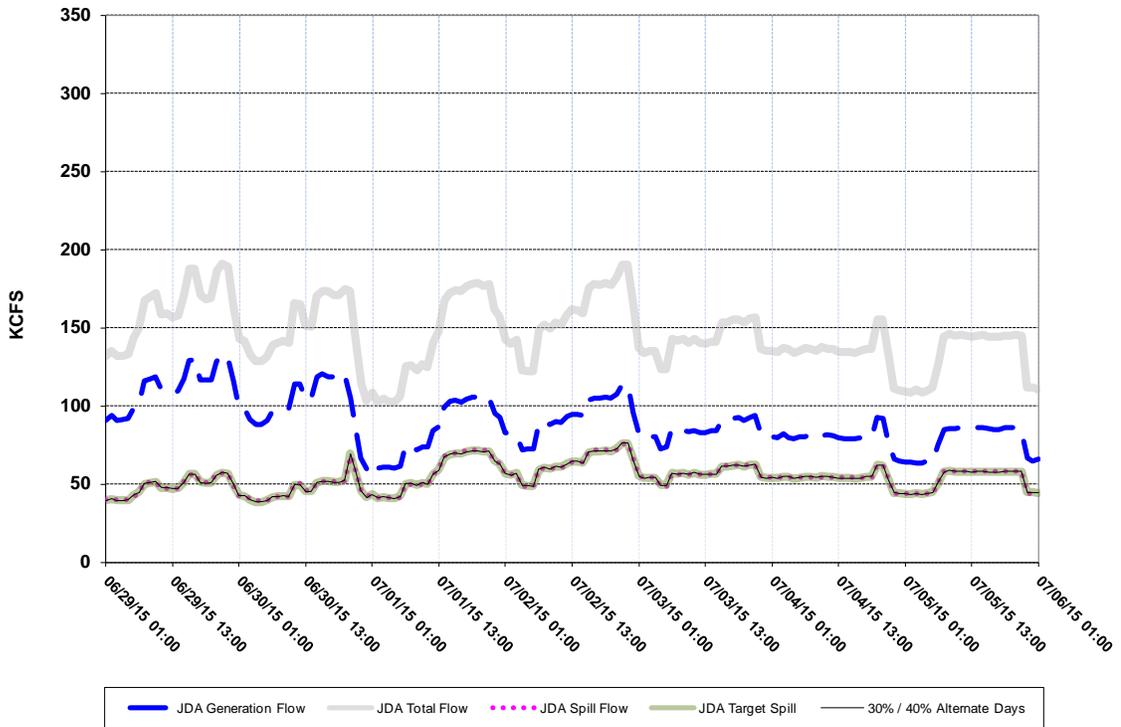


Figure 7

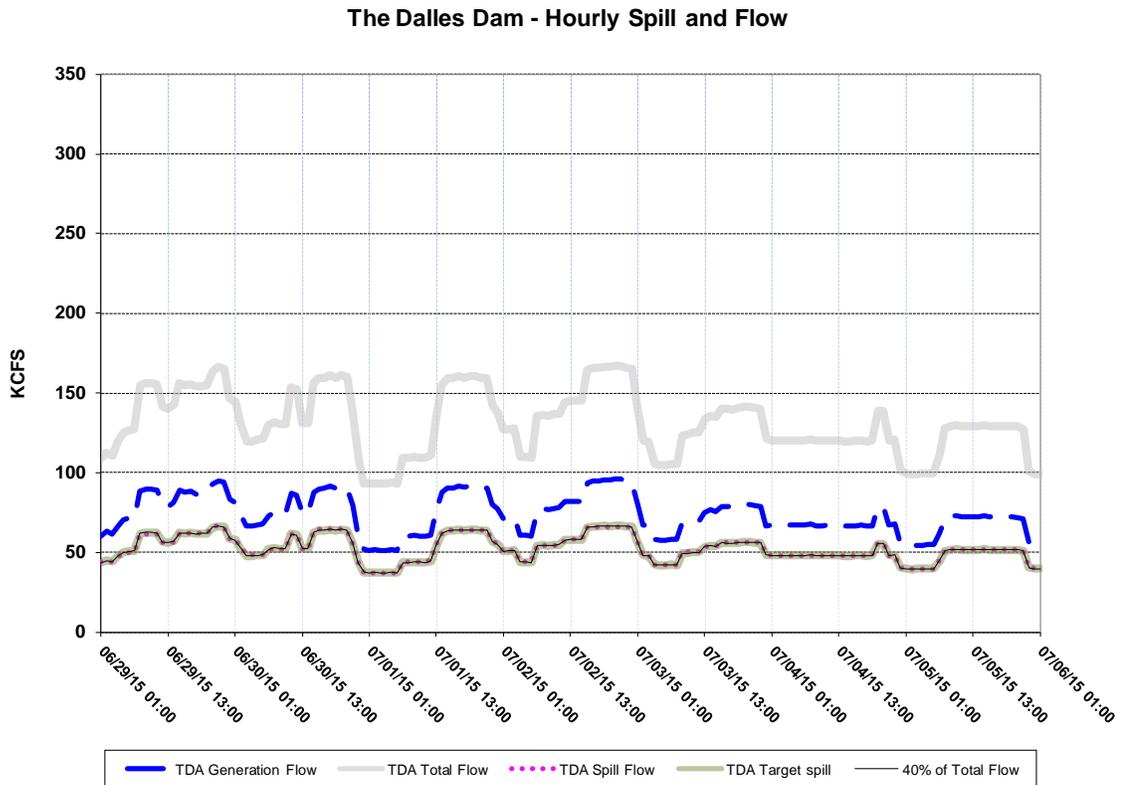
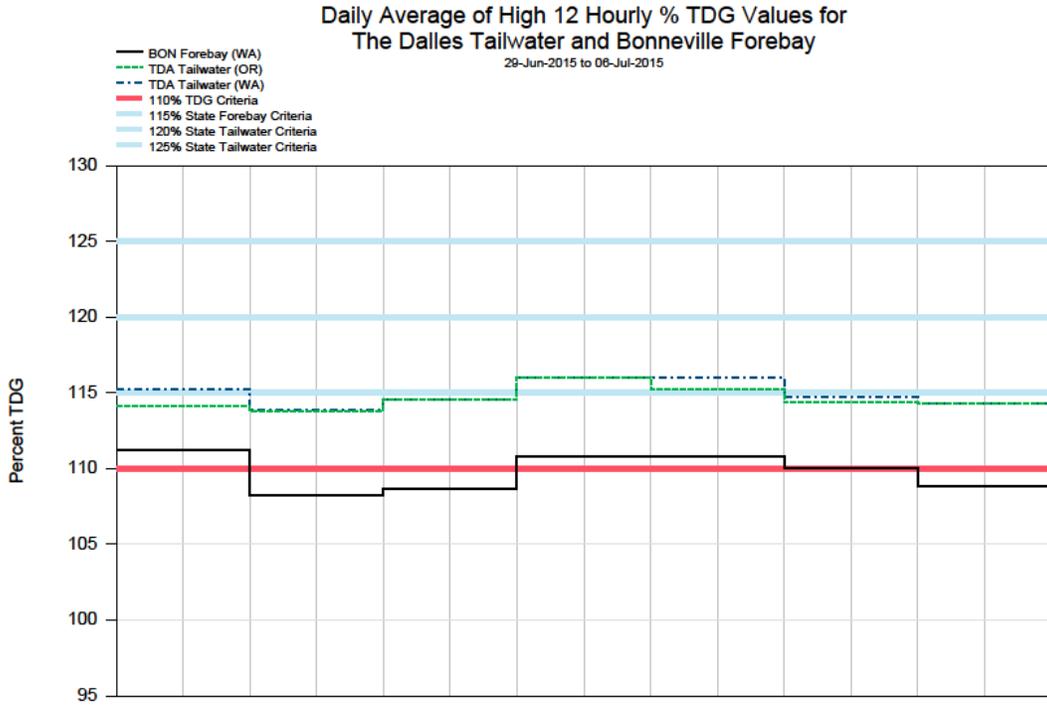
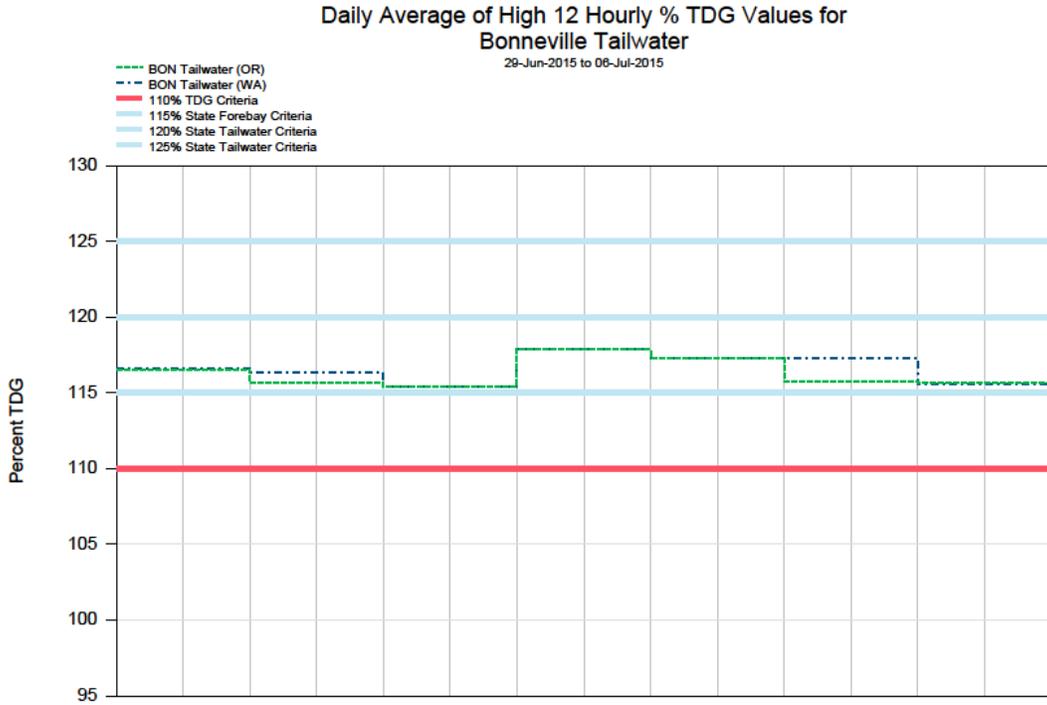


Figure 8



Bonneville Dam - Hourly Spill and Flow

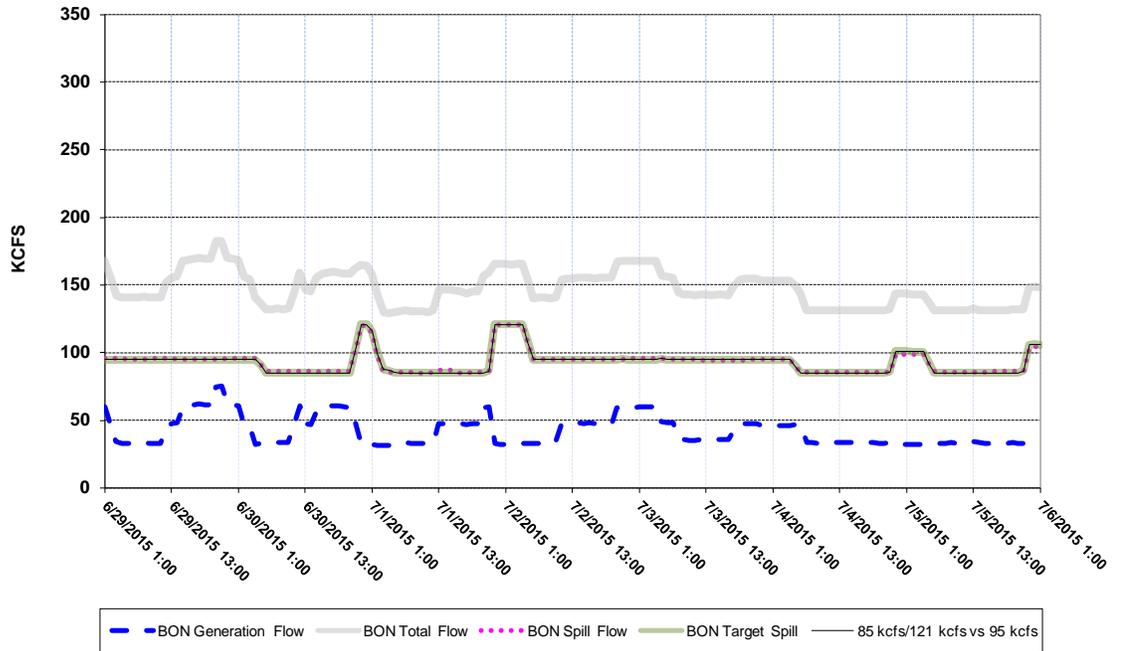


Figure 9

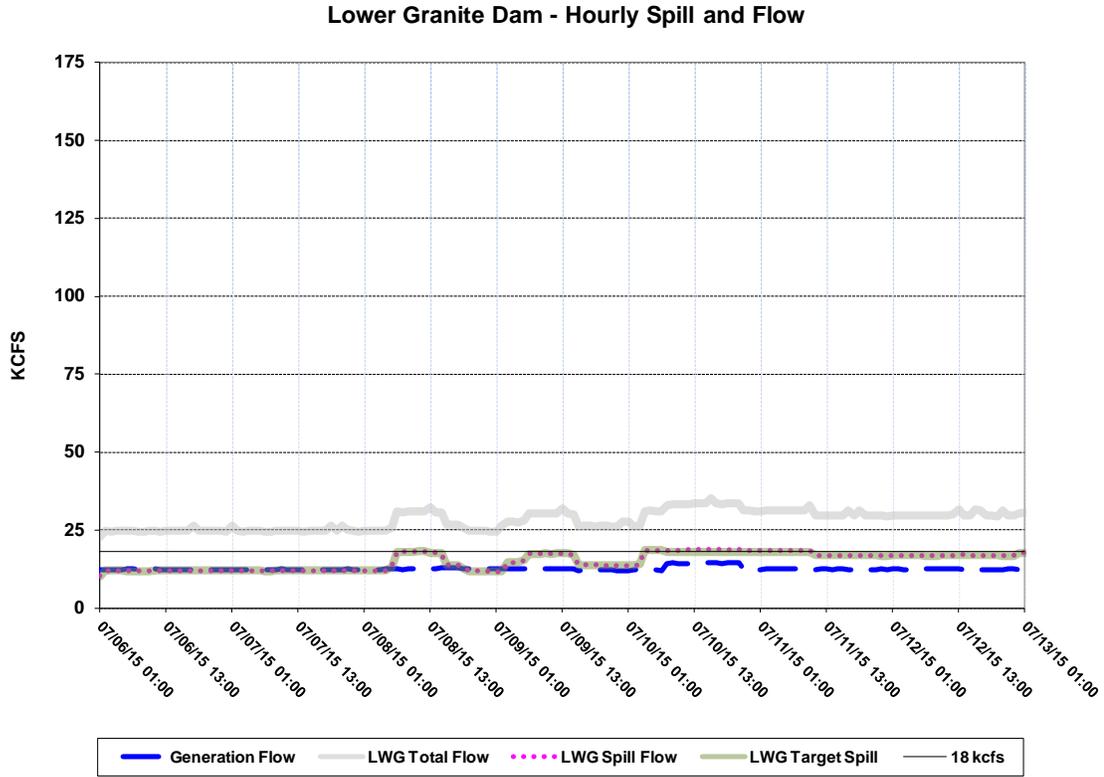
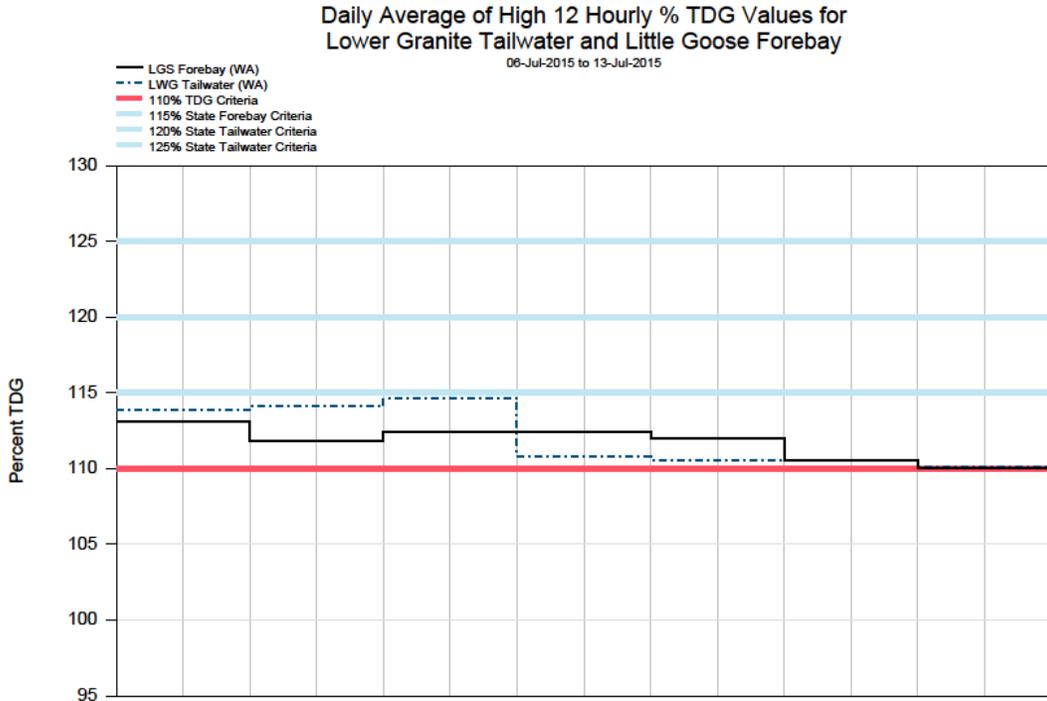


Figure 10

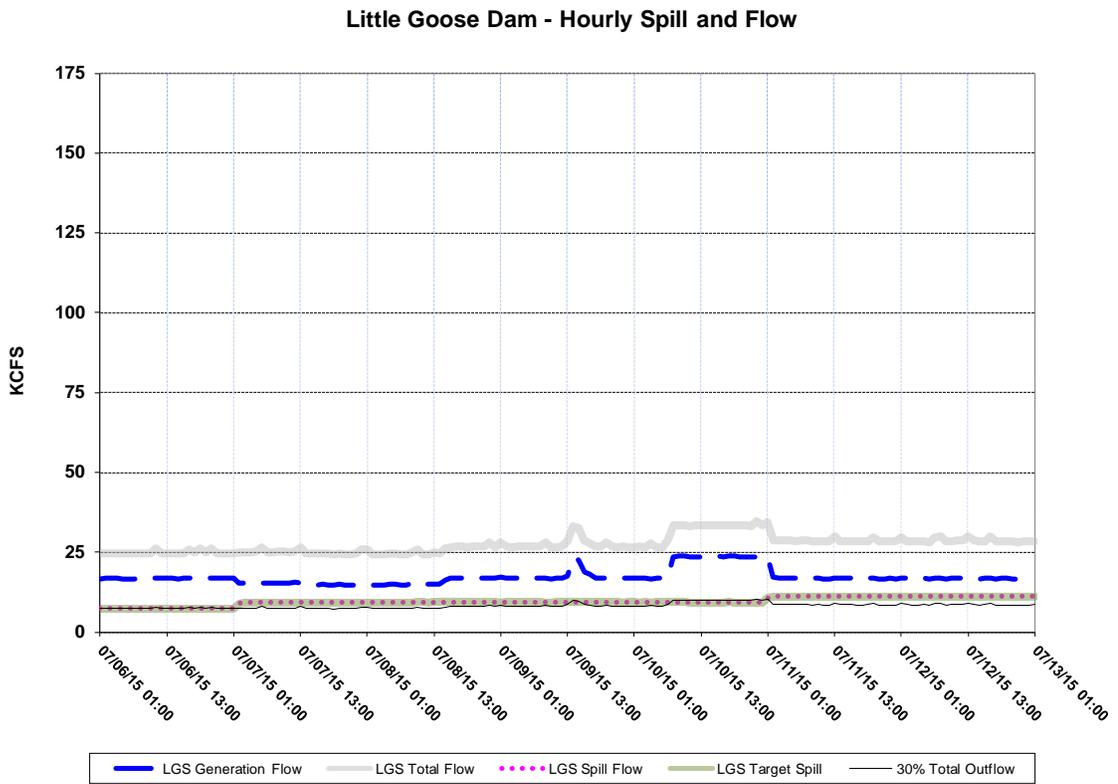
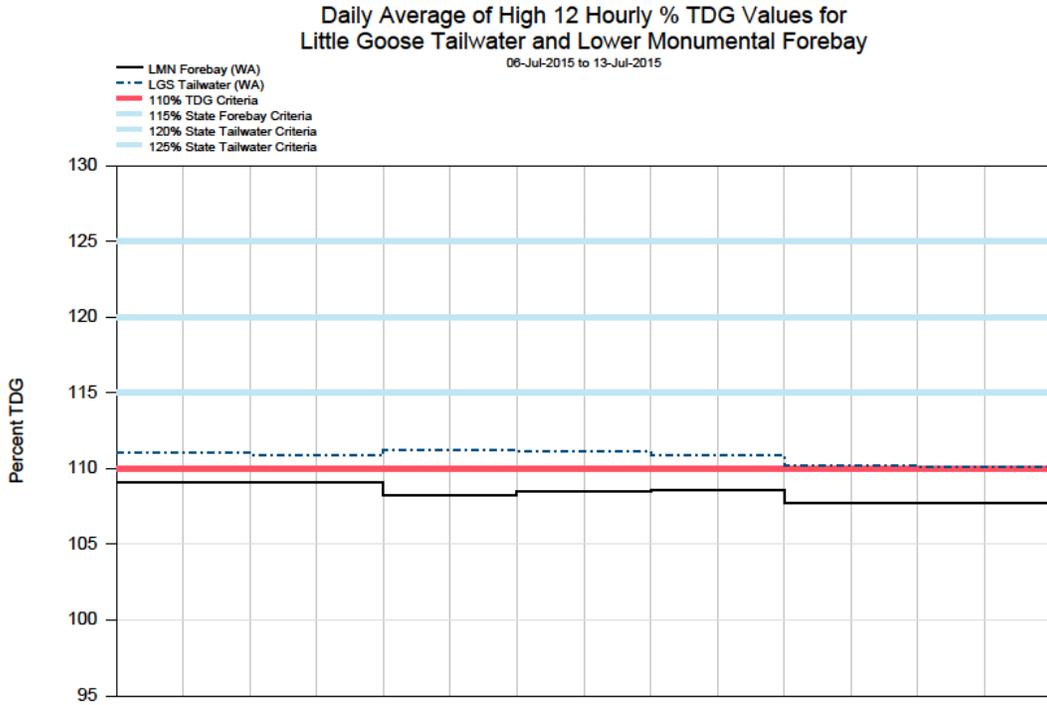


Figure 11

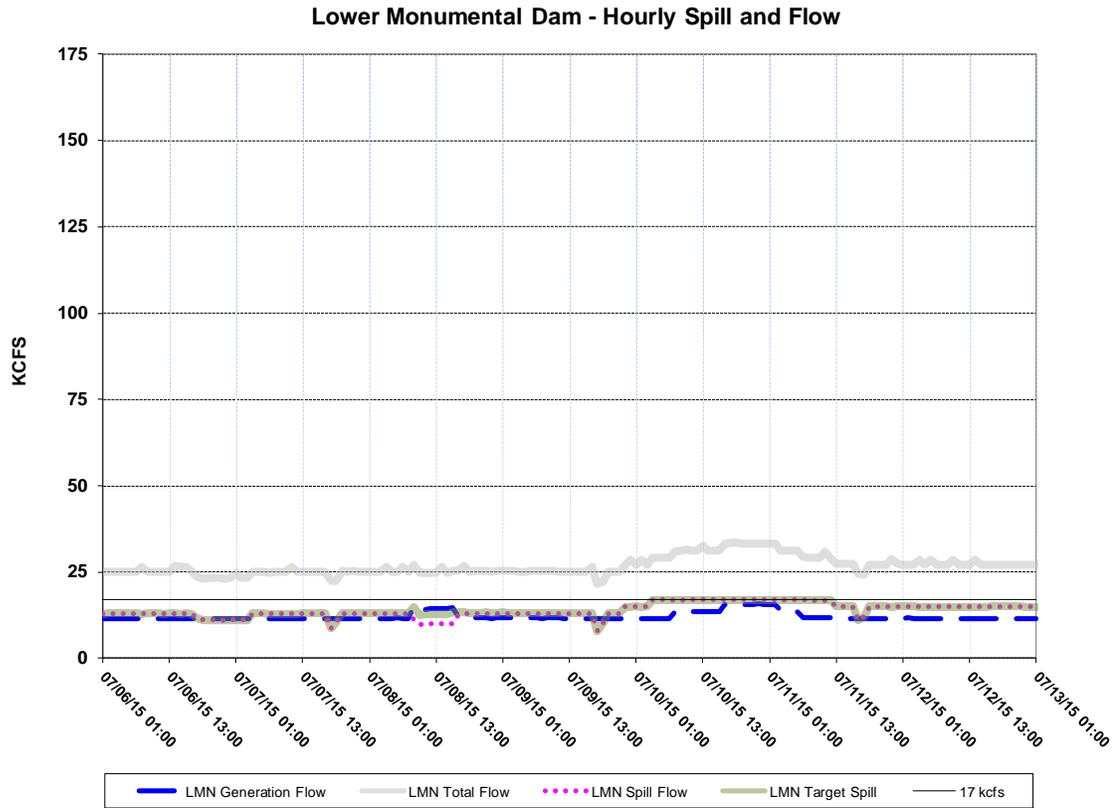
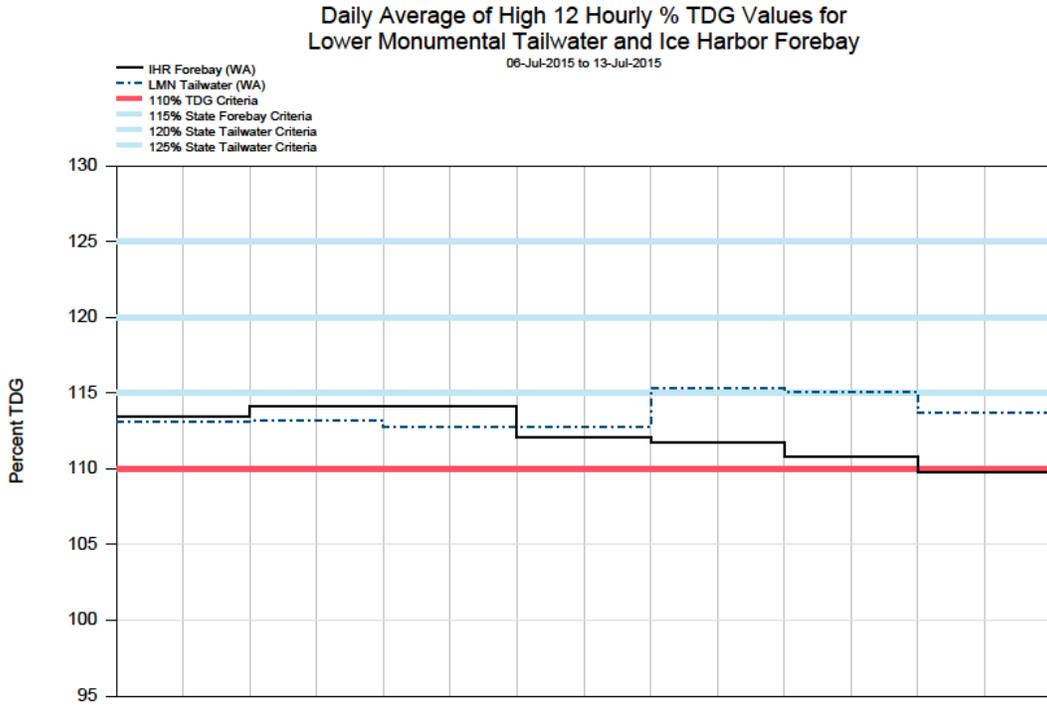
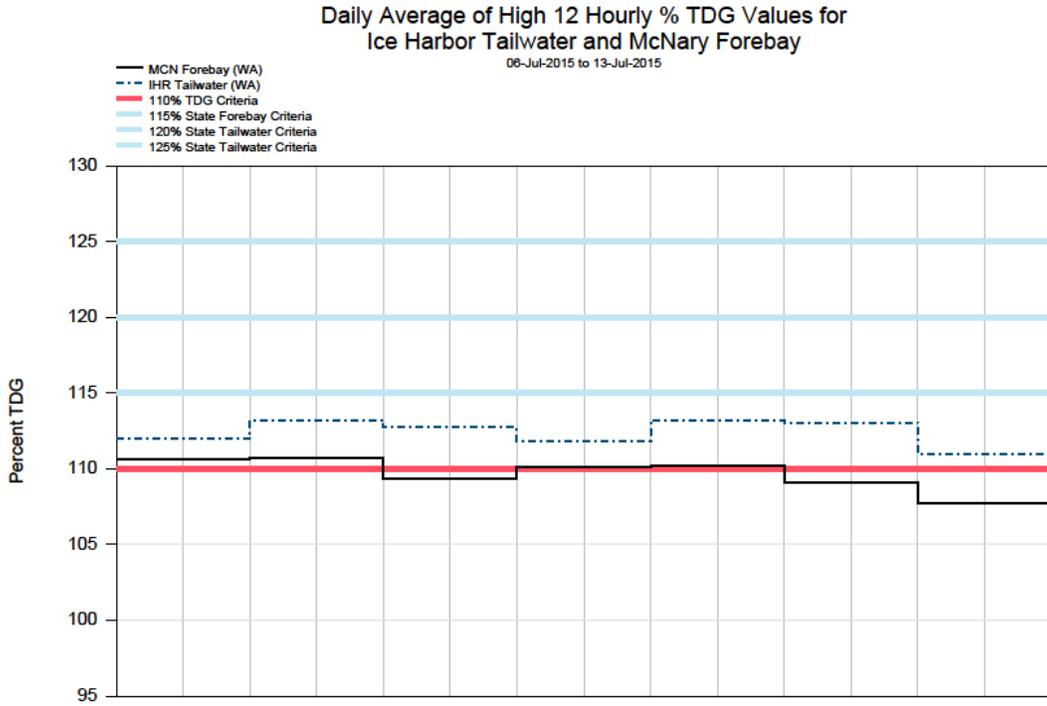


Figure 12



Ice Harbor Dam - Hourly Spill and Flow

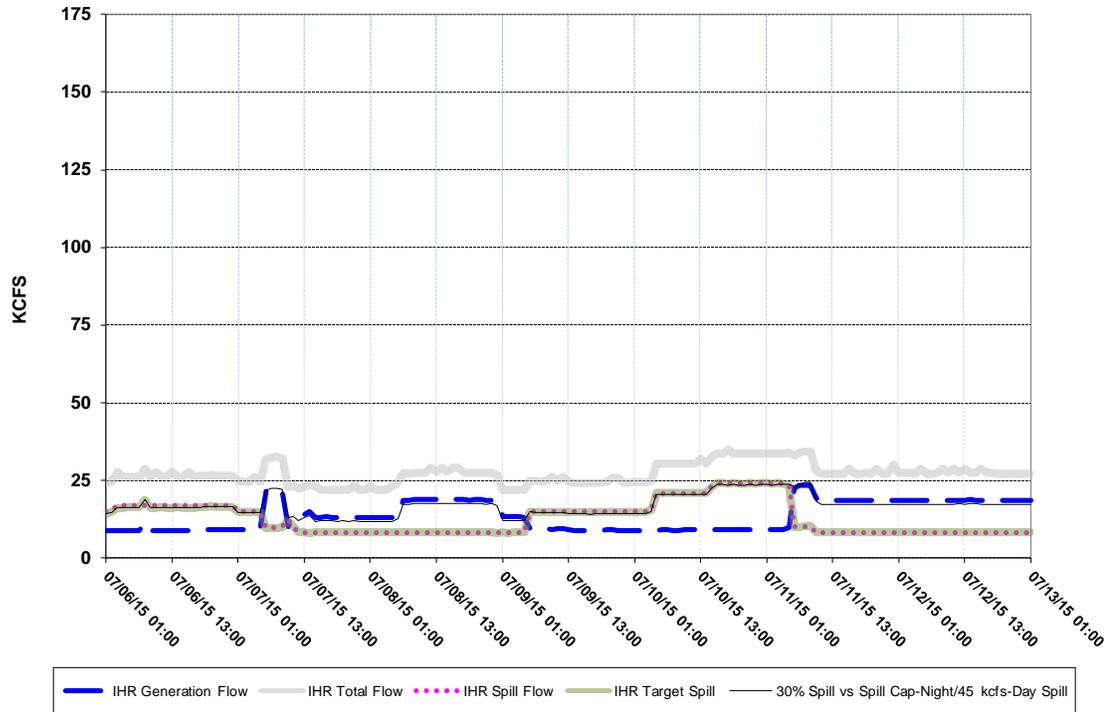
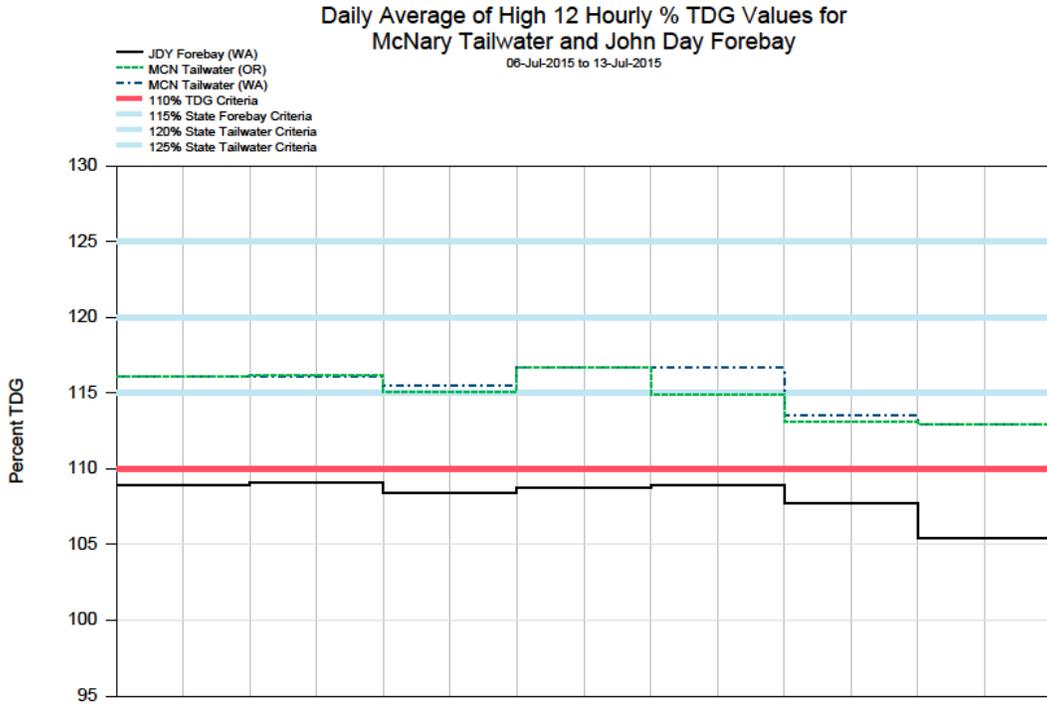


Figure 13



McNary Dam - Hourly Spill and Flow

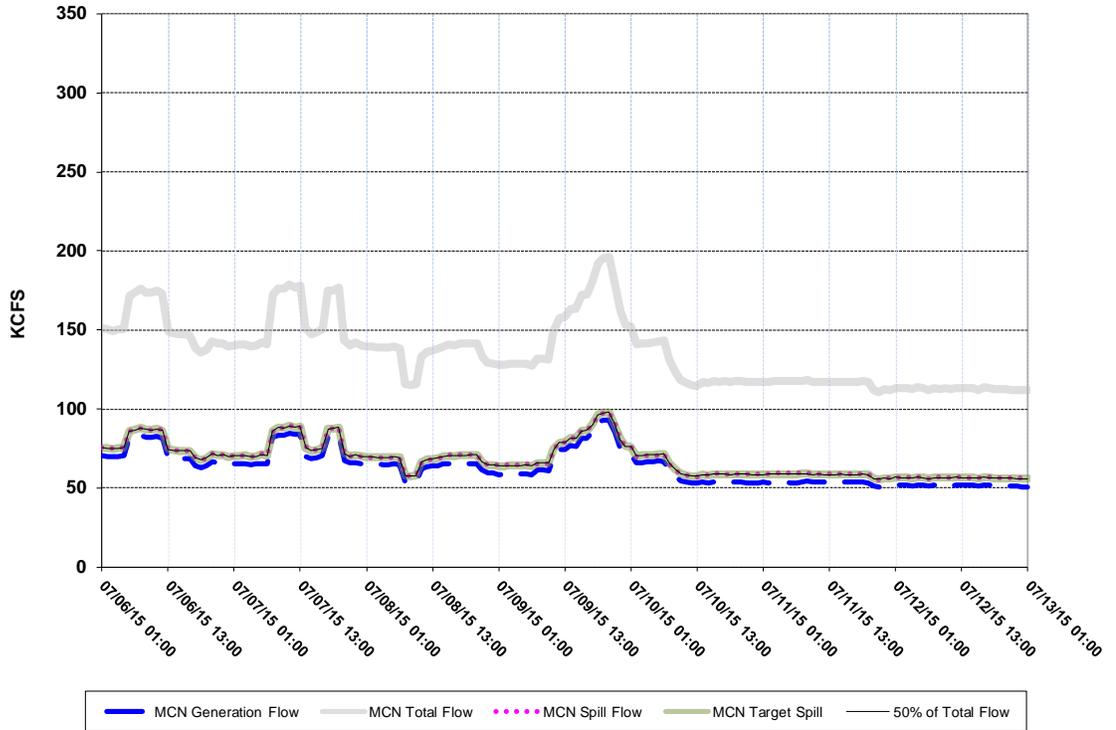
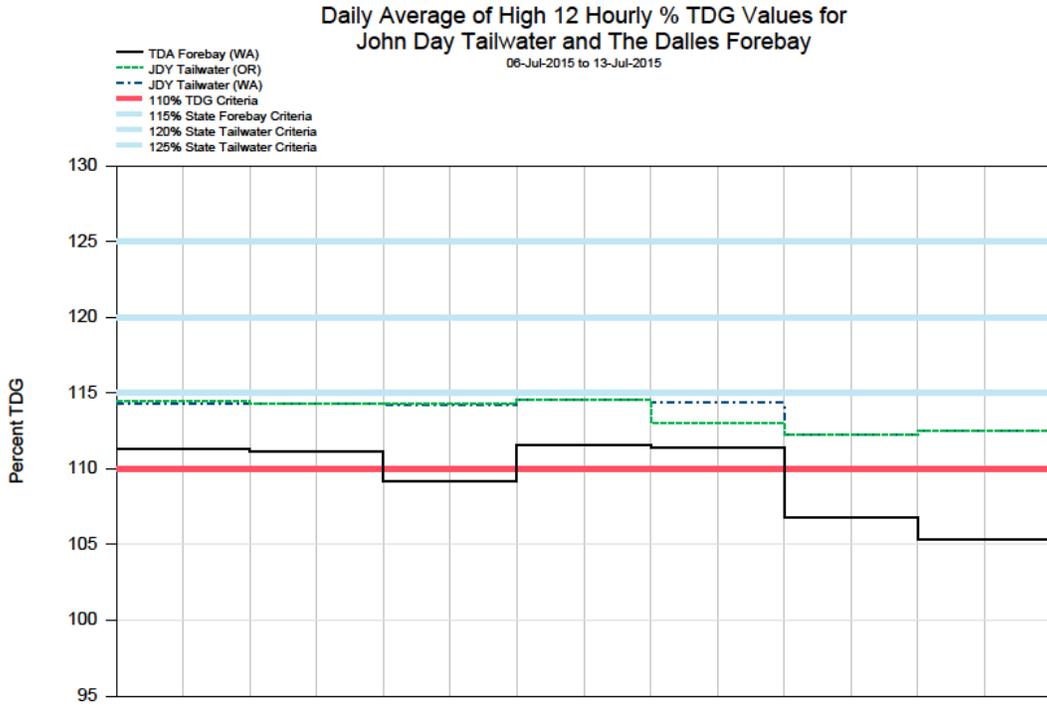


Figure 14



John Day Dam - Hourly Spill and Flow

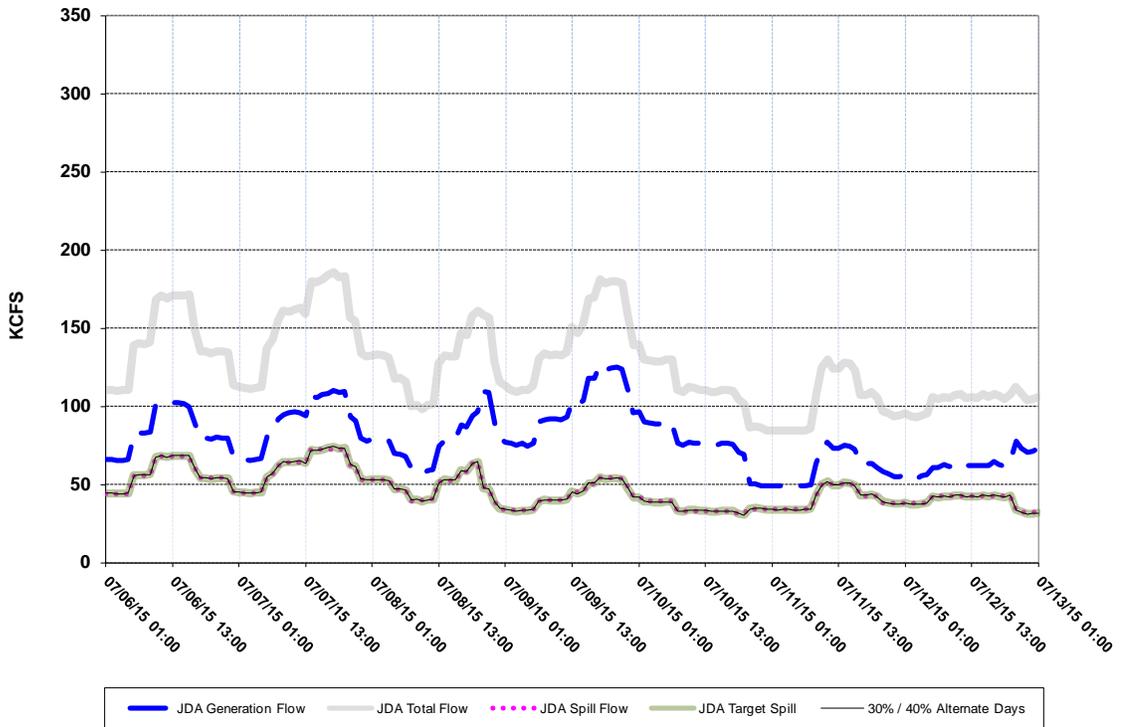
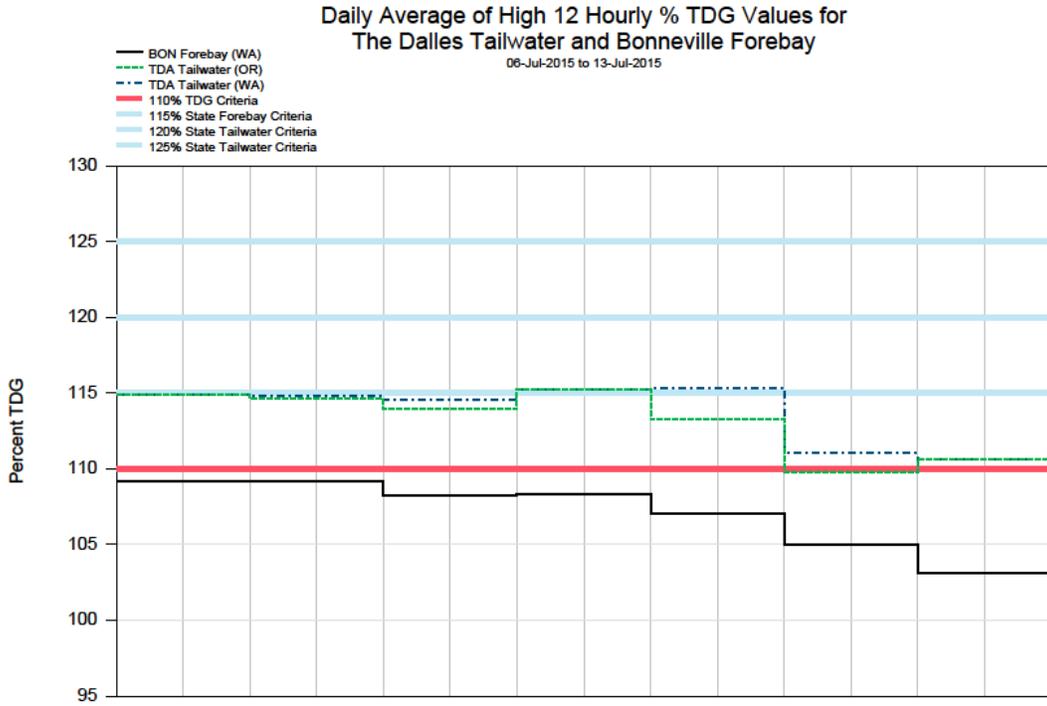


Figure 15



The Dalles Dam - Hourly Spill and Flow

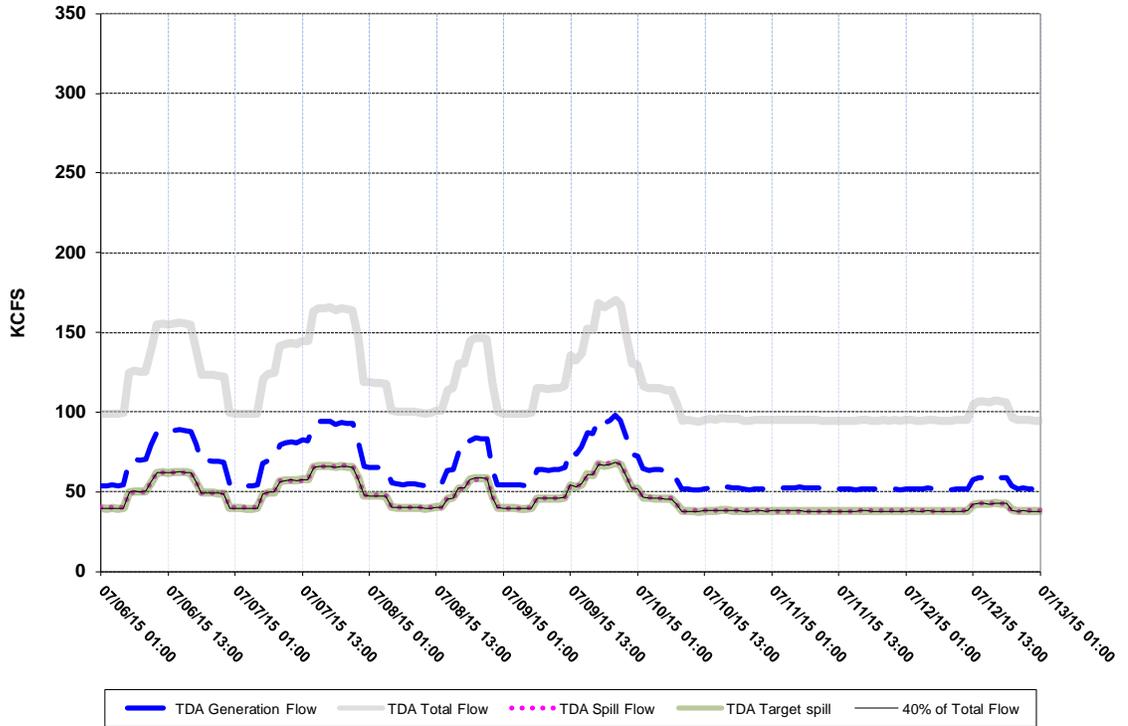


Figure 16

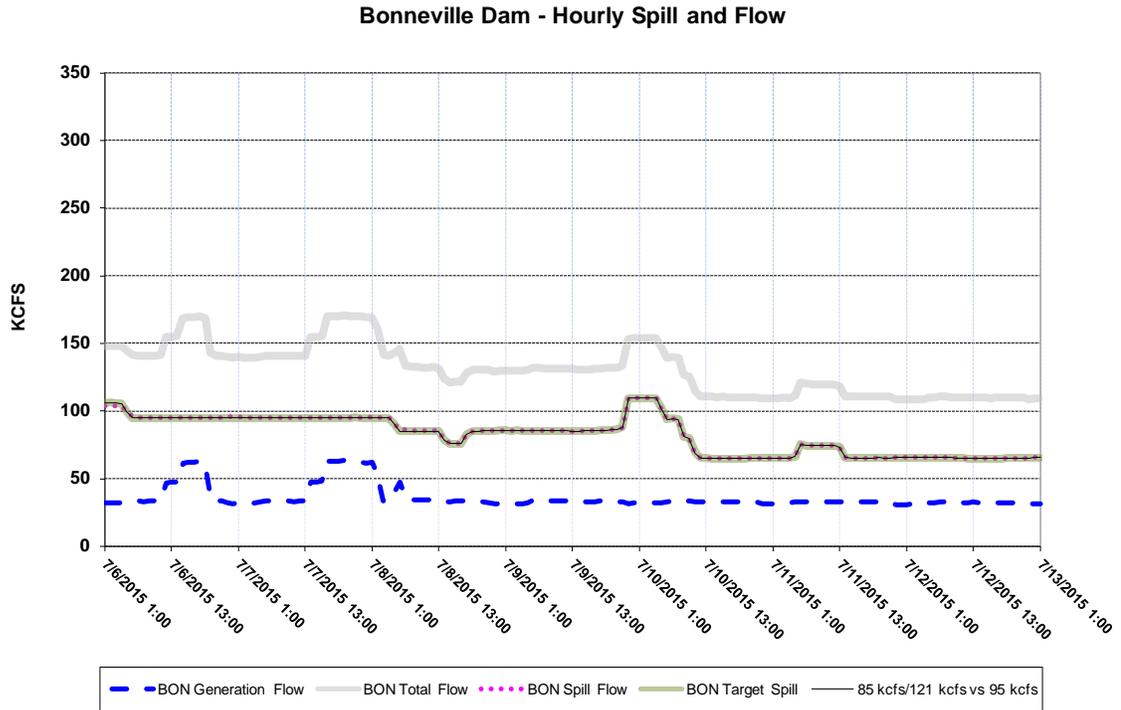
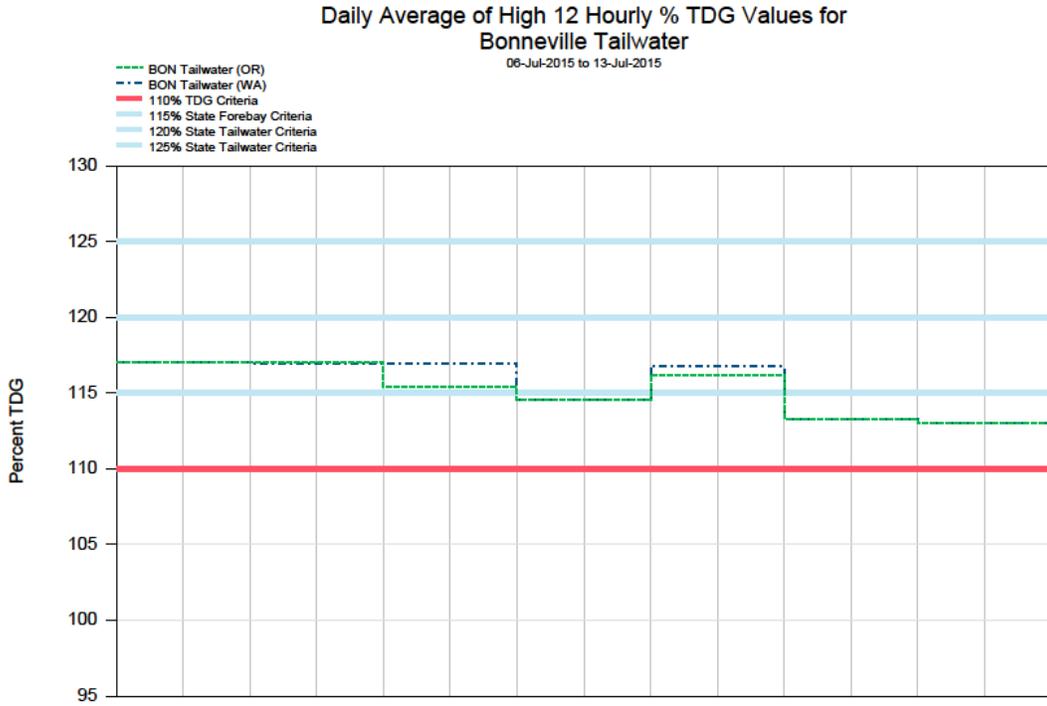


Figure 17

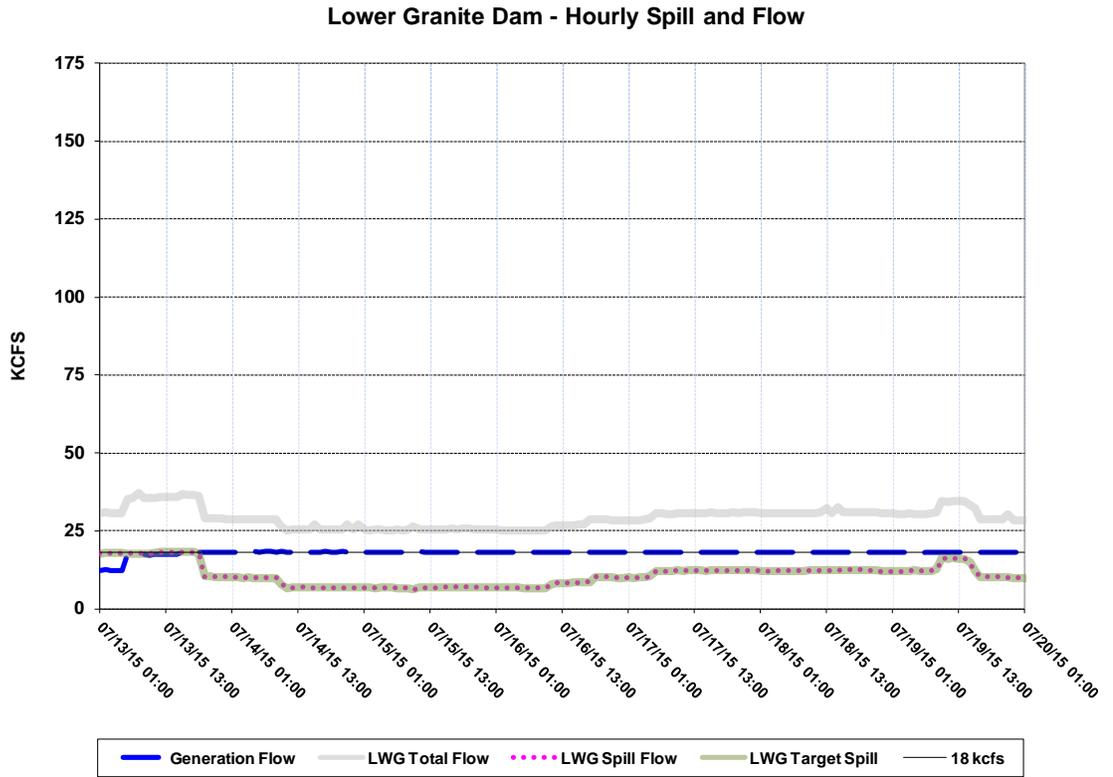
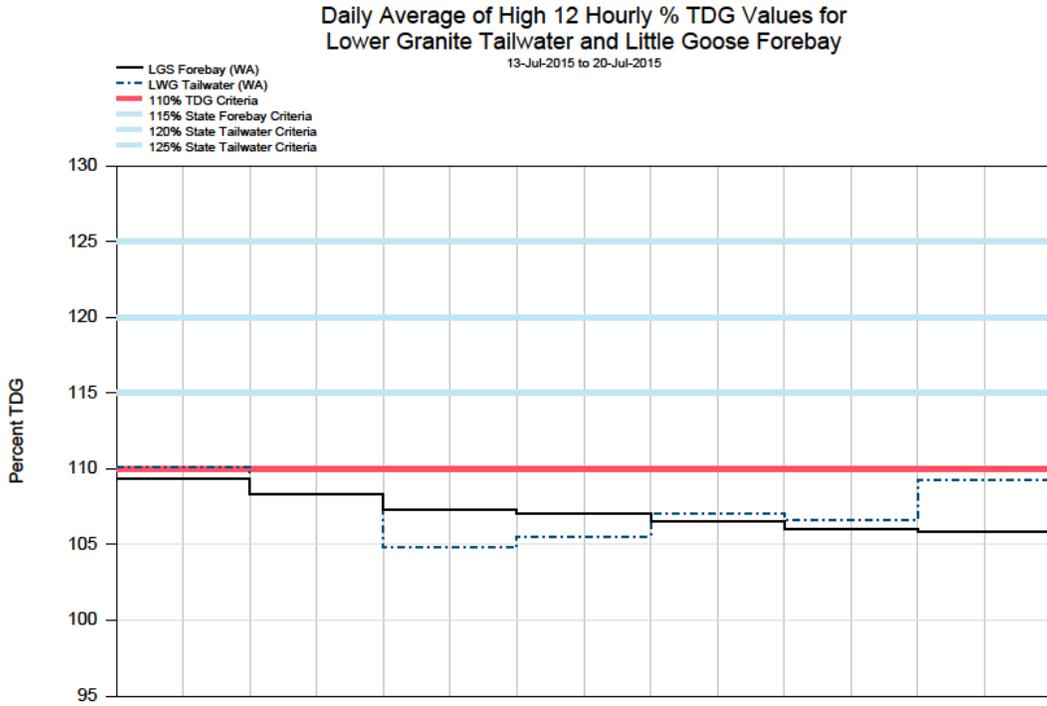


Figure 18

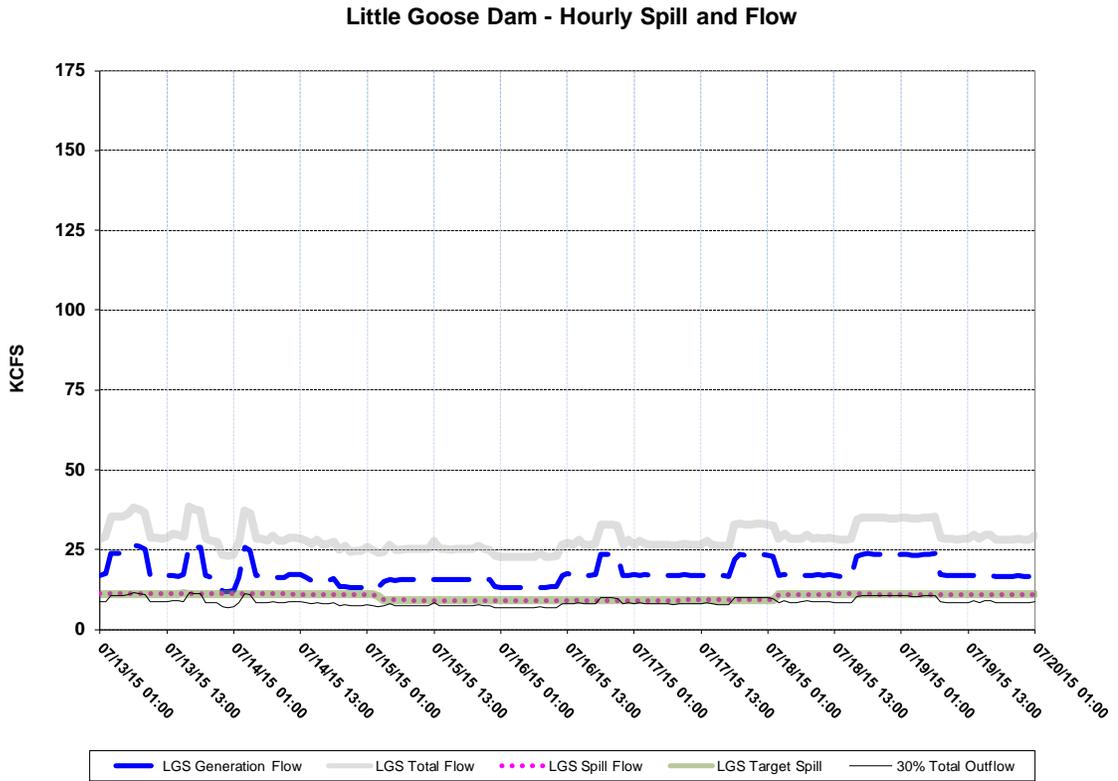
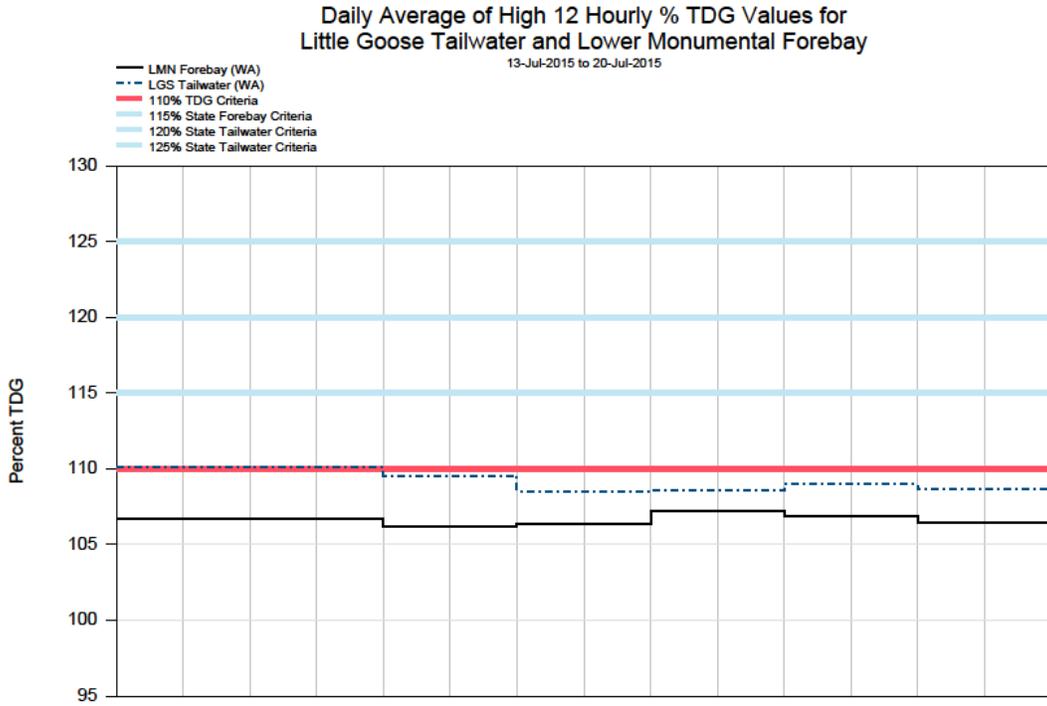


Figure 19

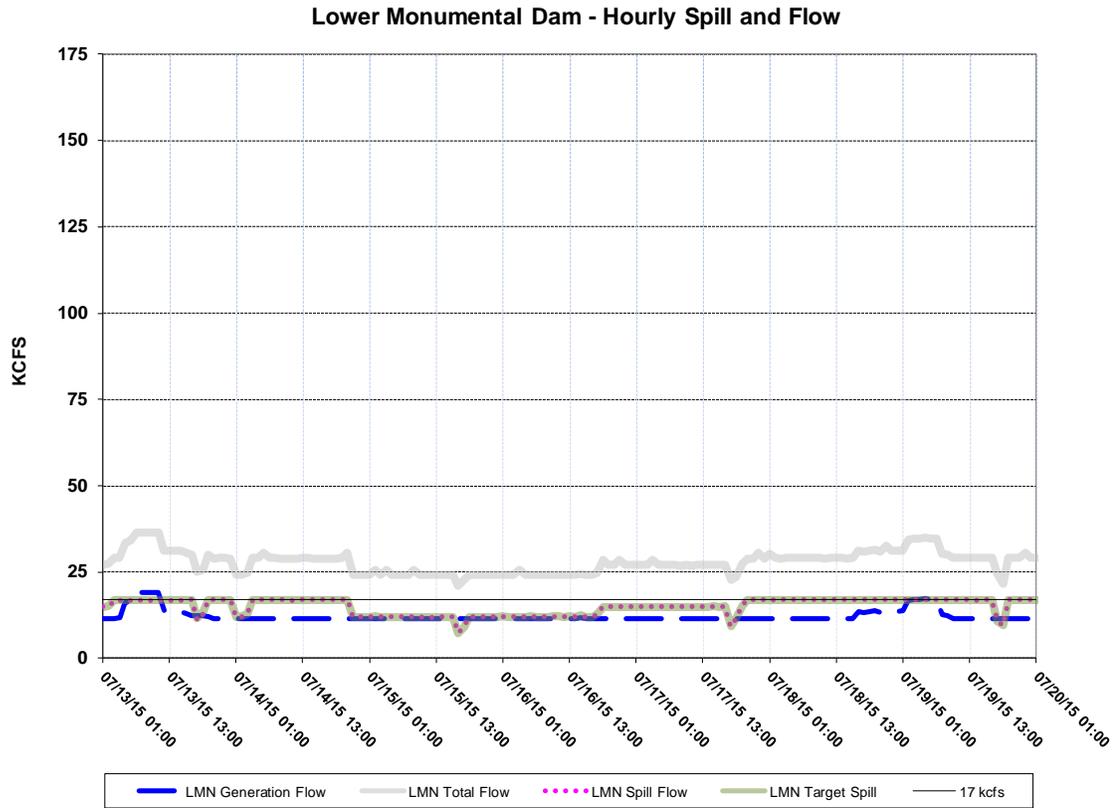
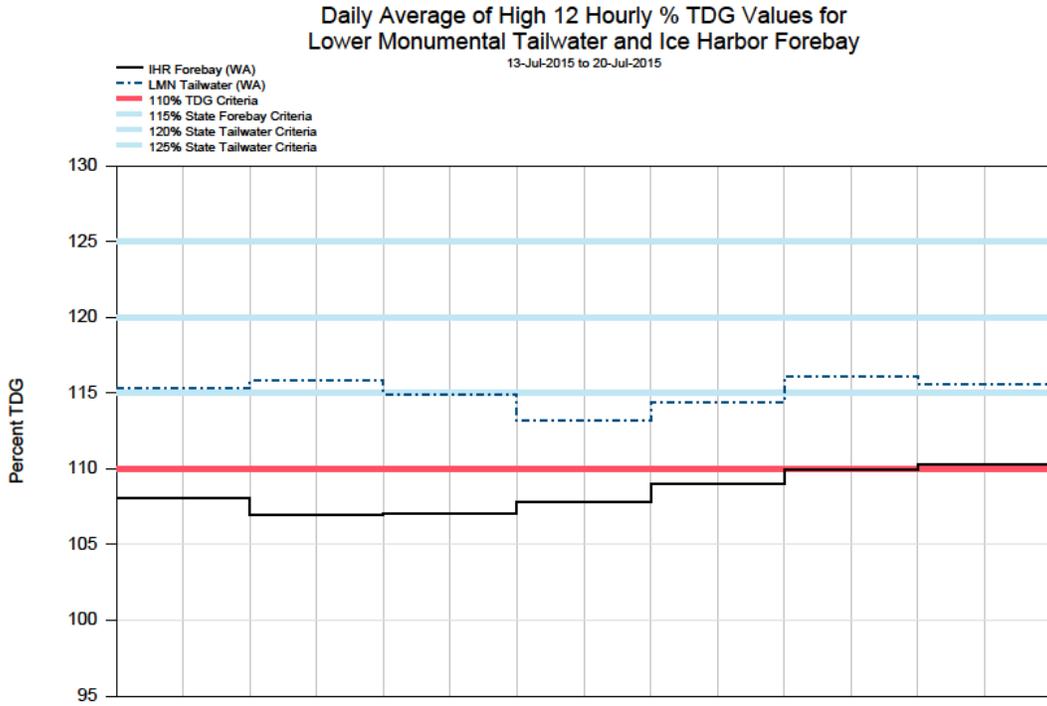
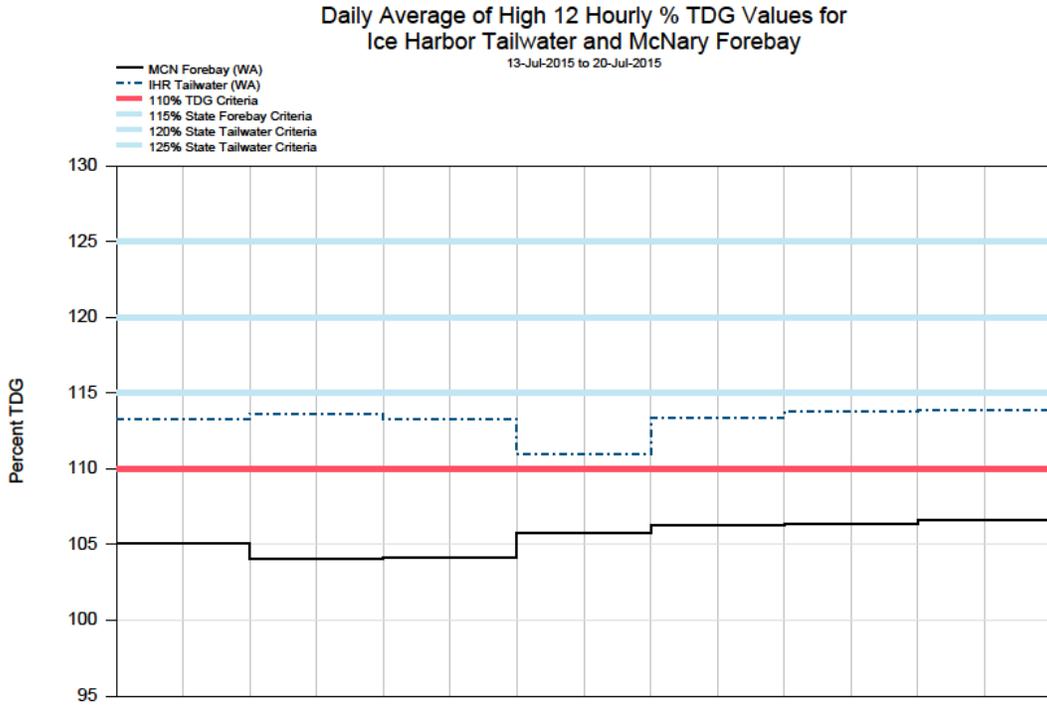


Figure 20



Ice Harbor Dam - Hourly Spill and Flow

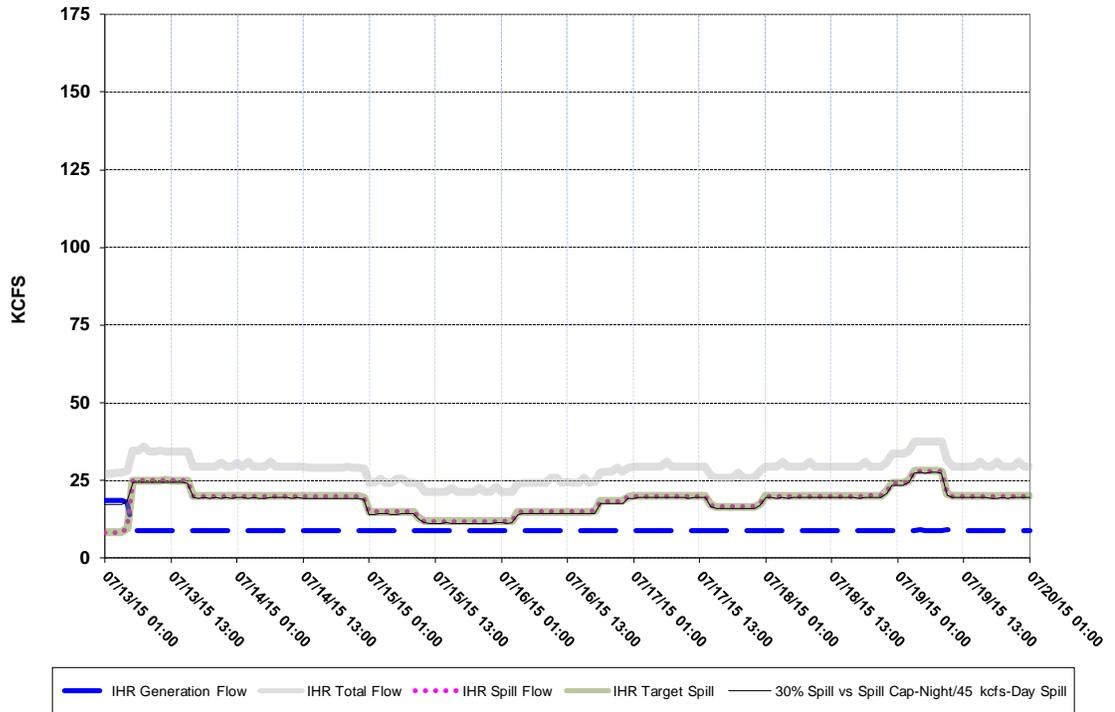
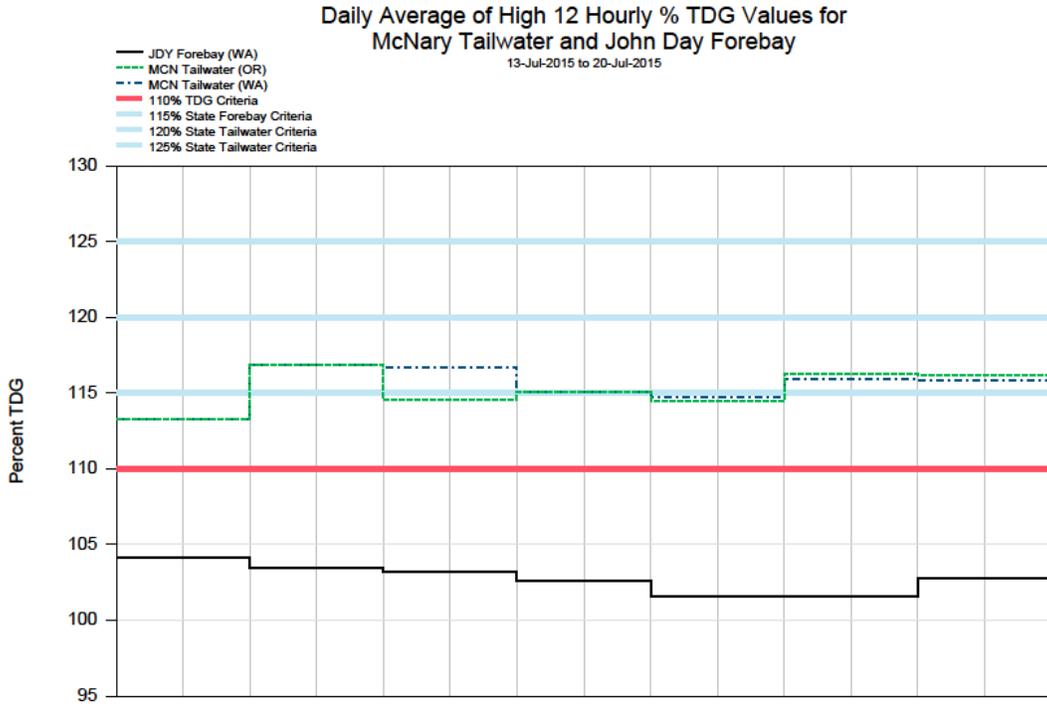


Figure 21



McNary Dam - Hourly Spill and Flow

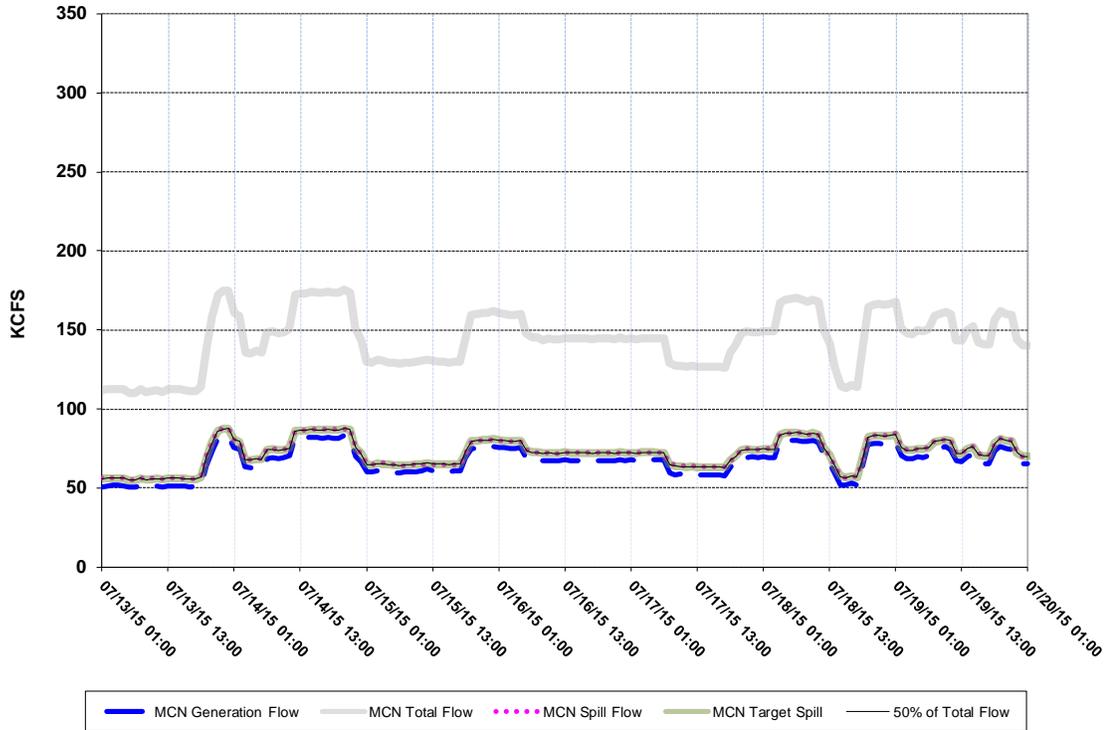
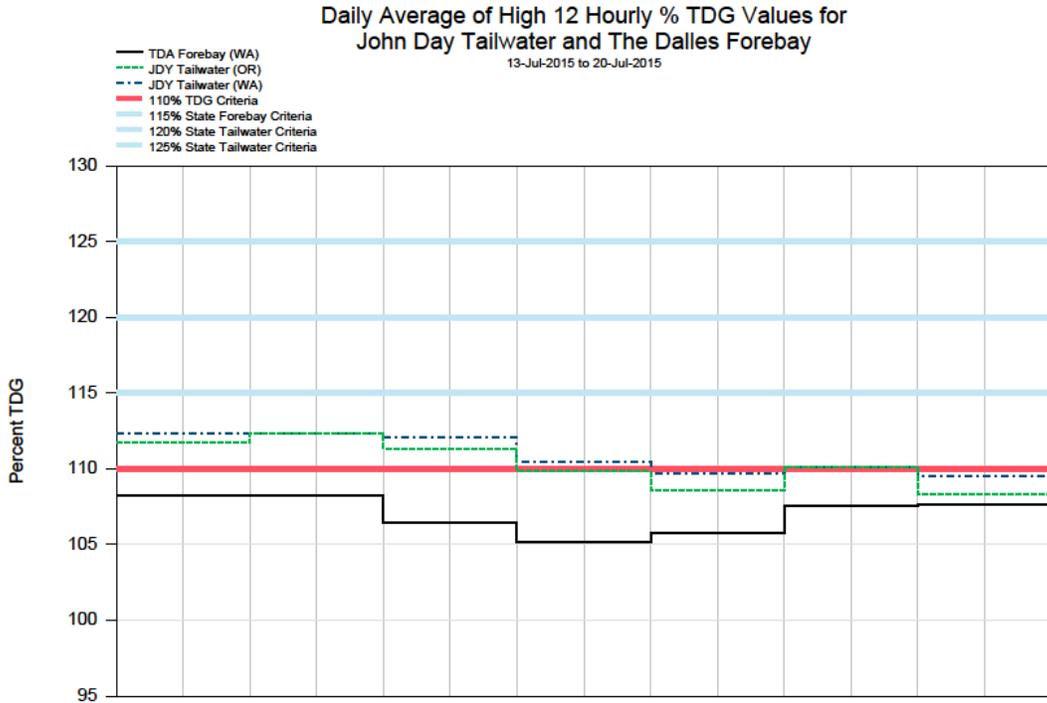


Figure 22



John Day Dam - Hourly Spill and Flow

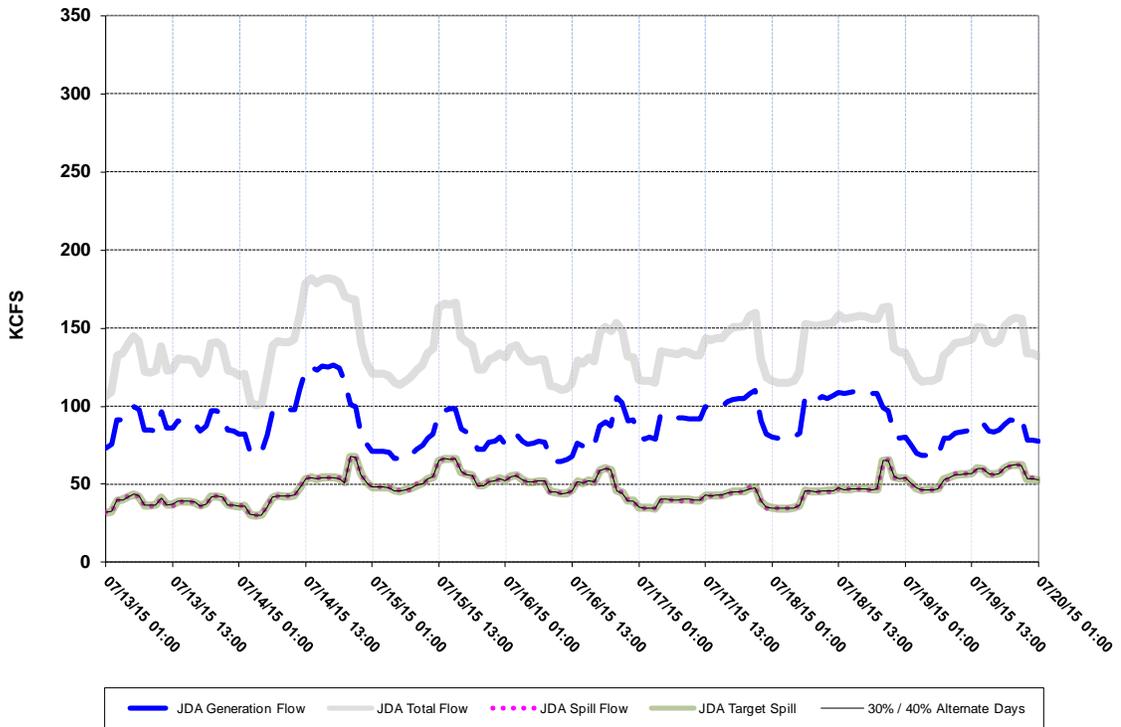
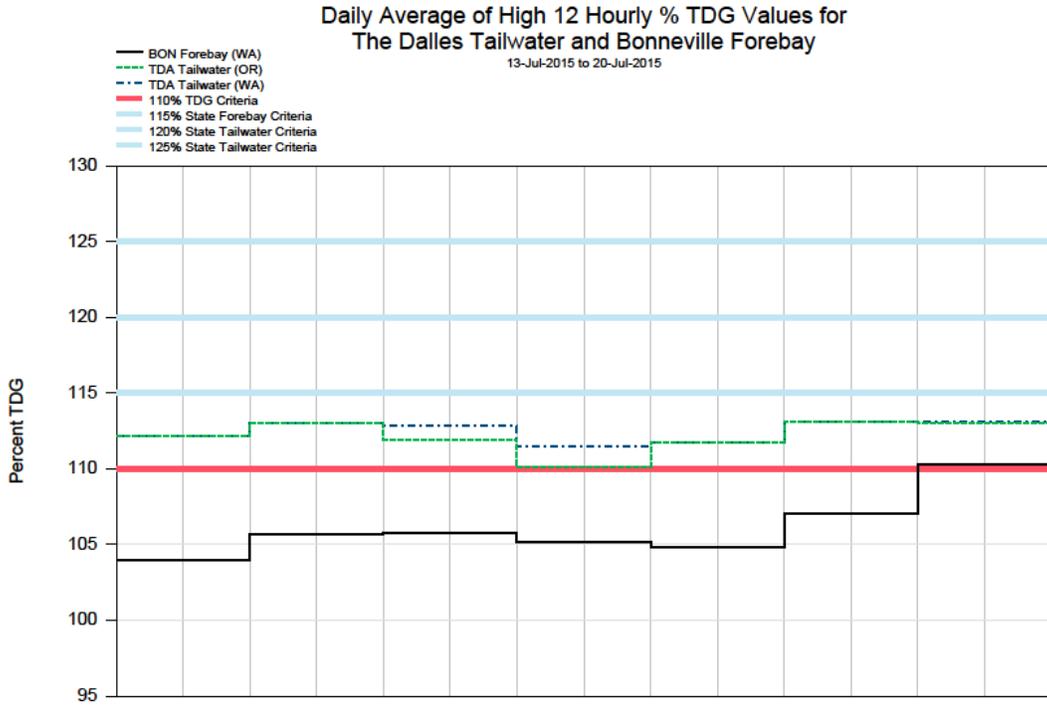


Figure 23



The Dalles Dam - Hourly Spill and Flow

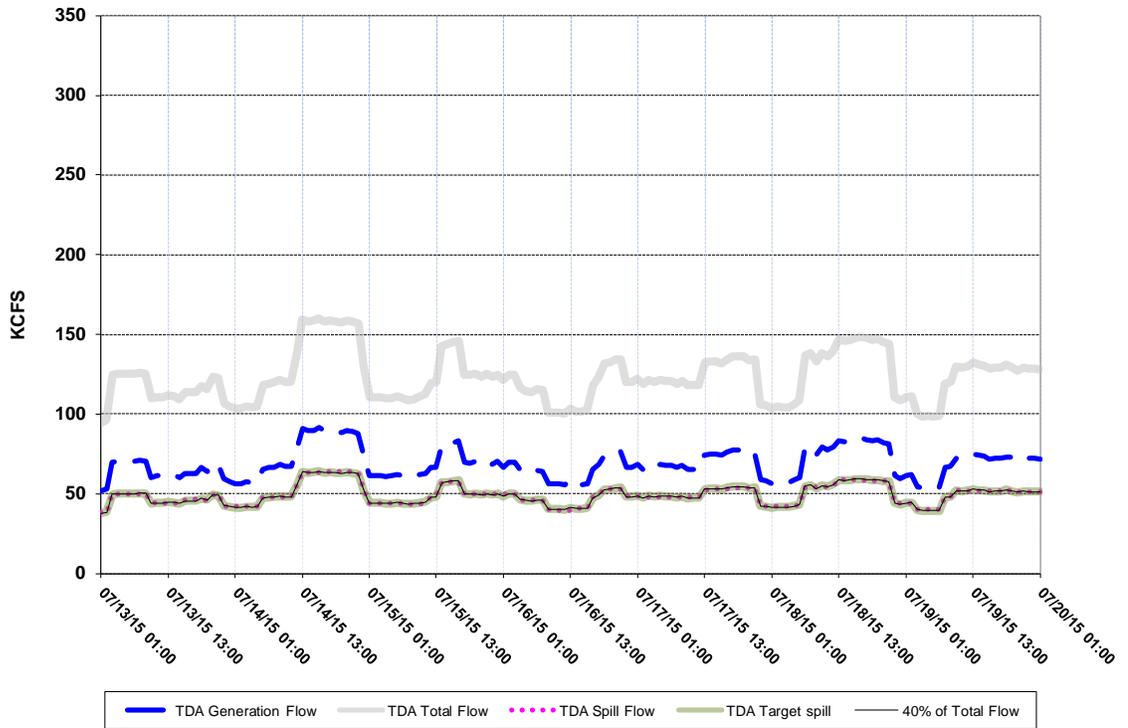


Figure 24

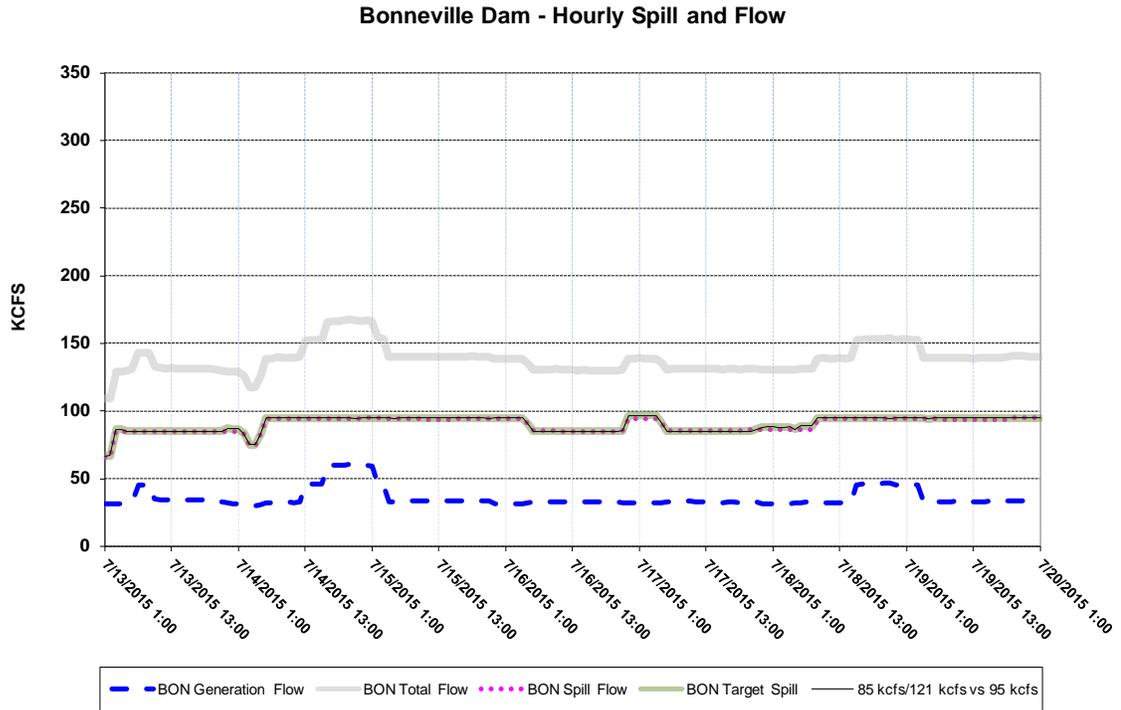
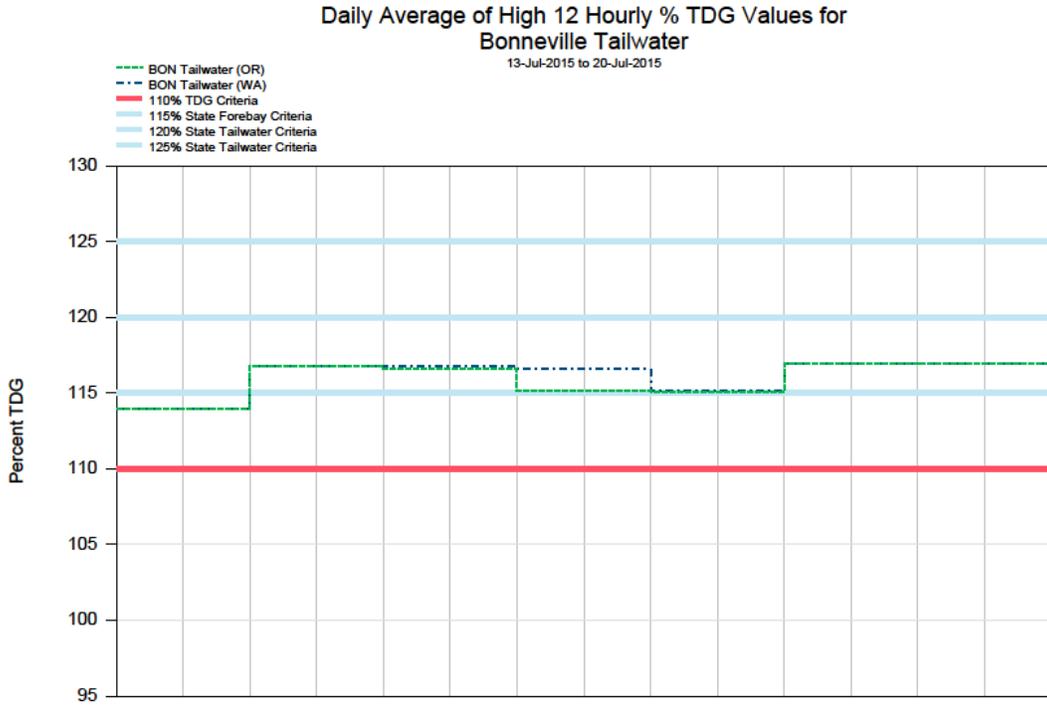


Figure 25

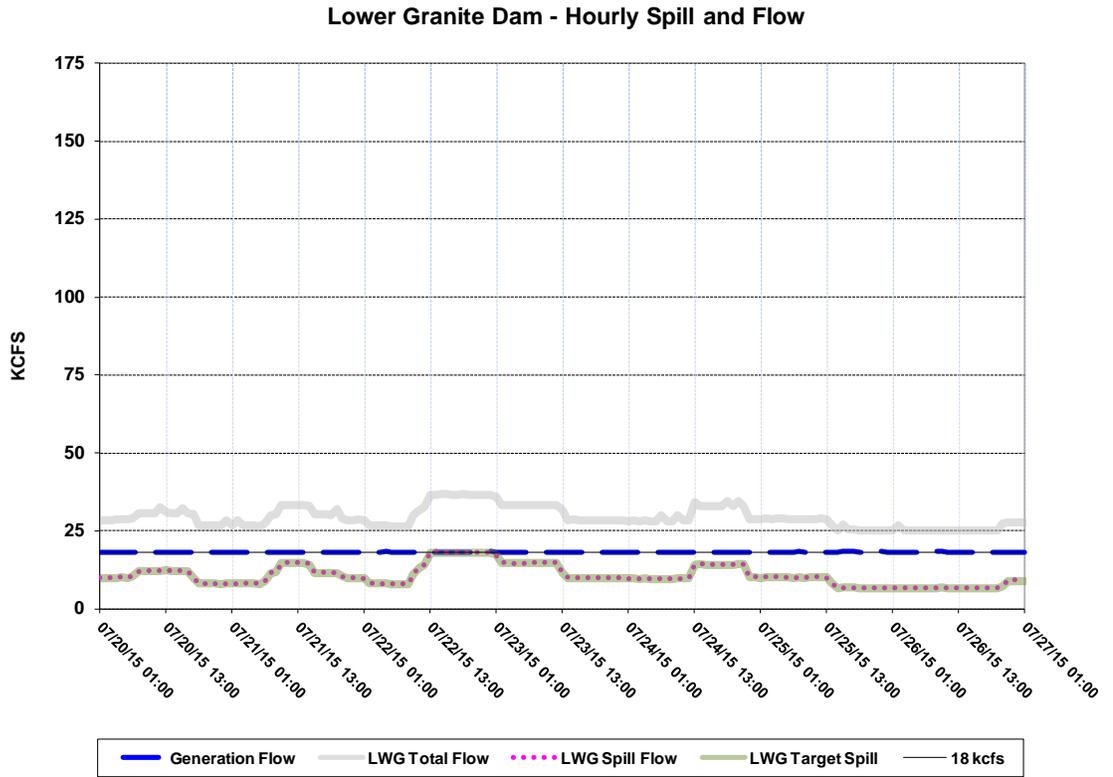
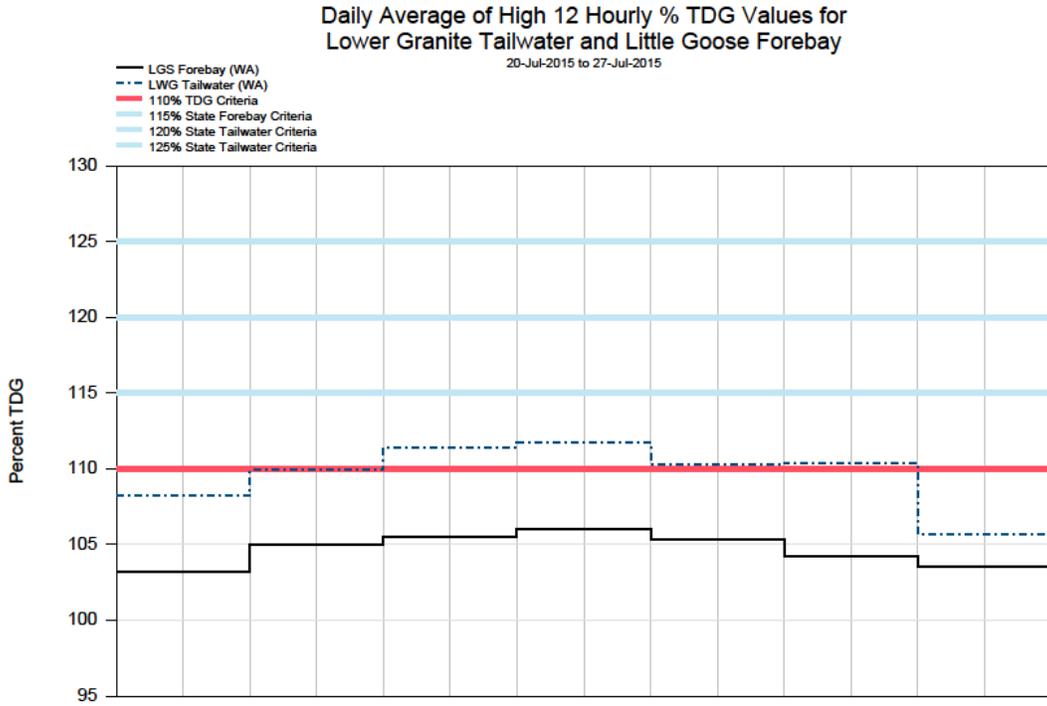
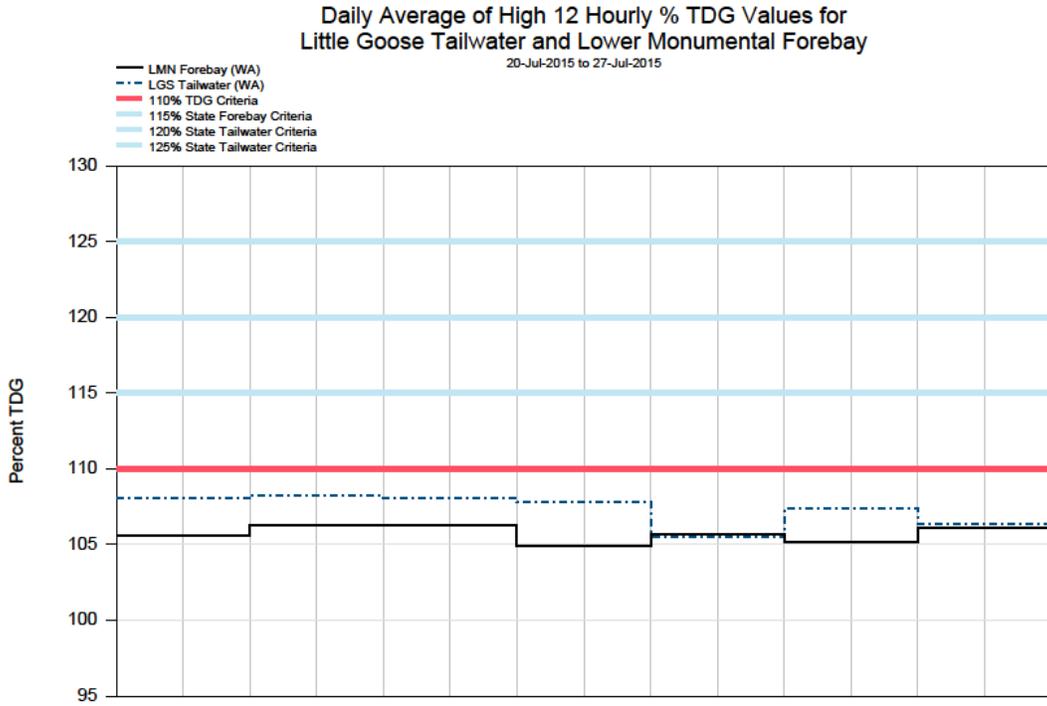


Figure 26



Little Goose Dam - Hourly Spill and Flow

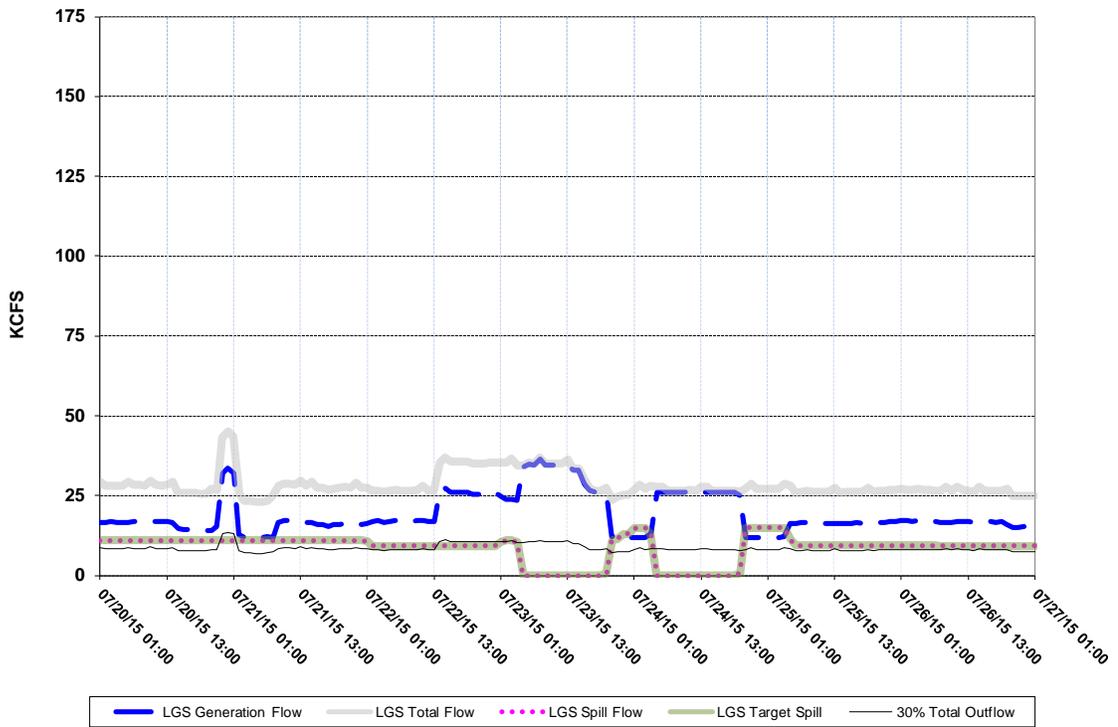


Figure 27

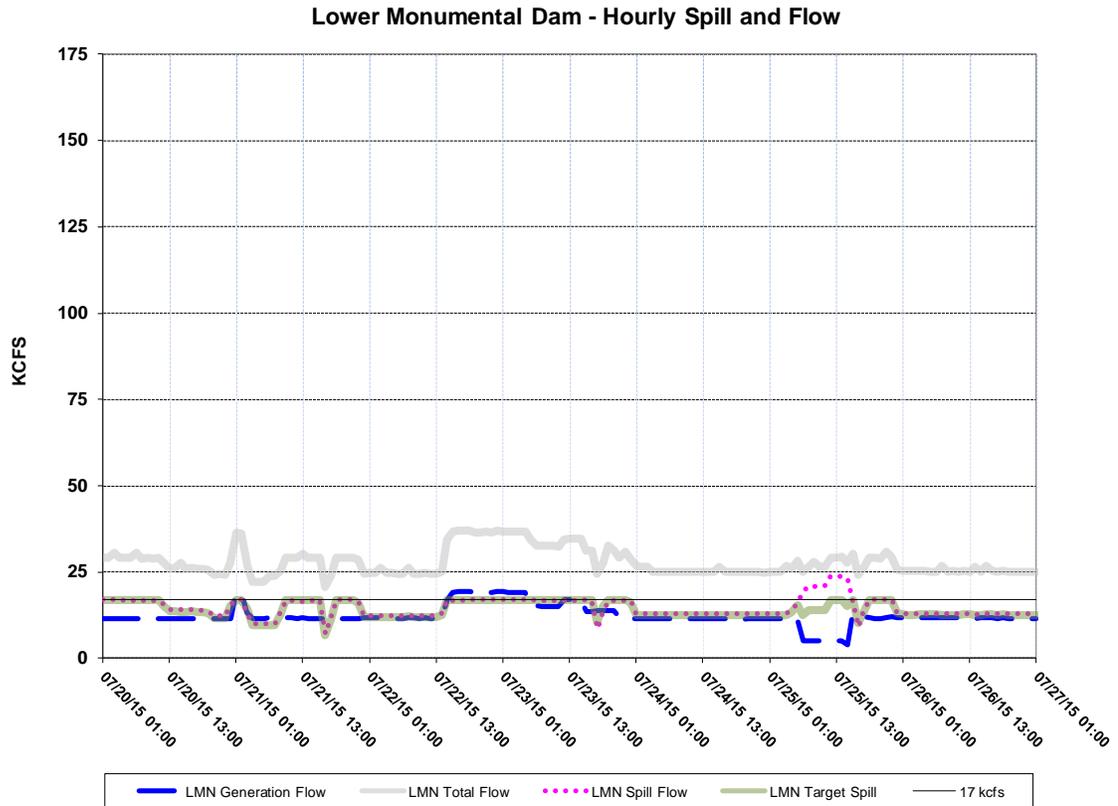
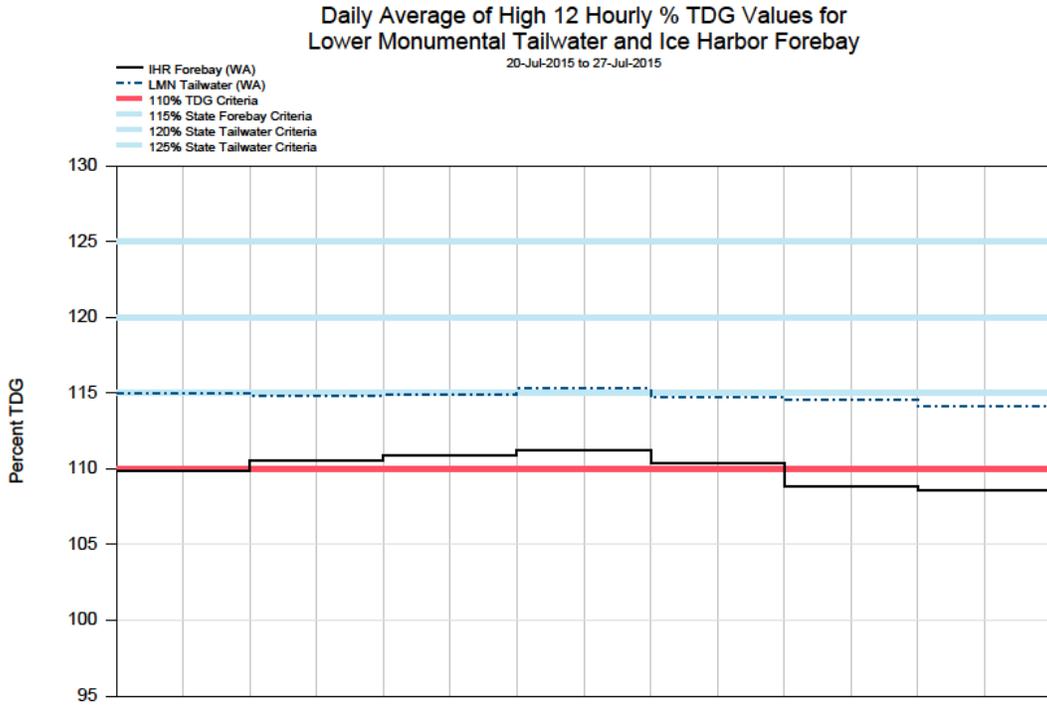
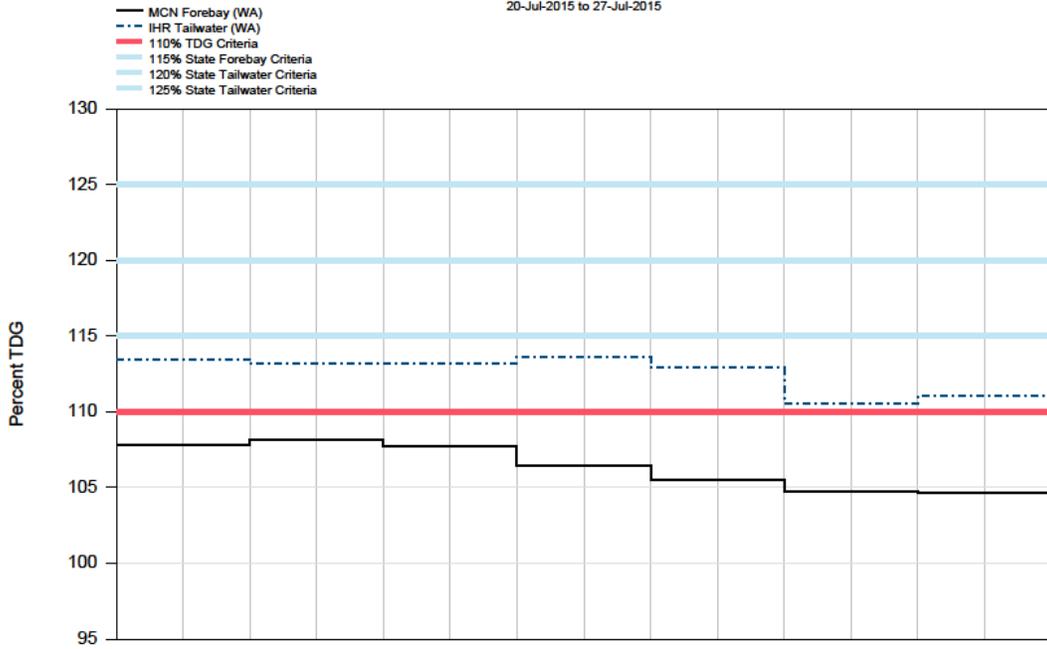


Figure 28

Daily Average of High 12 Hourly % TDG Values for Ice Harbor Tailwater and McNary Forebay

20-Jul-2015 to 27-Jul-2015



Ice Harbor Dam - Hourly Spill and Flow

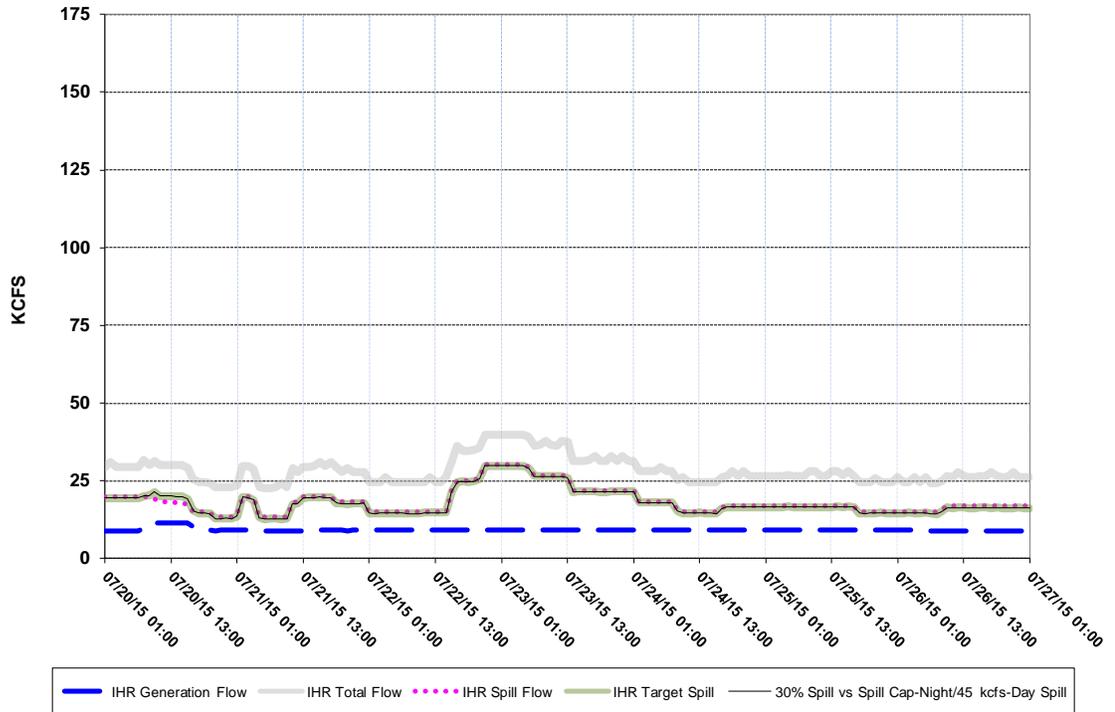


Figure 29

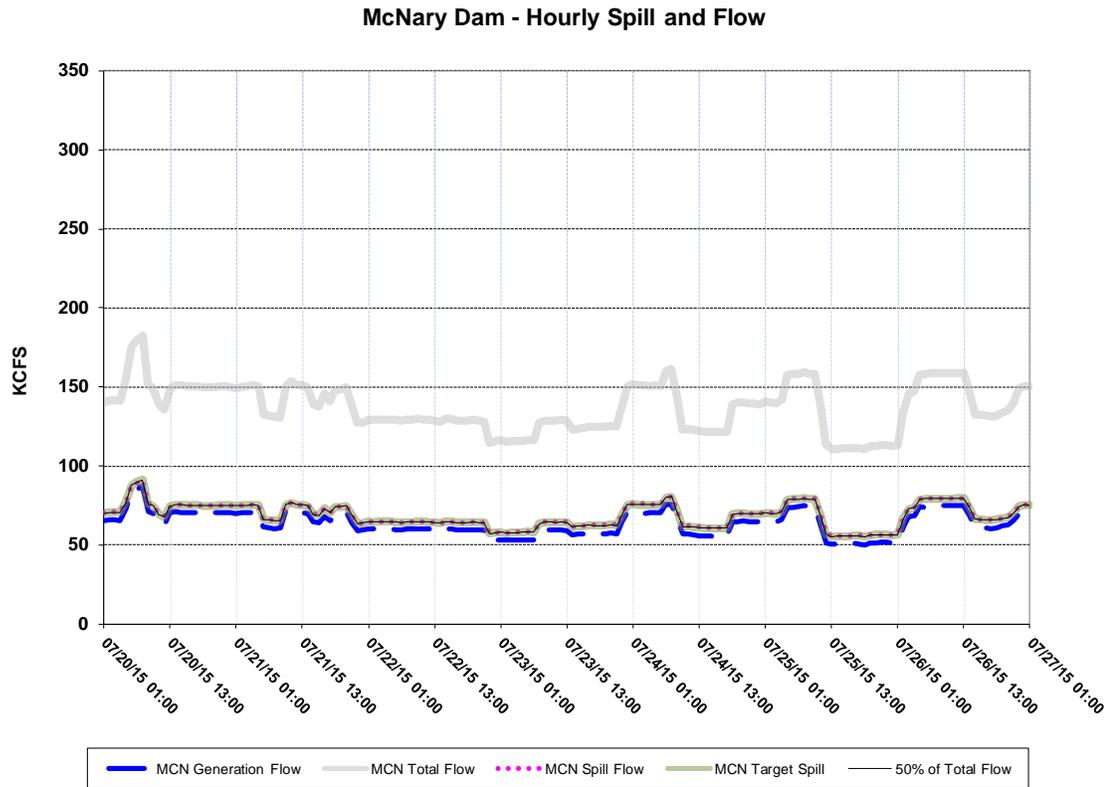
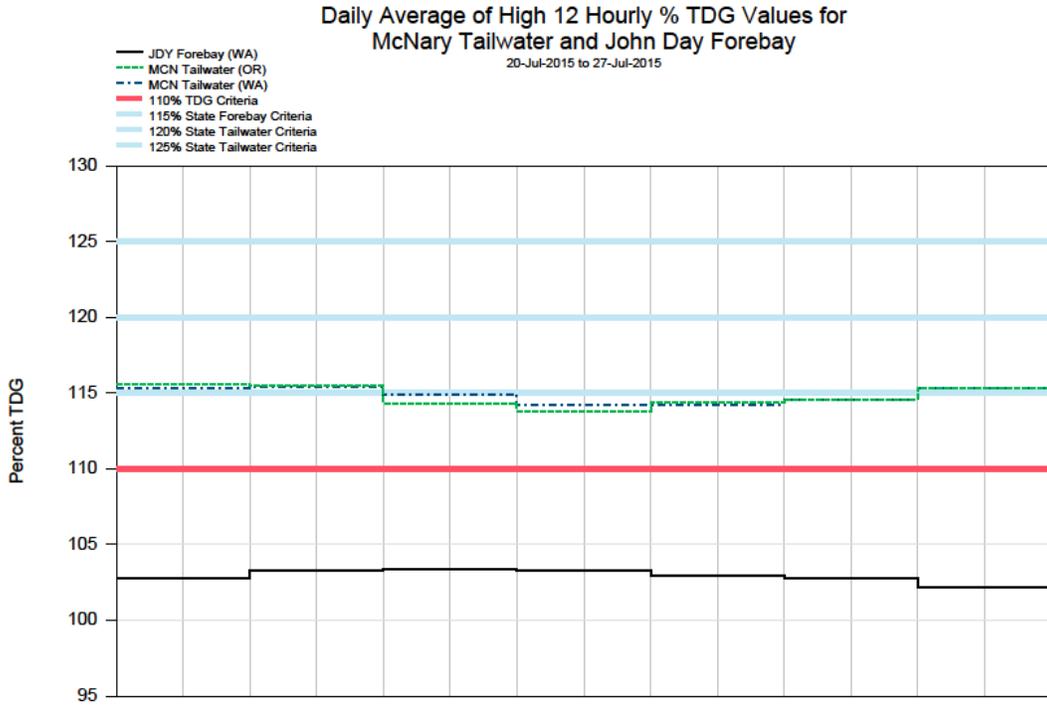
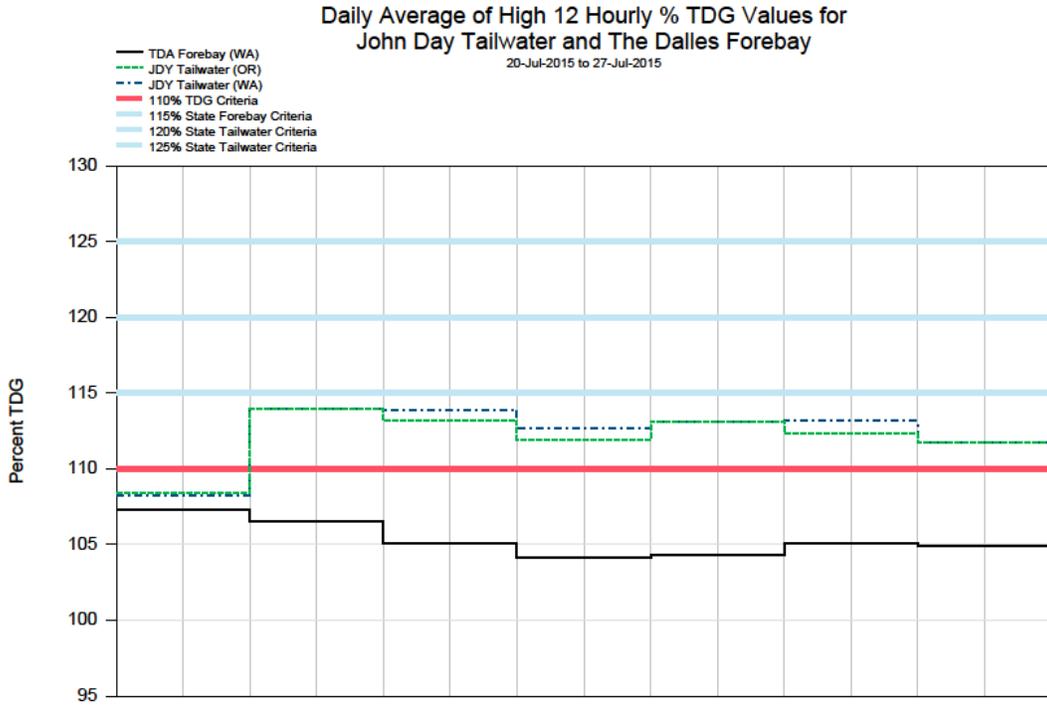


Figure 30



John Day Dam - Hourly Spill and Flow

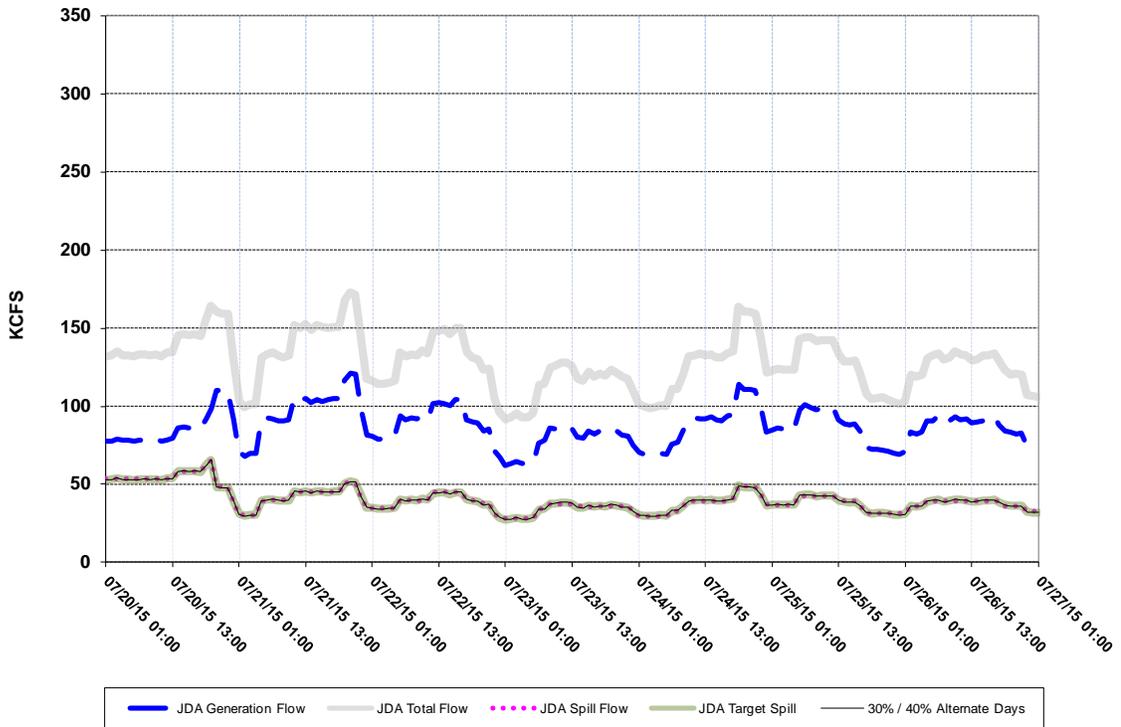
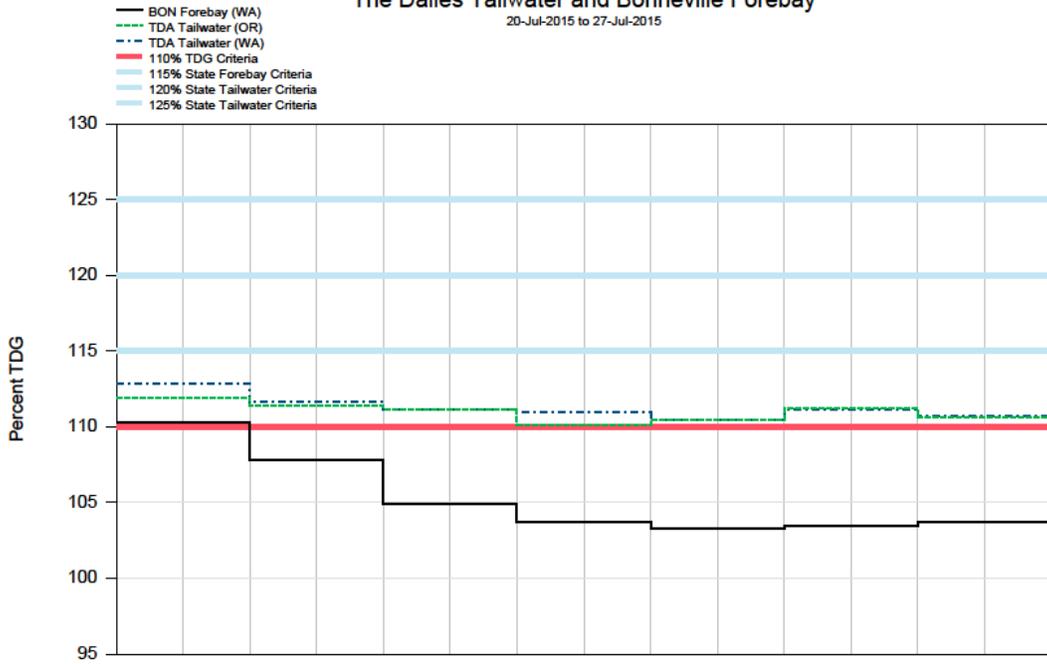


Figure 31

**Daily Average of High 12 Hourly % TDG Values for
The Dalles Tailwater and Bonneville Forebay**

20-Jul-2015 to 27-Jul-2015



The Dalles Dam - Hourly Spill and Flow

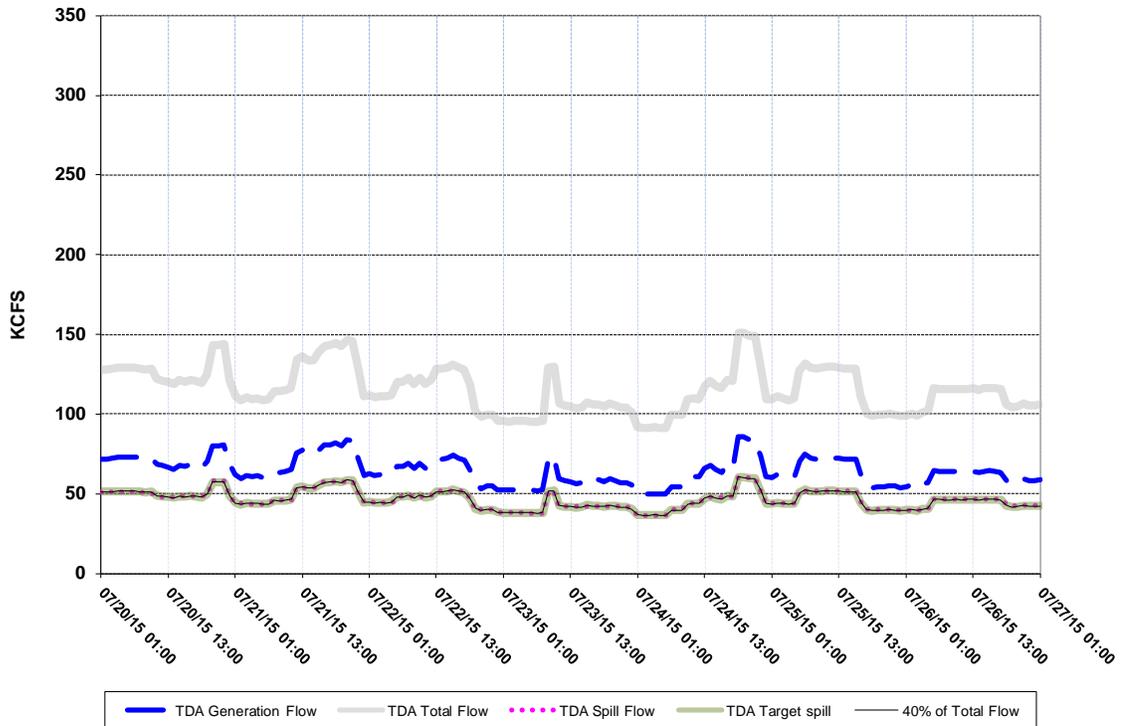
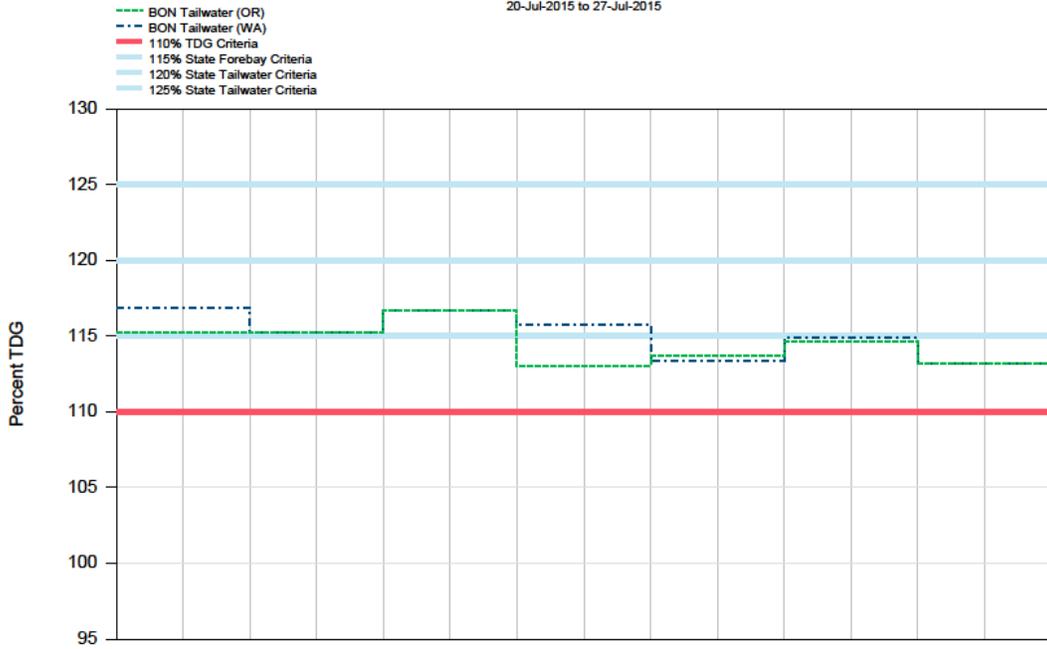


Figure 32

Daily Average of High 12 Hourly % TDG Values for Bonneville Tailwater

20-Jul-2015 to 27-Jul-2015



Bonneville Dam - Hourly Spill and Flow

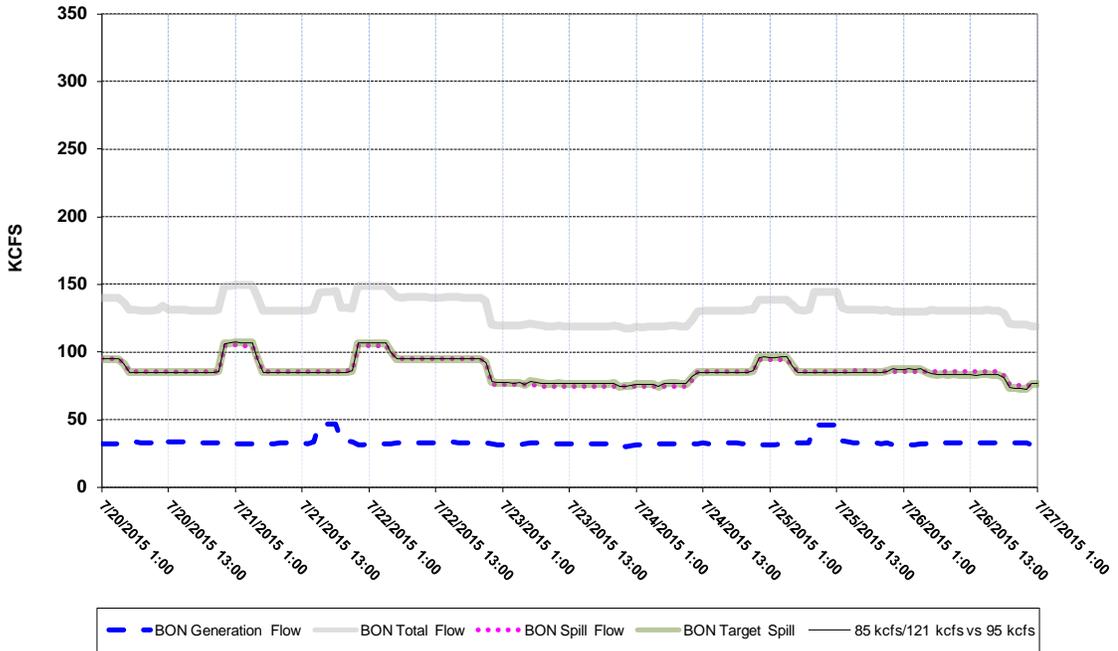


Figure 33

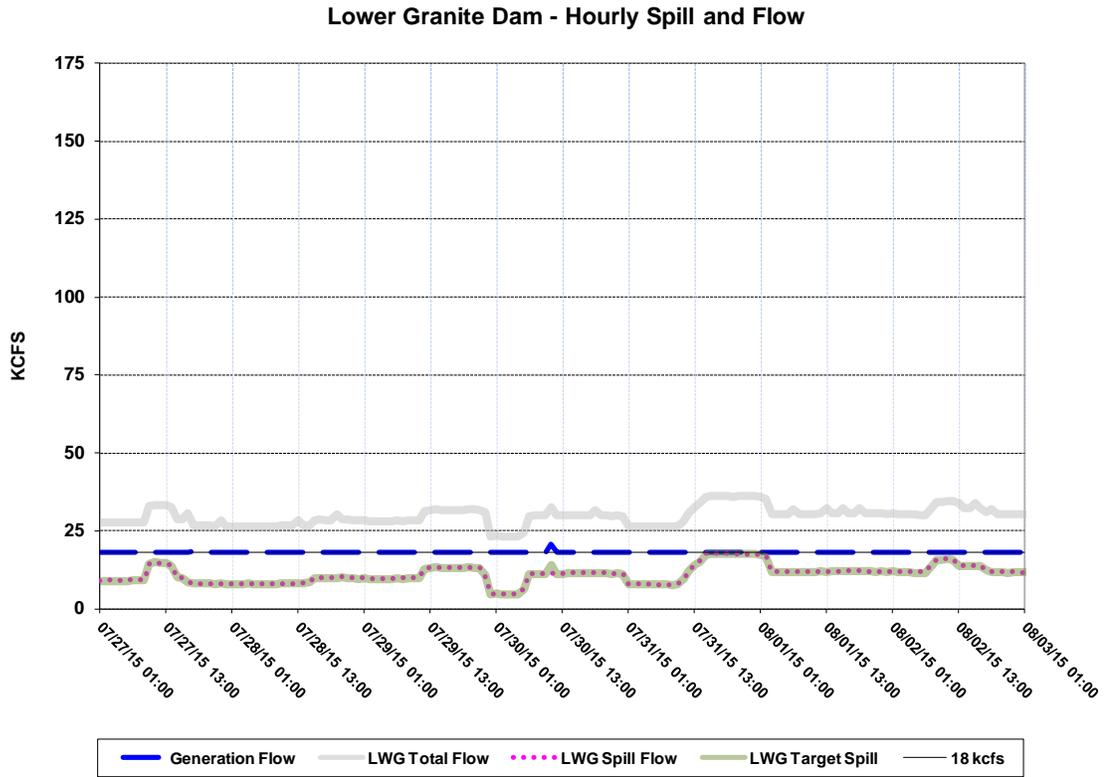
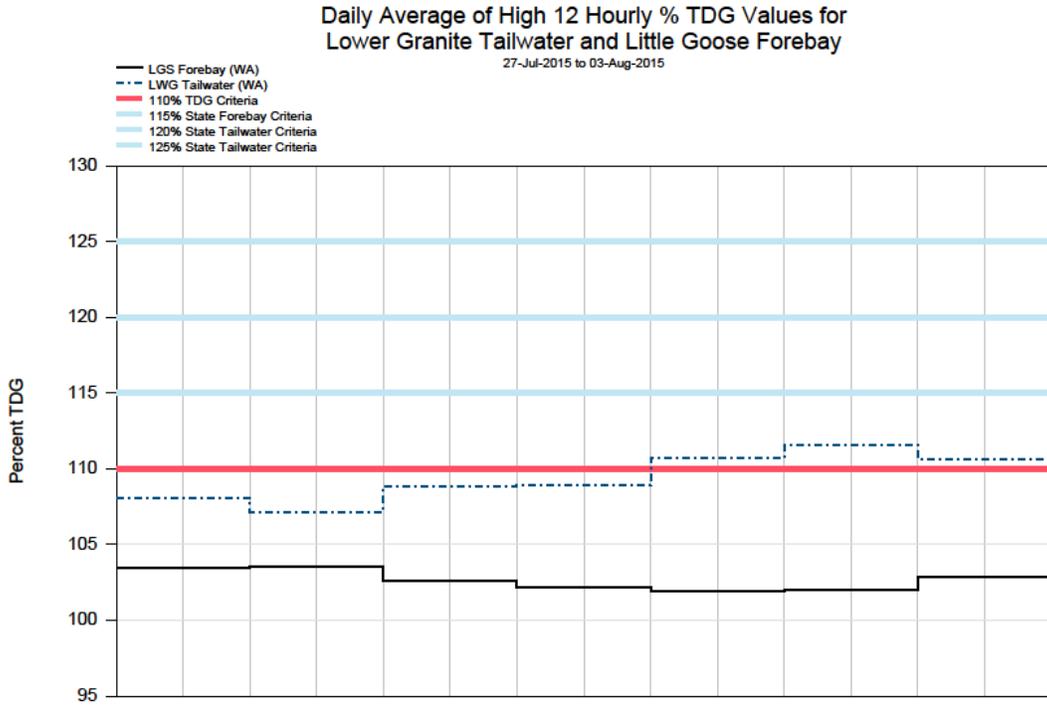
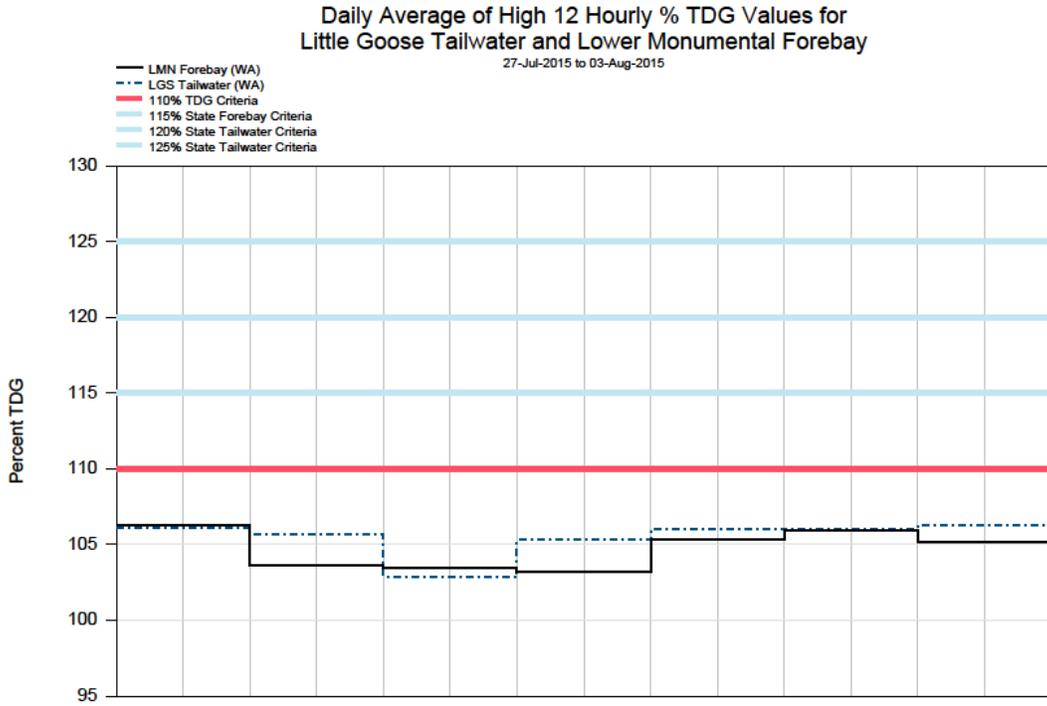


Figure 34



Little Goose Dam - Hourly Spill and Flow

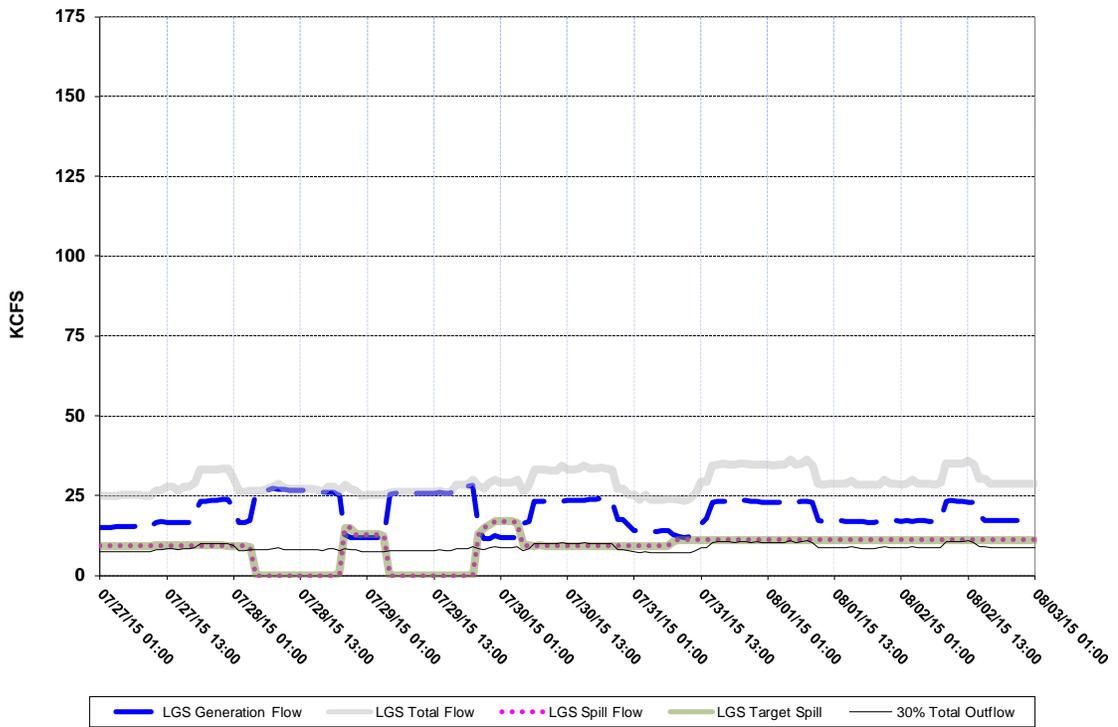


Figure 35

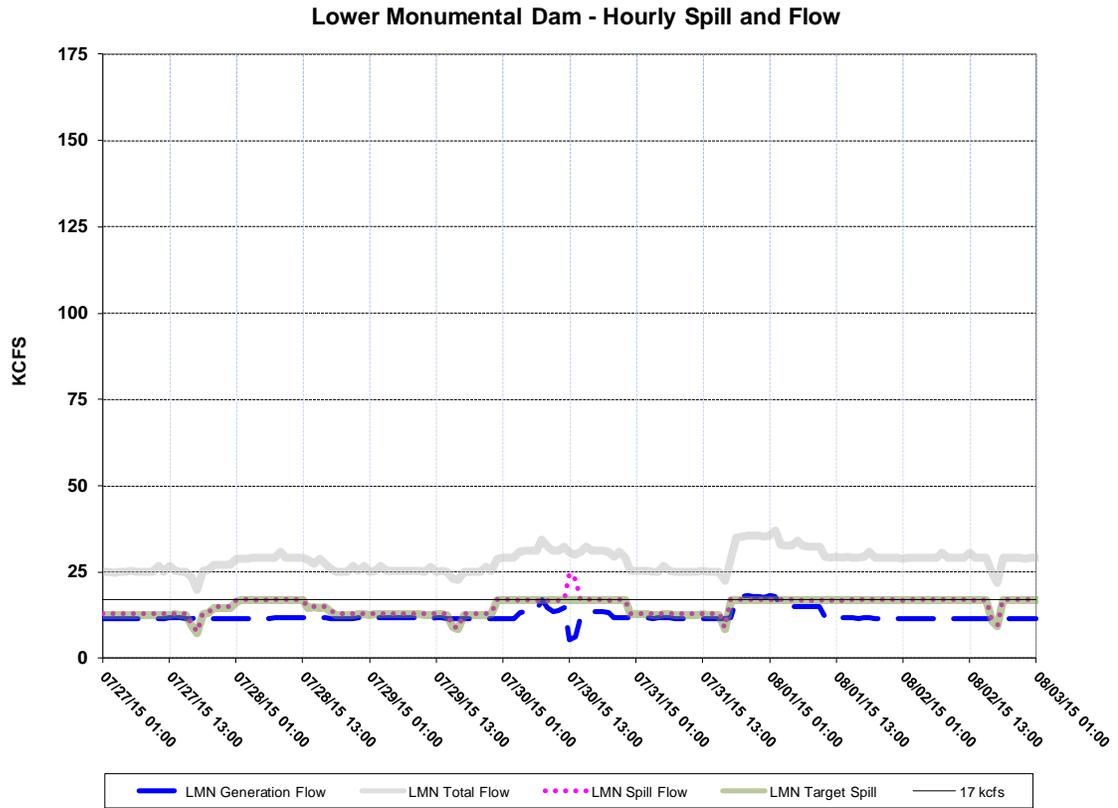
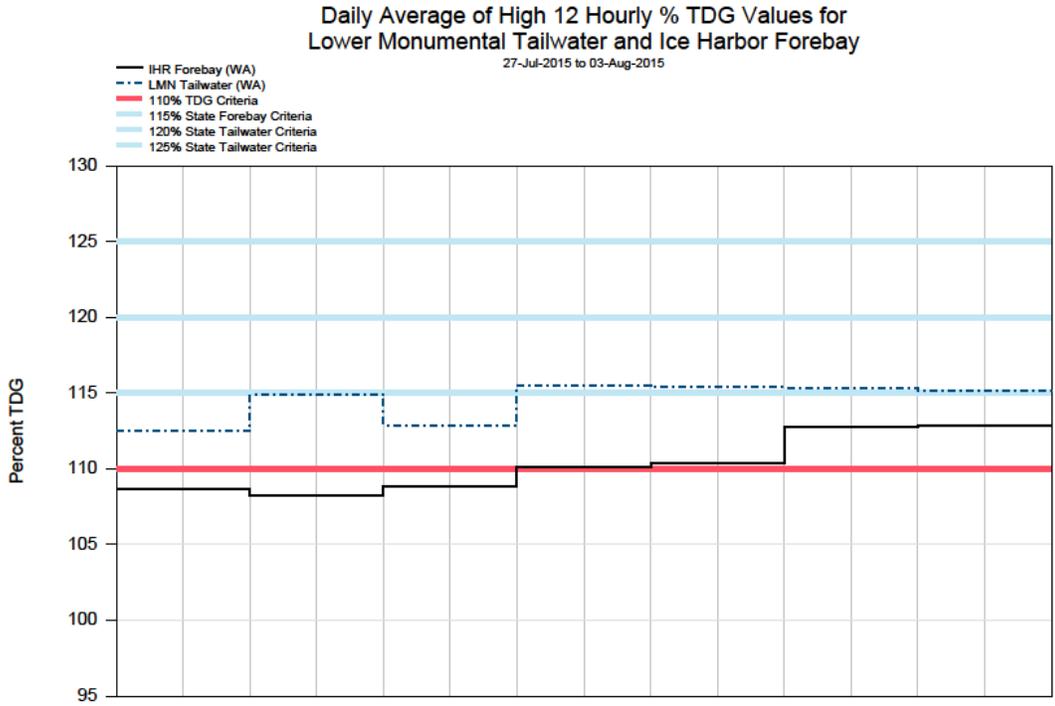
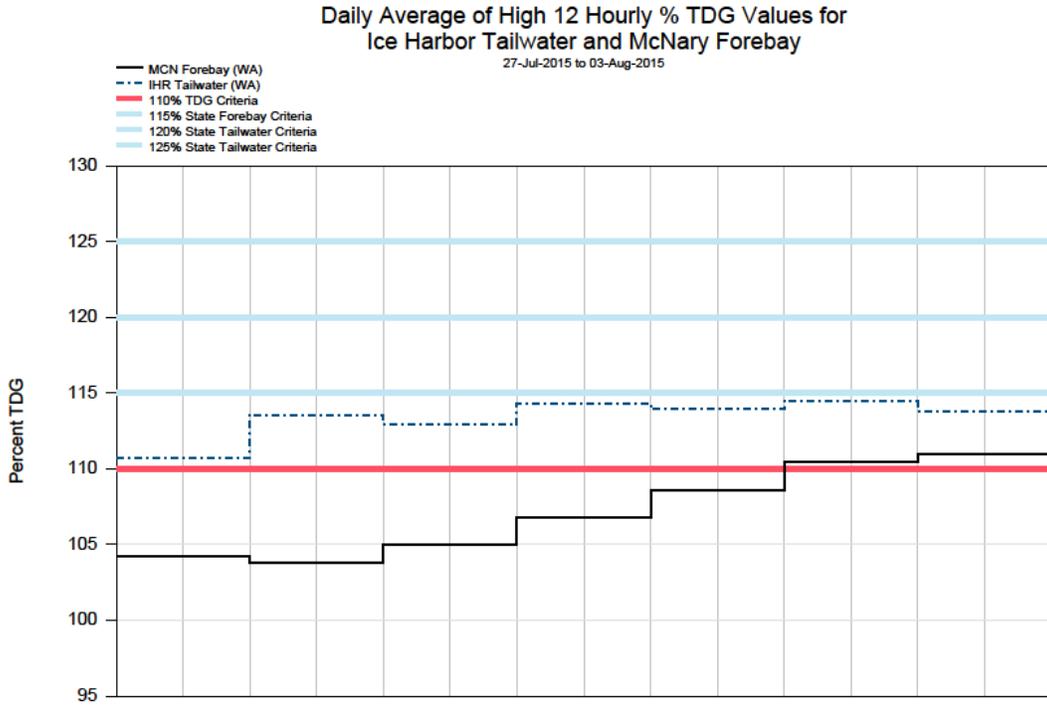


Figure 36



Ice Harbor Dam - Hourly Spill and Flow

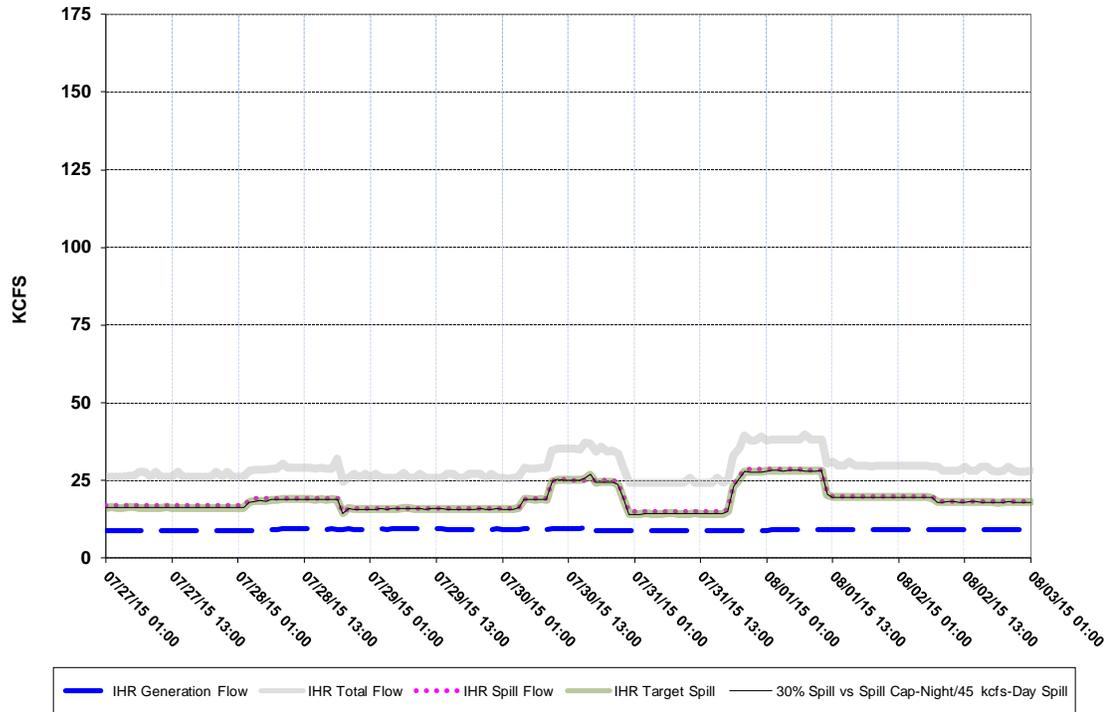


Figure 37

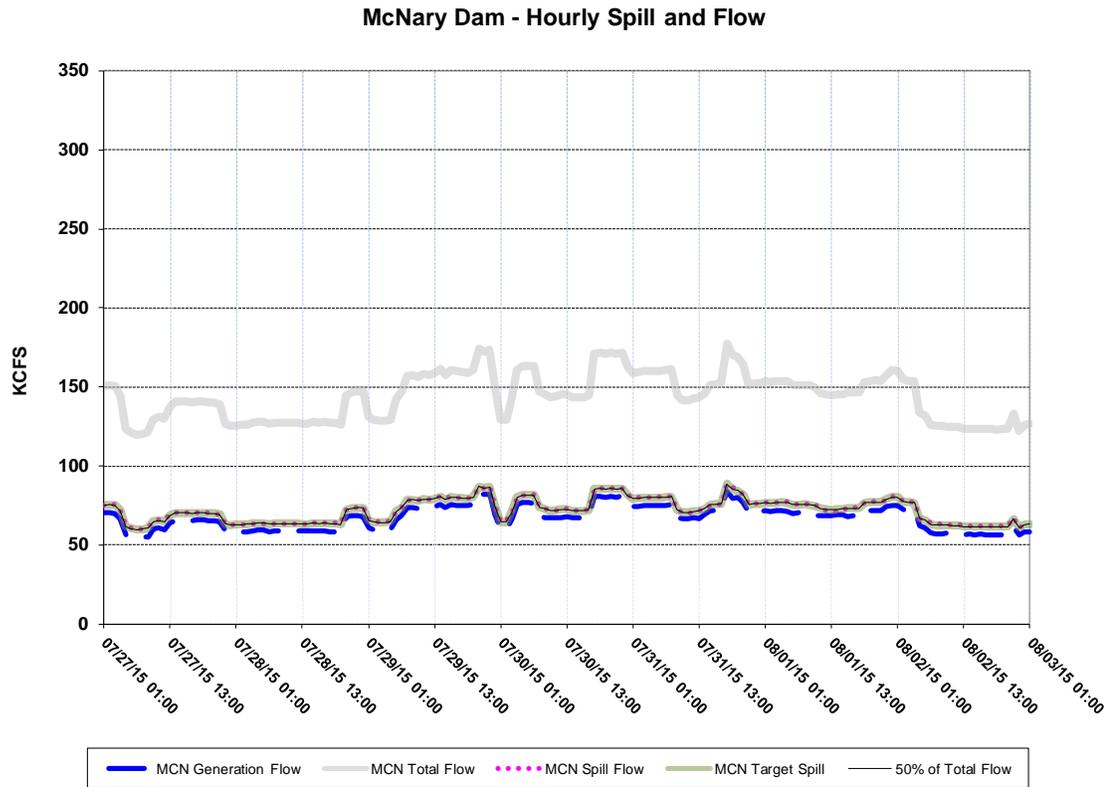
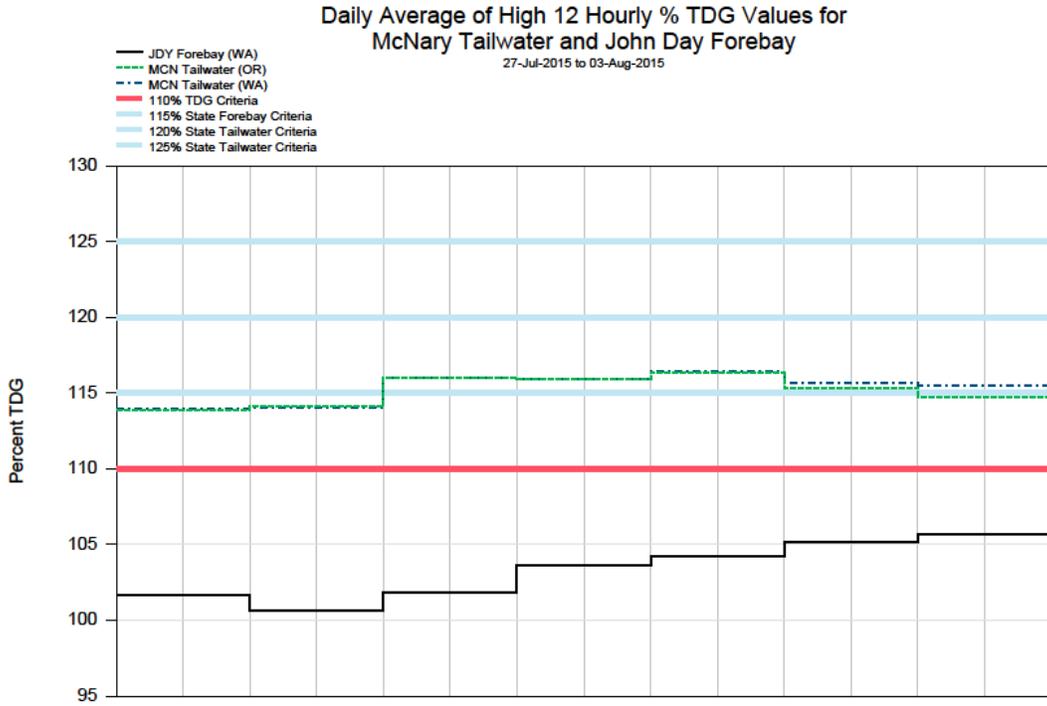
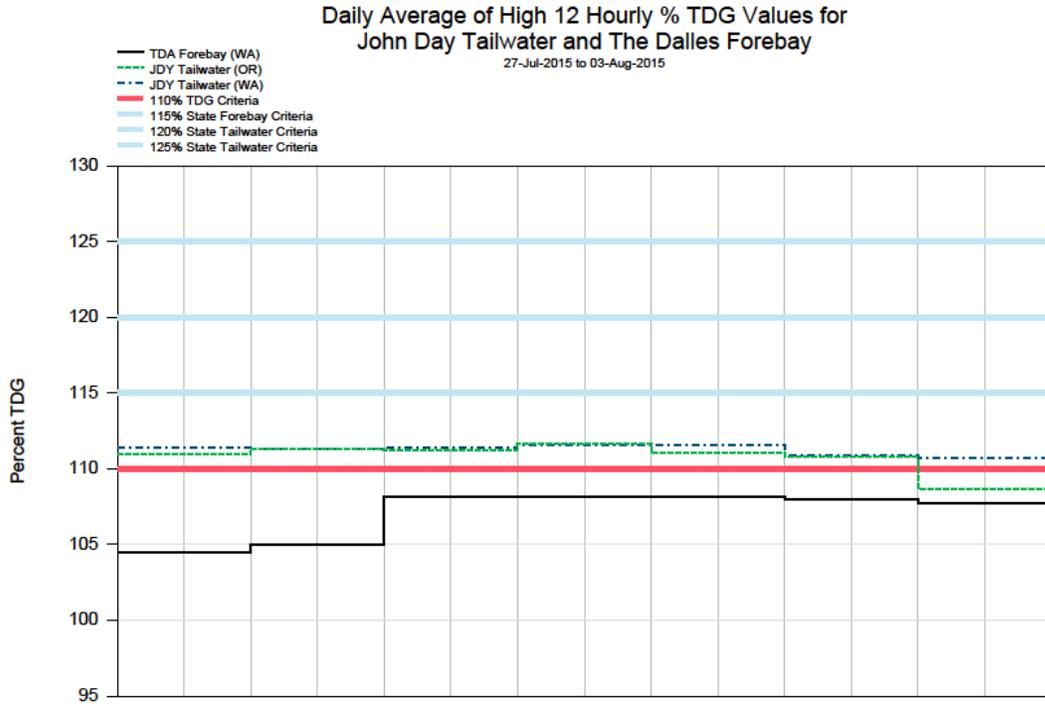


Figure 38



John Day Dam - Hourly Spill and Flow

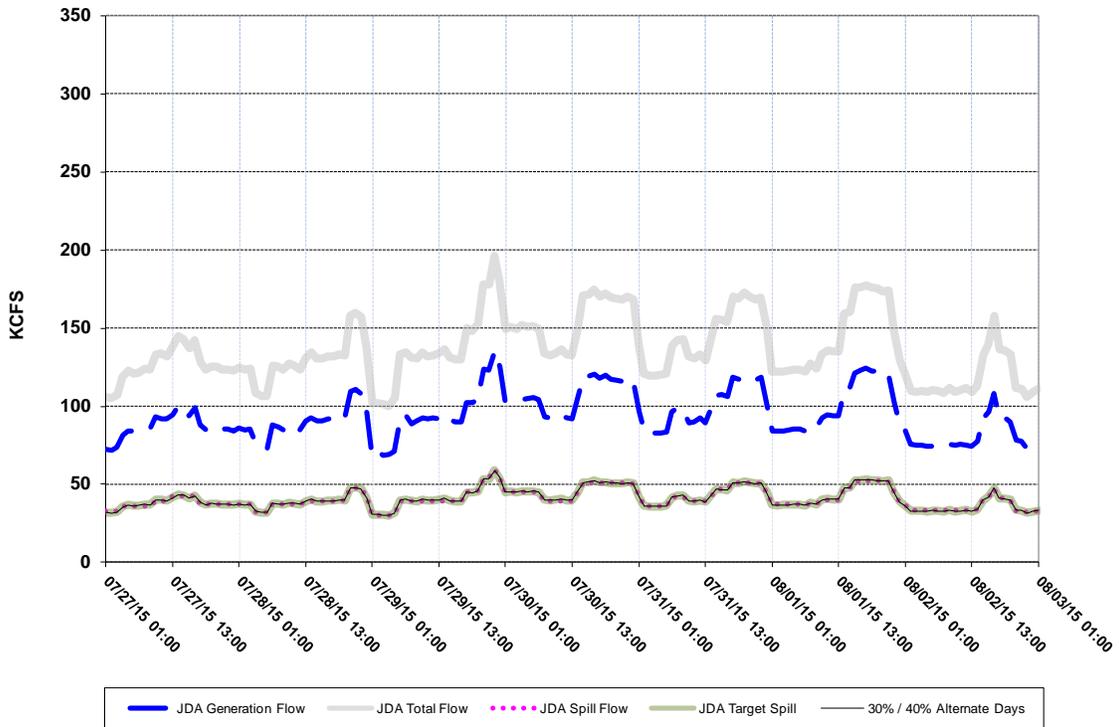
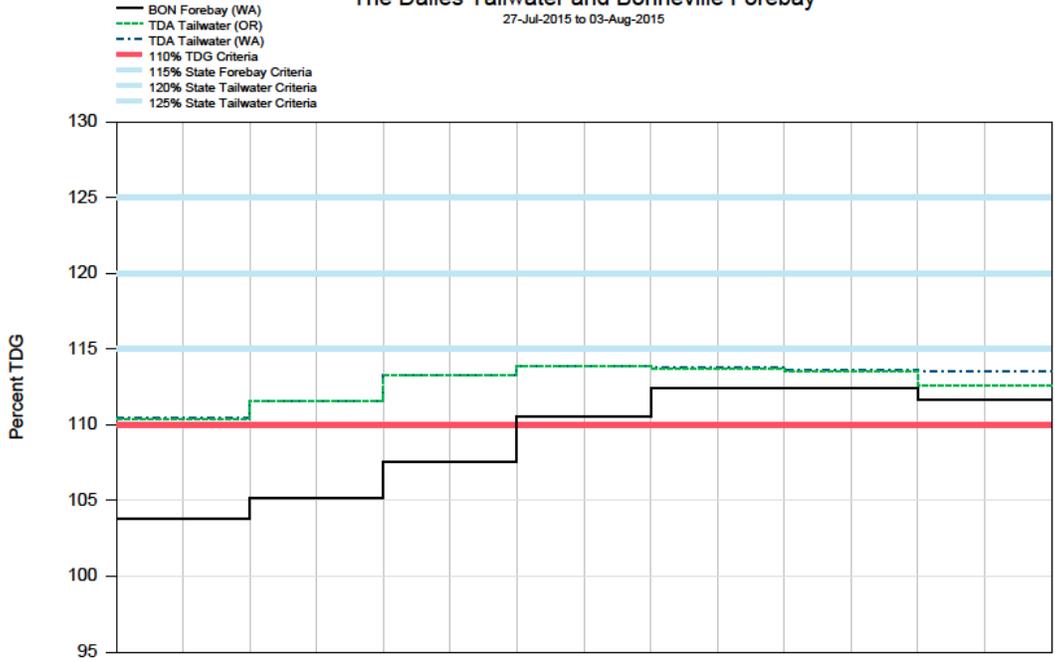


Figure 39

**Daily Average of High 12 Hourly % TDG Values for
The Dalles Tailwater and Bonneville Forebay**

27-Jul-2015 to 03-Aug-2015



The Dalles Dam - Hourly Spill and Flow

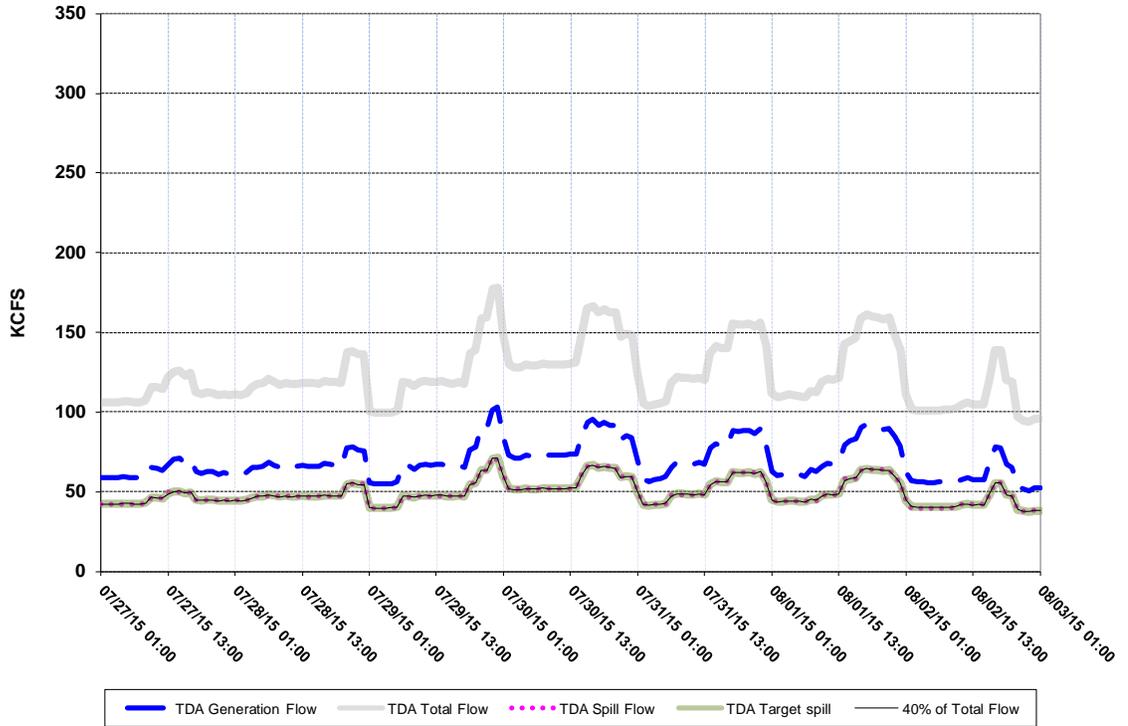
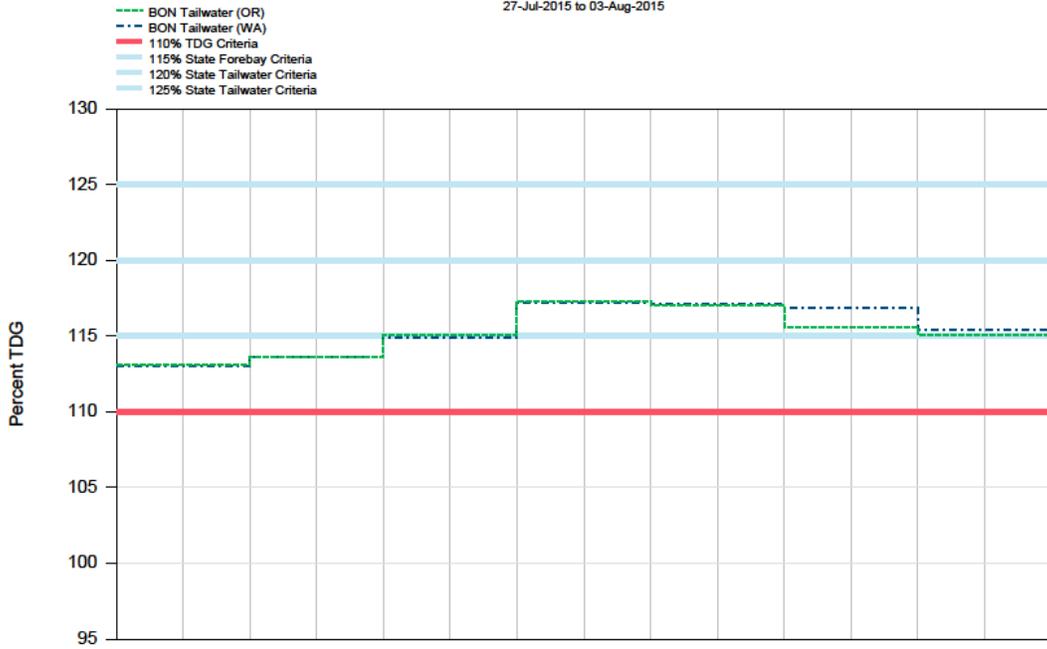


Figure 40

Daily Average of High 12 Hourly % TDG Values for Bonneville Tailwater

27-Jul-2015 to 03-Aug-2015



Bonneville Dam - Hourly Spill and Flow

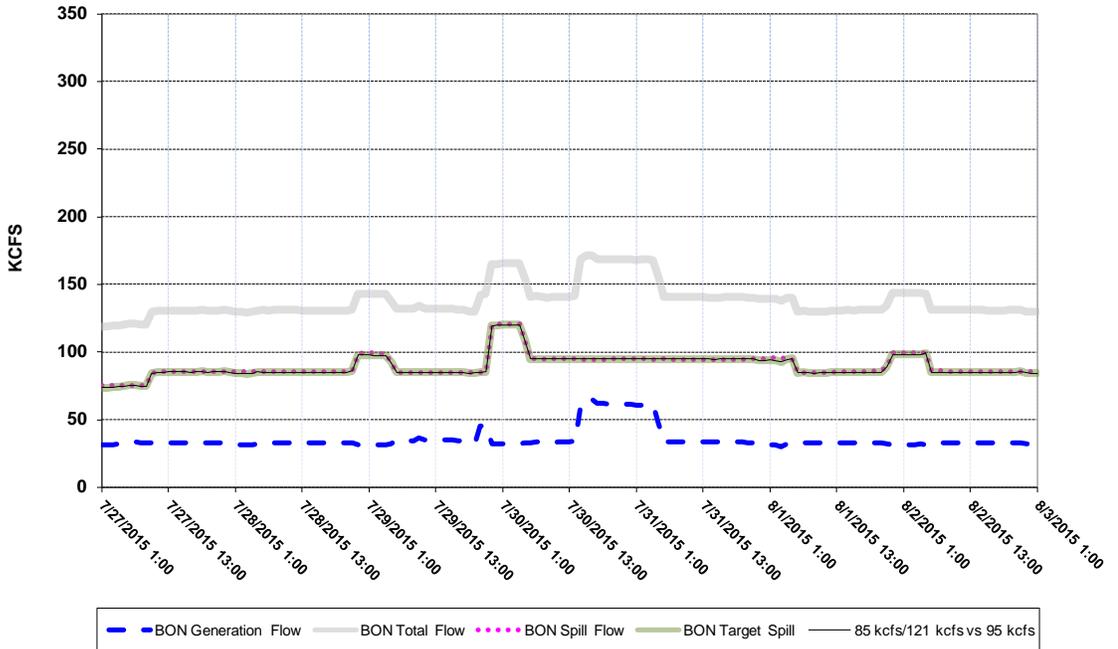


Table 2. Average Percent TDG Values For July 29 – August 2

Date	FIXED MONITORING STATIONS																				
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	IDSW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW		
	Method:	WA	OR	WA																	
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120	
6/29/2015	106.8	113.9	109.4	106	109.4	115.8	114.7	113.6	110.9	116.9	116.9	109.3	114.5	114.5	109	114	115.1	111	116.8	116.9	
6/30/2015	106.8	115.2	111.3	109.3	108.7	115.3	114.4	113.6	110.4	116.8	116.9	109	114.8	114.8	108.5	113	114	108.1	116	116.6	
7/1/2015	103.4	115.5	112.5	111.3	108.7	115.6	114.2	114.4	110.2	116.7	116.7	108.8	114.7	114.7	109.9	114.6	114.6	108.8	115.7	115.6	
7/2/2015	103.7	115.3	112.5	111.1	108.3	116	113.8	114.3	110.4	117.1	117.1	110.2	114.6	114.6	112.9	116	116	110.8	117.9	118	
7/3/2015	104.9	113.8	112.3	111.2	109.1	115.5	113.4	113.7	111.1	116	117.1	110.9	115.2	115.2	112.6	115.2	116	110.8	117.5	117.5	
7/4/2015	105.1	113.7	112.1	110.6	109.1	112.7	113.8	113.1	110.9	114.6	115.4	110.9	114.9	115	110.2	114.3	114.6	109.9	115.9	117.5	
7/5/2015	105.2	111.1	112	110.7	109	113.1	113.8	112.5	110.8	115.1	115.1	109.6	114.6	114.6	109.7	114.3	114.3	108.9	115.8	115.7	
7/6/2015	104.3	113.9	113.1	111.1	109.1	113.1	113.4	111.9	110.6	116.1	116.1	109	114.4	114.3	111.3	114.9	114.9	109.2	117.2	117.2	
7/7/2015	104.3	114.1	111.8	110.9	109.1	113.1	114.1	113.2	110.7	116.1	116.1	109.1	114.3	114.3	111	114.6	114.7	109.1	117.2	117.1	
7/8/2015	104.3	114.6	112.4	111.2	108.3	112.7	114.1	112.6	109.3	114.8	115.2	108.5	114.3	114.2	109	113.9	114.4	108.2	115.3	117.1	
7/9/2015	104.1	110.8	112.4	111.2	108.5	112.8	111.9	111.7	110.2	116.7	116.7	108.8	114.6	114.6	111.5	115.3	115.3	108.3	115	115	
7/10/2015	102.8	110.6	111.9	110.8	108.6	115.3	111.8	113.2	110.2	114.8	116.6	108.9	114.3	114.2	111.3	113	115.3	107	116	116.9	
7/11/2015	101.6	110.5	110.5	110.2	107.7	115	110.7	113	109.1	113.1	113.4	107.6	112.3	112.3	106.6	109.8	110.9	105	113.4	113.4	
7/12/2015	101.5	110.1	110.1	110.1	107.7	113.7	109.8	110.9	107.6	113	113	105.4	112.5	112.5	105.5	110.6	110.6	103.2	113.2	113.2	
7/13/2015	101.5	109.9	109.3	110.1	106.7	115.3	108	113.3	105	113.6	113.5	104.1	111.7	112.2	108.3	112.2	112.2	104.1	114.2	114.1	
7/14/2015	101.5	107.9	108.2	110.1	106.7	115.8	107	113.6	104.1	116.8	116.8	103.4	112.4	112.4	108.3	113	113.2	105.7	116.9	116.9	
7/15/2015	102.2	104.8	107.2	109.4	106.2	114.6	107.1	113	104.2	114.6	116.3	103.1	111.3	111.9	106.3	111.9	112.7	105.8	116.8	116.9	
7/16/2015	102.8	105.5	107	108.4	106.3	113.3	107.9	111	105.9	115	115	102.5	109.8	110.2	105	110.1	111.3	105.2	115.3	116.7	
7/17/2015	102.8	107	106.5	108.6	107.2	114.4	109.2	113.4	106.3	114.6	114.7	101.5	108.5	109.5	105.9	111.8	111.8	104.9	115	115.3	
7/18/2015	102.3	106.6	106	109	106.8	116.1	110	113.8	106.3	116.4	115.9	101.7	110.1	110.1	107.5	113.1	113.1	107.2	117.1	117.1	
7/19/2015	102.3	109.3	105.8	108.5	106.4	115.6	110.2	113.9	106.6	116	115.9	102.7	108.3	109.3	107.6	113	113.1	110.3	117.1	117.1	
7/20/2015	101.8	108.2	103.3	108	105.5	114.8	109.8	113.3	107.9	115.6	115.3	102.8	108.4	108.3	107.2	111.9	112.7	110.2	115.4	117	
7/21/2015	101.9	109.9	105.1	108.3	106.3	114.8	110.6	113.2	108.1	115.4	115.4	103.3	114	114	106.4	111.3	111.6	107.8	115.4	115.4	
7/22/2015	102.9	111.6	105.5	107.9	106.2	115	110.9	113	107.7	114.3	114.7	103.4	113.1	113.7	105	111.2	111.2	104.9	116.8	116.8	
7/23/2015	103.3	111.7	106	107.8	105.1	115.3	111.2	113.6	106.4	113.8	114.2	103.3	111.9	112.5	104	110.1	110.8	103.7	113.2	115.6	
7/24/2015	103.2	110.4	105.2	105.5	105.6	114.6	110.3	112.7	105.5	114.3	114.2	102.9	113.2	113.2	104.3	110.6	110.6	103.3	114.1	113.7	
7/25/2015	102.4	110.4	104.2	107.4	105.1	114.5	108.8	110.4	104.7	114.6	114.6	102.8	112.3	113.1	105.1	111.2	111.2	103.5	114.5	115	
7/26/2015	102.1	105.4	103.5	106.4	106.2	114	108.6	111.1	104.6	115.3	115.3	102.1	111.8	111.7	104.9	110.6	110.6	103.8	113.3	113.3	
7/27/2015	101.8	108.1	103.5	106	106.3	112.4	108.7	110.7	104.2	113.8	113.8	101.6	111	111.3	104.4	110.4	110.4	103.8	113.2	113.2	
7/28/2015	101	106.7	103.5	105.5	103.6	114.9	108.3	113.6	103.8	114.2	114	100.6	111.4	111.4	105	111.6	111.6	105.3	114	114	
7/29/2015	100.8	108.9	102.5	102.9	103.4	112.6	108.9	112.6	105.2	116	116	102.1	111.3	111.3	108.2	113.3	113.3	107.8	115.3	115	
7/30/2015	100.1	108.6	102.1	105.3	103.2	115.5	110.2	114.3	106.9	116	115.9	103.8	111.6	111.6	108.1	113.8	113.8	110.7	117.4	117.3	
7/31/2015	99.9	111	101.9	106	105.5	115.1	110.4	113.7	108.7	116.3	116.4	104.2	111	111.5	108.1	113.7	113.7	112.4	117.1	117.2	
8/1/2015	101	111.6	102	106.1	105.9	115.3	112.8	114.5	110.7	115.4	115.6	105.2	110.8	110.8	108	113.5	113.6	112.4	115.7	117	
8/2/2015	103.5	110.6	103	106.3	105.1	115.1	112.9	113.8	111	114.6	115.5	105.7	110.5	110.6	107.6	112.6	113.5	111.6	114.9	115.6	

Note: The Oregon TDG standard modification (OR) and Washington TDG criteria adjustments (WA) have different methodologies for calculating TDG. When standards vary or conflict, the Corps applies the more stringent standard. TDG values are presented in Table 1 by displaying highest value %TDG (more stringent), and the lower value is displayed with a strikethrough.

Total Dissolved Gas Monitoring Stations

Code	Station Name	Code	Station Name
LWG	Lower Granite Forebay	LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay	LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay	LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay	IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay	MCPW	McNary Tailwater
JDY	John Day Forebay	JHAW	John Day Tailwater
TDA	The Dalles Forebay	TDDO	The Dalles Tailwater
BON	Bonneville Forebay	CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal		

FISH OPERATIONS PLAN IMPLEMENTATION REPORT

August 2015

**Submitted by the U.S. Army Corps of Engineers
Northwestern Division
Portland, OR.**

Introduction

The U.S. Army Corps of Engineers (Corps) is submitting this report in accordance with the 2015 Fish Operations Plan (2015 FOP) posted to the TMT website on March 1, 2015. The 2015 FOP describes the Corps' project operations for fish passage at its Federal Columbia River Power System (FCRPS) dams during the spring and summer fish migration season, generally April through August. To the extent Corps project operations are not specified in the 2015 FOP, the FCRPS operations will be consistent with the 2014 NOAA Fisheries Supplemental Biological Opinion (2014 Supplemental BiOp), the USFWS 2000 and 2006 BiOps, and/or other operative documents, including the 2015 Water Management Plan (WMP), WMP seasonal updates, and the 2015 Fish Passage Plan (FPP).

The Corps' August 2015 lower Snake and Columbia River project and fish passage operations are contained in this report. In particular, information in this report includes the following:

- Hourly flow through the powerhouse at each dam;
- Hourly flow over the spillway compared to the spill target for that hour; and
- Daily average Total Dissolved Gas (TDG) levels (percent of saturation) in the tailwater at each project, and in the subsequent downstream project's forebay.¹

This report also provides information on presented issues and unanticipated or emergency situations that arose during implementation of the 2015 FOP in August 2015.

Data Reporting

I. For each project providing fish passage operations, this report contains two figures per operational week² in August displaying the performance of the fish passage spill program as follows:

- (A) Average % TDG Values - displayed in the upper figure.
- (B) Hourly Spill and Generation Flows - described in the lower figure.

¹ Averages reported are consistent with current and applicable Oregon TDG standard modification (120% tailwater) and Washington TDG criteria adjustments (120% tailwater/115% forebay). The Oregon TDG standard modification and Washington TDG criteria adjustments have different methodologies for calculating TDG. When standards vary or conflict, the Corps applies the more stringent standard.

² Operations are implemented Monday through Sunday.

The weekly figures begin on August 3 and end on August 31 for the following lower Snake River and lower Columbia River projects: Lower Granite, Little Goose, Lower Monumental, Ice Harbor, McNary, John Day, The Dalles, and Bonneville.

Each figure represents one week of a project's operation. The figures start at 0000 hours (%TDG graphs) and 0100 hours (flow/spill figures) on August 3 for the lower Snake River and the lower Columbia River projects.

August 3 – August 9	Figures 1 – 8
August 10 – August 16	Figures 9 – 16
August 17 – August 23	Figures 17 – 24
August 24 – August 30	Figures 25 – 32
August 31	Figures 33 – 40

A. Upper Figure: Displays the daily average %TDG for the Corps' lower Snake River and lower Columbia River projects. The Corps' objective is to operate each project in accordance with the spill levels in the 2015 FOP; and to the extent practicable, avoid exceeding the applicable state TDG limits.

1. The green dashed line represents the observed percent TDG in the tailwater of the dam using the Oregon 120 %TDG standard calculated with the high 12-hour average.¹ Applies only to figures which include the lower Columbia dams.
2. The blue dot-dash line represents the observed percent TDG in the tailwater of the dam using the Washington 120 %TDG standard calculated with the high 12-hour average.¹
3. The black solid line represents the observed percent TDG in the forebay of the next dam downstream using the Washington 115 %TDG standard calculated with the high 12-hour average.¹

B. Lower Figure: Displays the hourly flow and spill at each dam.

- The dashed blue line shows the flow through the powerhouse each hour, in thousand cubic feet per second (kcfs).
- The heavy grey line represents the average hourly total project outflow in kcfs.
- The dotted pink line represents the average hourly flow through the spillway in kcfs.
- The thin black line represents the hourly spill level as defined in the 2015 FOP.
- The heavy green line represents the target spill. This is the hourly maximum spill level. The hourly target spill may vary as a function of total project outflow, forebay elevation and generator capacity, subject to the following conditions:
 - spill percentage or flow rate specified in the 2015 FOP;
 - spill caps as set daily for TDG management;
 - test spill levels for fish passage research;
 - minimum generation for power system needs;
 - minimum spill at Bonneville Dam (50 kcfs);
 - minimum spill at John Day (25% of project outflow).

II. A table is included at the end of the figures that lists the daily average of high %TDG values for all projects. The numbers in red indicate the project exceeded the %TDG cap -- i.e. 115% (forebay of the next downstream dam) or 120% (tailwater) for each project. For the lower Columbia projects, tailwater TDG values are presented by displaying the highest value %TDG (controlling limit), and the lower value is displayed with a strikethrough.

General Implementation Remarks

For all projects that spill for fish passage, the actual spill may vary from the target spill due to various conditions as described below. When spill levels briefly deviate below or above the level specified in the 2015 FOP, the dotted pink line will be below or above the heavy green line in the figures. Actual deviations from the target operation during voluntary spill hours are described below in the August 2015 Spill Variance Table.³ The Spill Variance Table includes average hourly data; therefore, while spill may vary from target FOP spill for only a portion of an hour, the Spill Variance Table characterizes the variance as a full hour. There are instances when the hourly FOP spill levels are not achievable due to mechanical limitations in setting spill gates to implement the regionally coordinated spill pattern. The project operator sets the spill gate stops to most closely approximate the 2015 FOP level of spill while also avoiding exceeding the %TDG spill cap to the extent practicable.

"Low flow" operations at the lower Columbia and Snake projects are triggered when inflow is insufficient to provide both minimum generation and the specified spill levels. In these situations, the projects operate at minimum generation and pass the remainder of project inflow as spill and through other routes, such as fish ladders, sluiceways, and navigation locks. As flows transition from higher flows to low flows, there may be situations when flows recede at a higher rate than forecasted. In addition, inflows provided by nonfederal projects upstream are variable and uncertain.

The combination of these factors may result in instances when unanticipated changes to inflow result in forebay elevations dropping to the low end of the Minimum Operating Pool (MOP). Since these projects have limited operating flexibility, maintaining minimum generation, MOP elevation, and the target spill may not be possible throughout every hour. During low flow periods at Little Goose Dam, the overall project spill percentage appears to be reduced because the calculations do not account for the volume of water released during navigational lockages; however, the actual spill volume remains constant. When these variances occur, they are recorded in the monthly Spill Variance Table for Little Goose under the variance type "Navigation."

Actual spill levels at Corps projects with set flow targets may vary up to ± 2 kcfs within the hour (except as otherwise noted in the 2015 FOP for Bonneville and The Dalles dams,⁴ which may

³ Involuntary spill conditions may appear in the figures but are not considered variances and are not reported in the Spill Variance Table. Involuntary spill conditions result from lack of load, high river inflows that exceed available powerhouse capacity, scheduled or unscheduled turbine unit outages or transmission outages of various durations, passing debris, or any other operational and/or maintenance activities required to manage dam facilities for safety and authorized project uses.

⁴ As specified in the 2015 FOP (p. 14), this applies when spill is below 40% of total outflow at The Dalles Dam.

range up to ± 3 kcfs) as compared to those specified in the 2015 FOP and the RCC spill priority list (defining the project %TDG spill caps). A number of factors influence actual spill, including hydraulic efficiency, exact gate opening calibration, spillway gate hoist cable stretch due to temperature changes, and forebay elevation (e.g. a higher forebay results in a greater volume of spill since more water can pass under the spill gate).

The 2015 FOP describes project “Operations during Rapid Load Changes” (p. 6). For reporting purposes, the notation “Transmission Stability” in the Spill Variance Table replaces “Rapid Load Changes,” and identifies instances when hourly spill levels were not met as a result of load swing hours and other related within-hour load variability issues. “Transmission Stability” occurs because projects must be available to respond to within-hour load variability to satisfy North American Electric Reliability Corporation (NERC) reserve requirements (“on response”). In addition to within-hour load variability, projects on response must be responsive to within hour changes resulting from intermittent generation (such as wind generation). During periods of rapidly changing loads and intermittent generation, projects on response may have significant changes in turbine discharge within the hour while spill quantity remains the same within the hour. Under normal conditions, within-hour load changes primarily occur immediately preceding and following the peak load hours; however, within-hour changes in intermittent generation can occur at any hour of the day. Occasionally, several hours after peak load hours, the project may be decreasing total outflow and generation faster than the corresponding spill decreases causing the percent spill to be slightly higher. Due to the high variability of within-hour load, reporting actual spill percentages that vary by more than the ± 1 percent within hour requirement (or other ranges specified in the 2015 FOP) may occur with greater frequency with “Transmission Stability” hours than other hours.

Occurrences requiring an adjustment in operations and/or regional coordination are described in greater detail in the “Operational Adjustments” section below.

August 2015 Operations

The month of August was characterized by well below average flows for both the lower Snake and the lower Columbia rivers. The NOAA Northwest River Forecast Center’s Runoff Processor indicated that the August 2015 adjusted volume runoff on the lower Snake River was below the 30 year average (1981-2010): 0.9 MAF (Million Acre Feet) or 70% of average as measured at Lower Granite Dam. For the lower Columbia River, the Runoff Processor indicated the August 2015 adjusted volume runoff was below the 30 year average (1981-2010): 5.2 MAF or 68% of average as measured at The Dalles. The monthly precipitation summary for August was well below average at 56% on the Snake River above Ice Harbor Dam and below average on the Columbia River above The Dalles Dam at 64%.

During the August 2015 reporting period, the planned 2015 FOP spill operations were carried out as follows:

- Lower Granite Dam - The hourly target spill level was 18 kcfs, 24 hours/day.
- Little Goose Dam - The hourly target spill level was 30% of total project outflow, 24 hours/day. Due to low flow conditions, the operation transitioned to an hourly constant spill

target of 7/9/11 kcfs operation⁵, depending on the previous day's outflow as coordinated with TMT on June 25.

- Lower Monumental Dam - The hourly target spill level was 17 kcfs, 24 hours/day.
- Ice Harbor Dam - The hourly target spill level was 45 kcfs spill during the daytime and the %TDG cap spill during the nighttime. Nighttime spill hours (1800-0500).
- McNary Dam - The hourly target spill level was 50% of total project outflow, 24 hours/day.
- John Day Dam - The hourly target spill level was 30% of total river flow for 24 hours/day.
- The Dalles Dam - The hourly target spill level was 40% of total project outflow, 24 hours/day.
- Bonneville Dam - The hourly target spill level alternated in 2-day blocks between 95 kcfs, 24 hours/day vs. 85 kcfs during the day and 121 kcfs during the nighttime.

Operational Adjustments

No Operational Adjustments to report.

⁵ See FOP (p. 6) for low flow operations at Little Goose Dam.

August 2015 Spill Variance Table

Project	Parameter	Date	Time ⁶	Hours	Type	Reason
Lower Granite	Reduced Spill	8/26/15	1300	1	Maintenance	Hourly spill was reduced from 5.9 kcfs to 3.2 kcfs to operate unit 4 for maintenance in addition to operating unit 2 at minimum generation (FOP Table 1).
John Day	Additional Spill	8/31/15	2300	1	Transmission Stability	Hourly spill increased to 33.1% (above 30% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg. spill 30.1%.
The Dalles	Reduced Spill	8/14/15	1200	1	Transmission Stability	Hourly spill decreased to 38.9% (below 40% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg. spill 39.9%.
The Dalles	Reduced Spill	8/29/15	2000	1	Transmission Stability	Hourly spill decreased to 38.4% (below 40% \pm 1% range). Project on response during rapidly changing load and/or intermittent generation (see p. 3-4). 24-hr avg. spill 39.9%.
Bonneville	Additional Spill	8/8/15	0100	1	Operational Limitations	Hourly spill increased to 99.4 kcfs (above 95 kcfs FOP spill). Operation for offloading a transformer from a barge ended earlier than planned and required drafting the Bonneville pool to resume the normal forebay operating range. 24-hr avg. spill 95.2 kcfs.

⁶ Note: Data collected for reporting spill variances is reported using hourly-averaged data. Therefore, while spill may be increased or decreased for only a portion of an hour, it is represented in the Spill Variance Table as an hour.

Figure 1

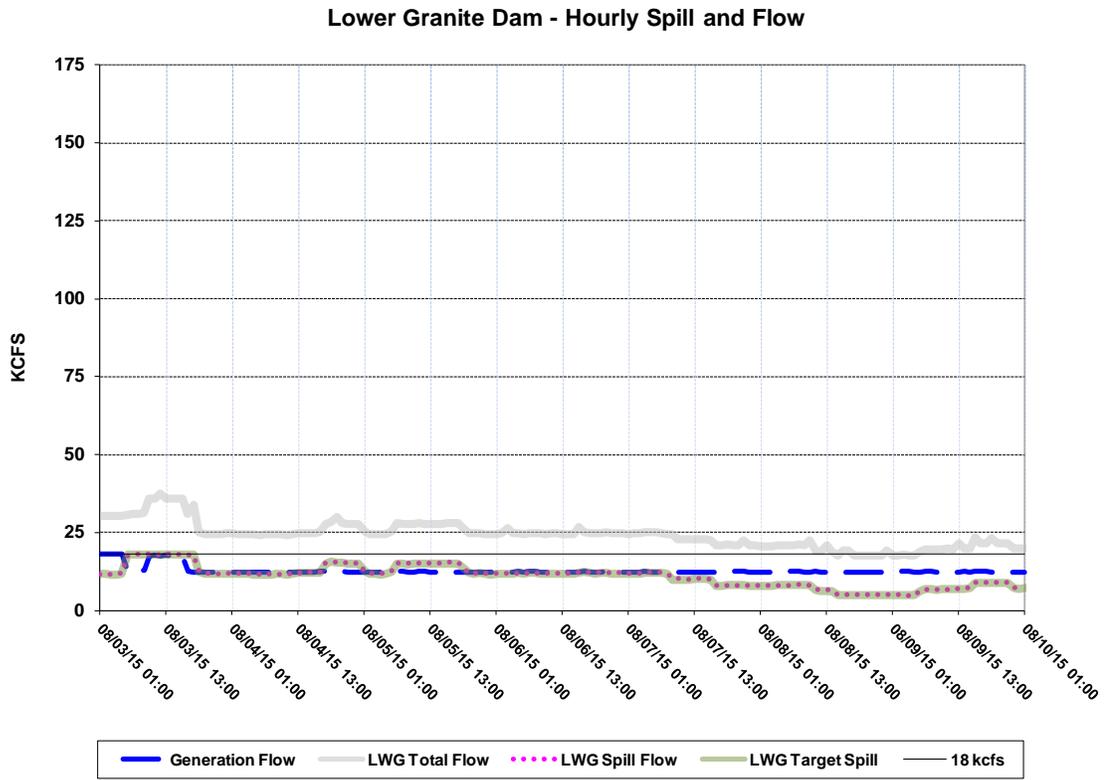
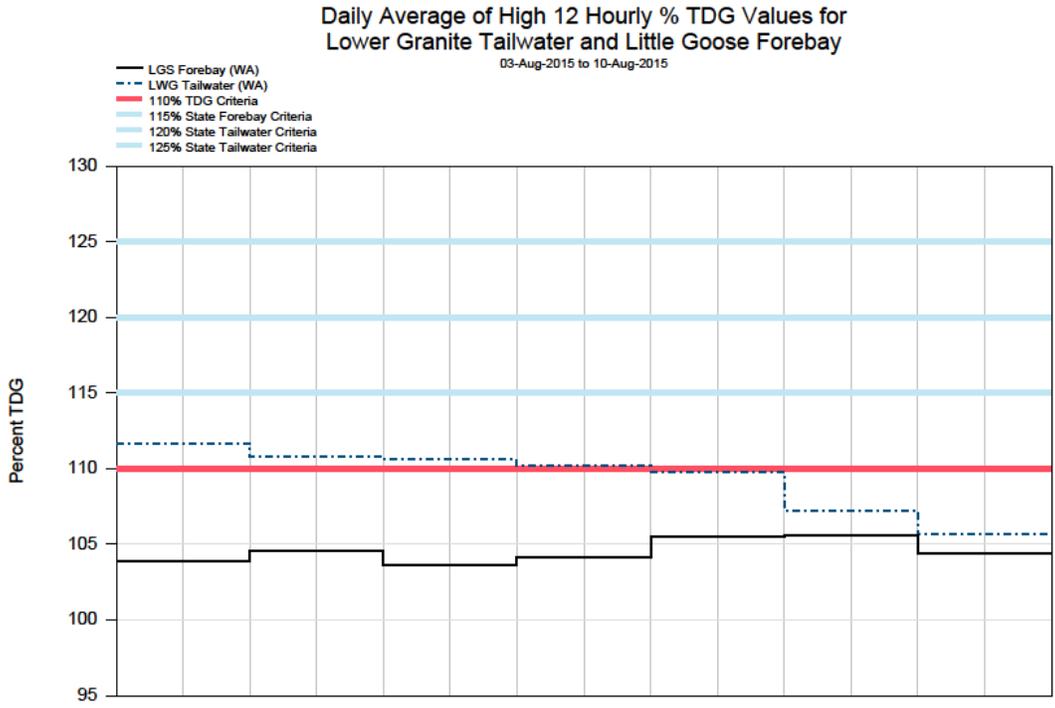


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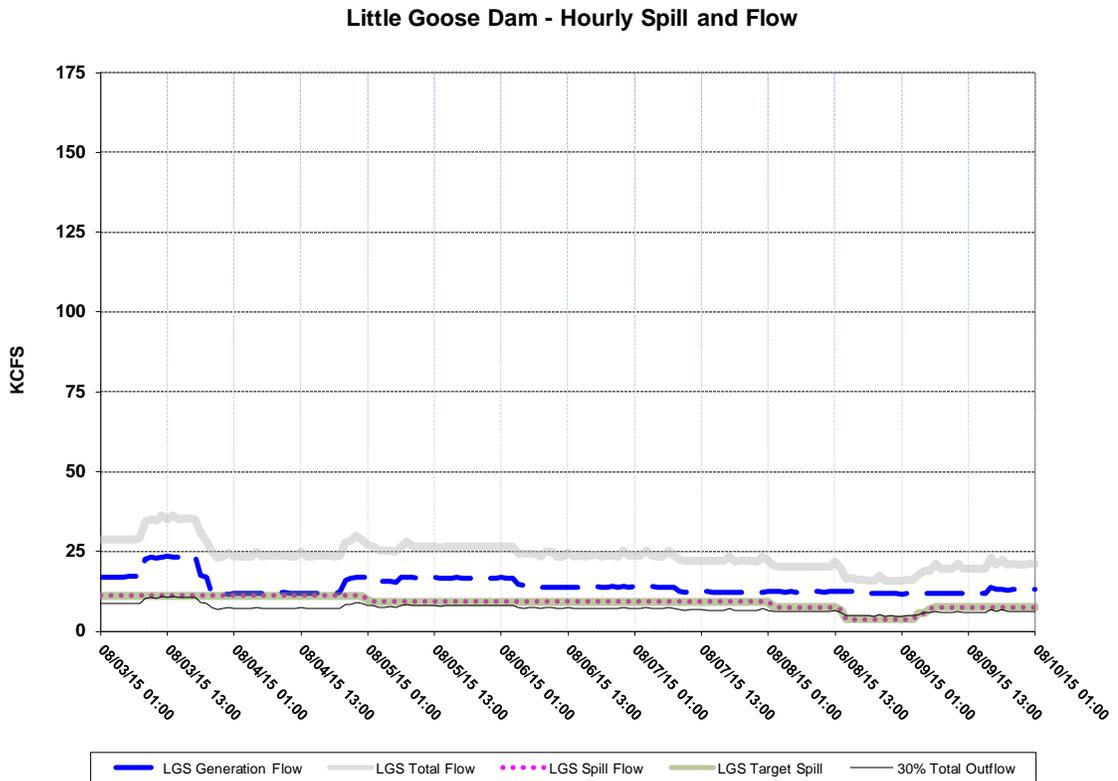
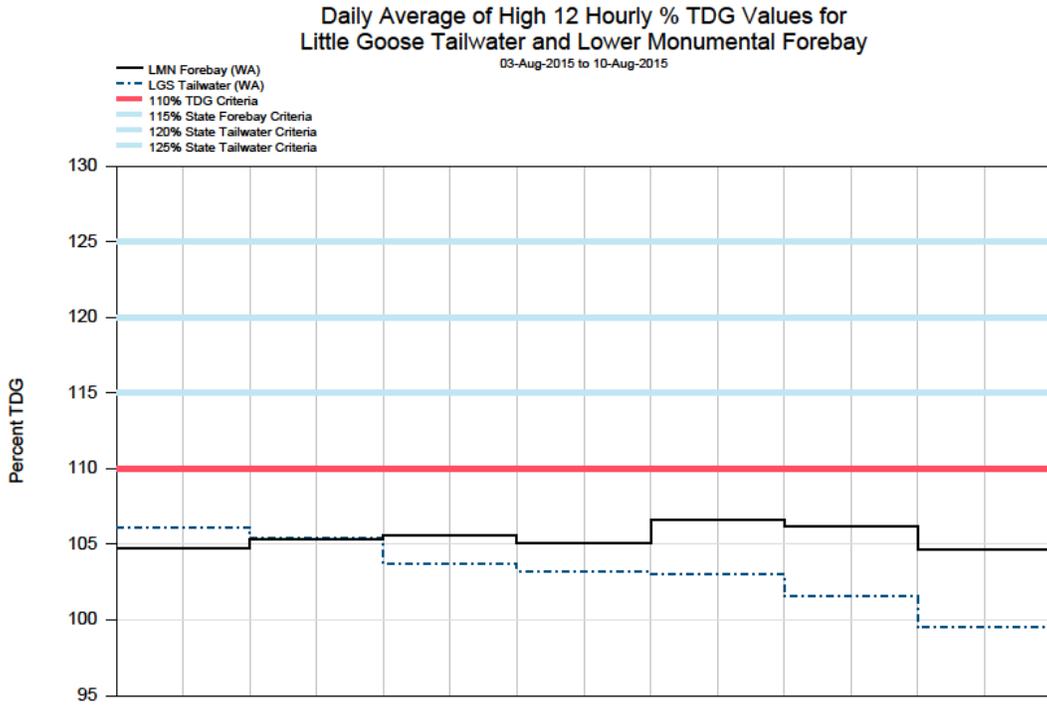


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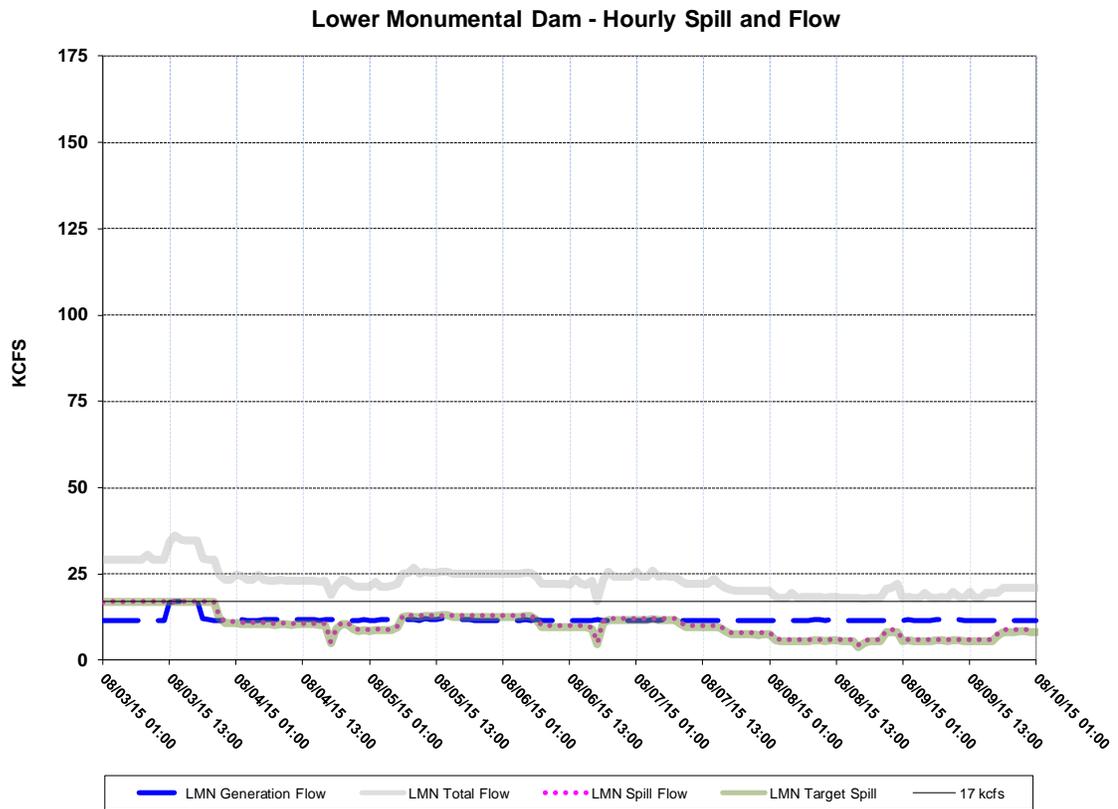
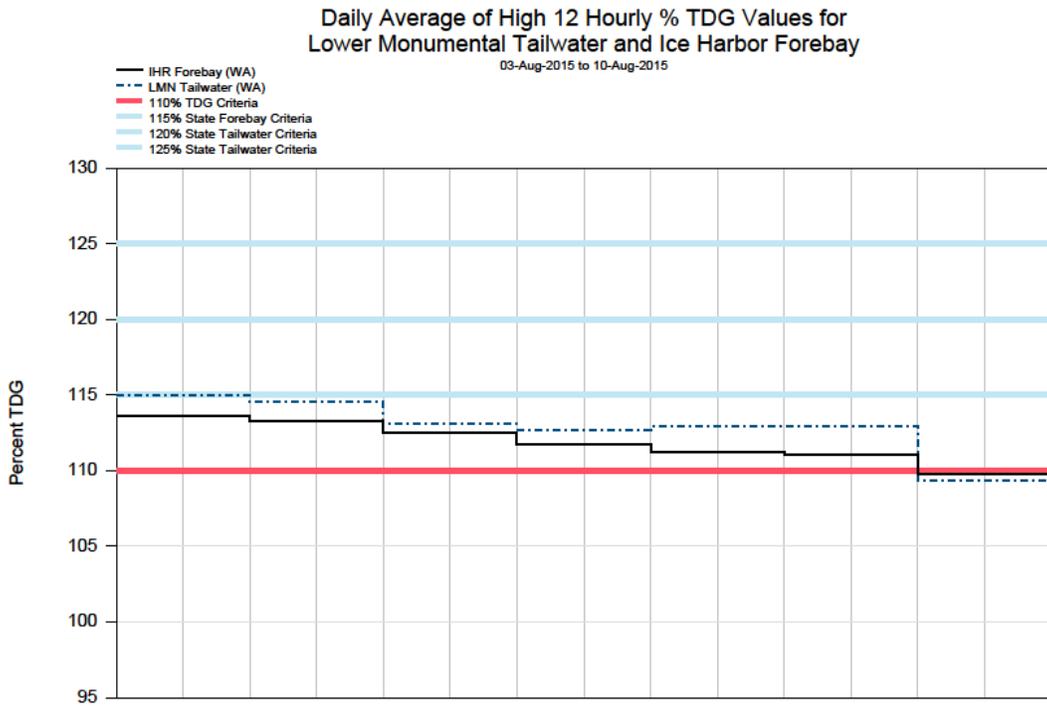


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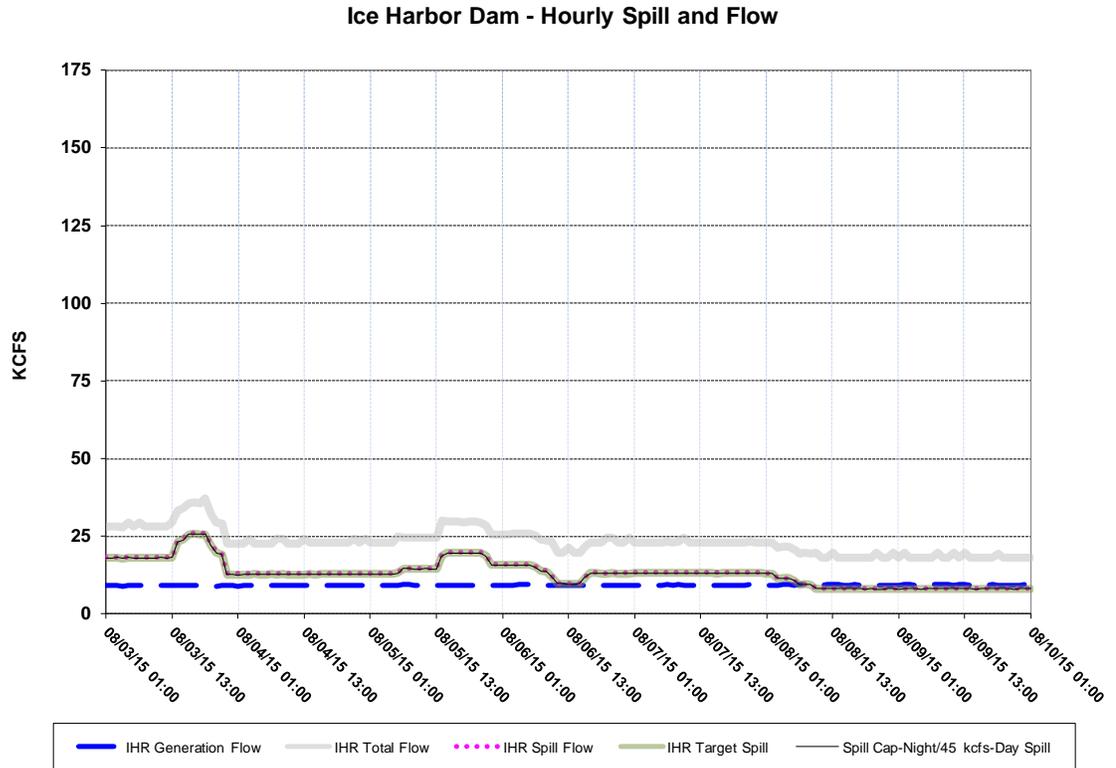
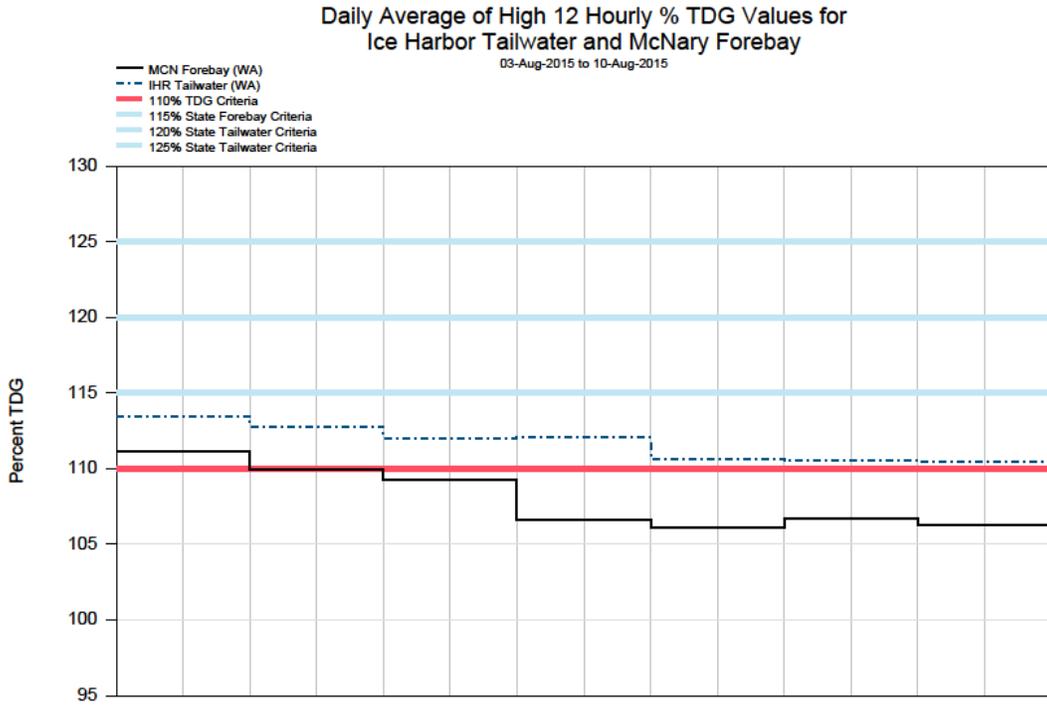


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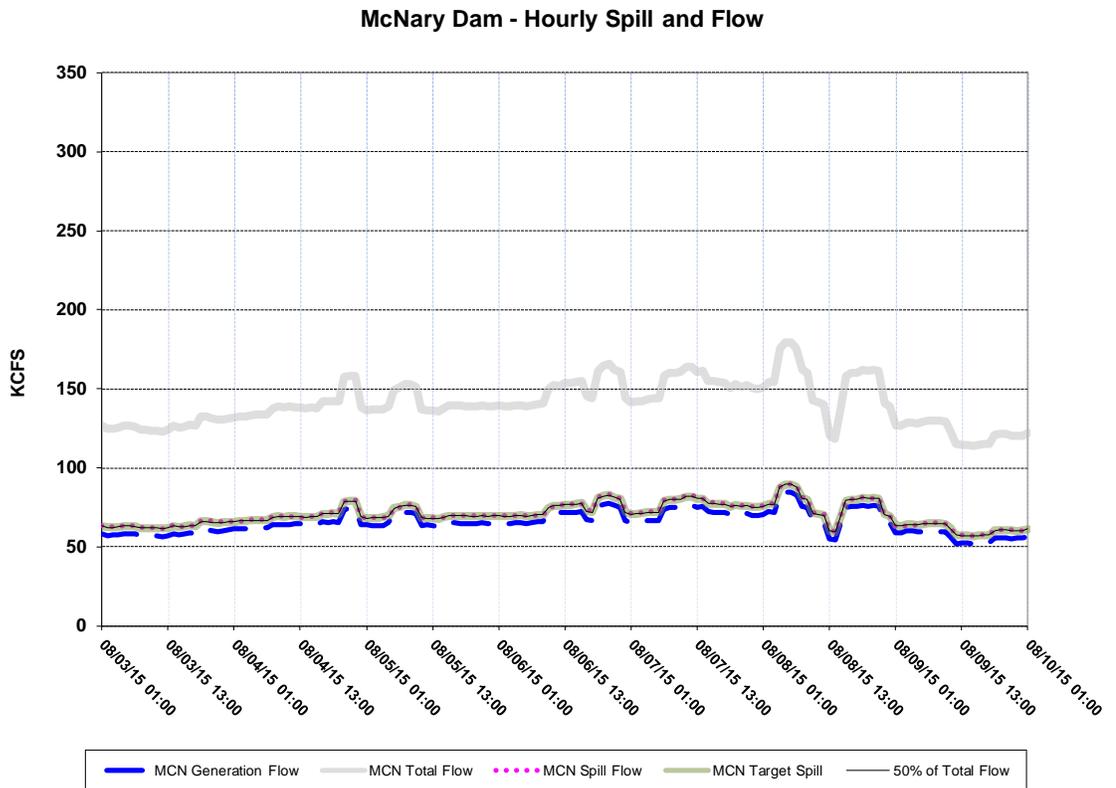
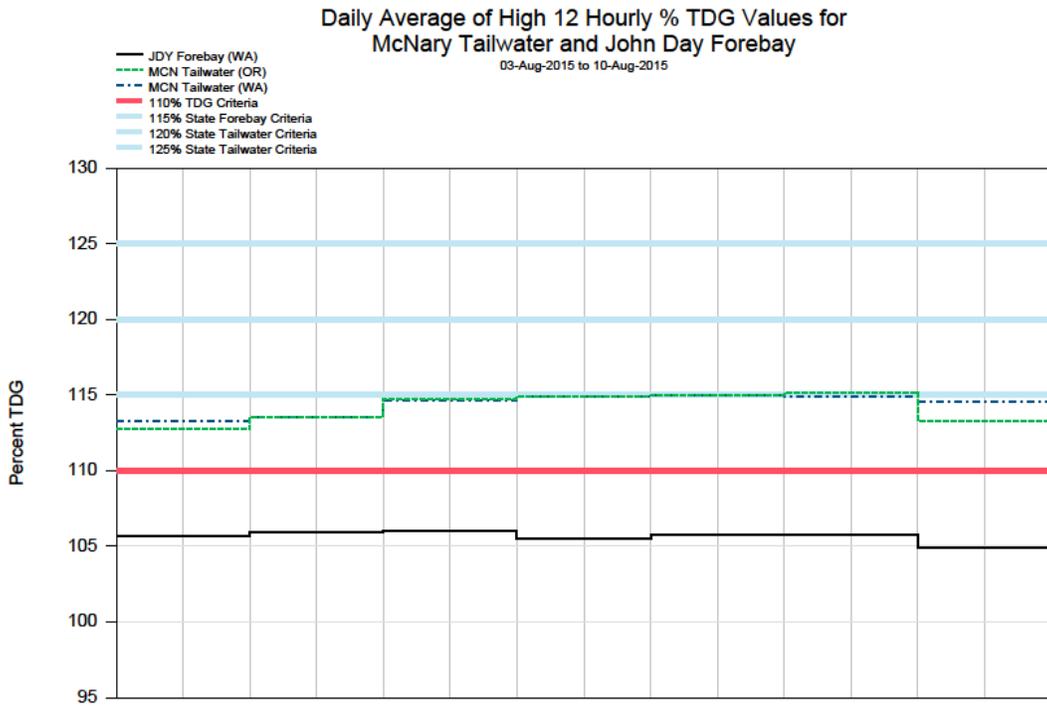


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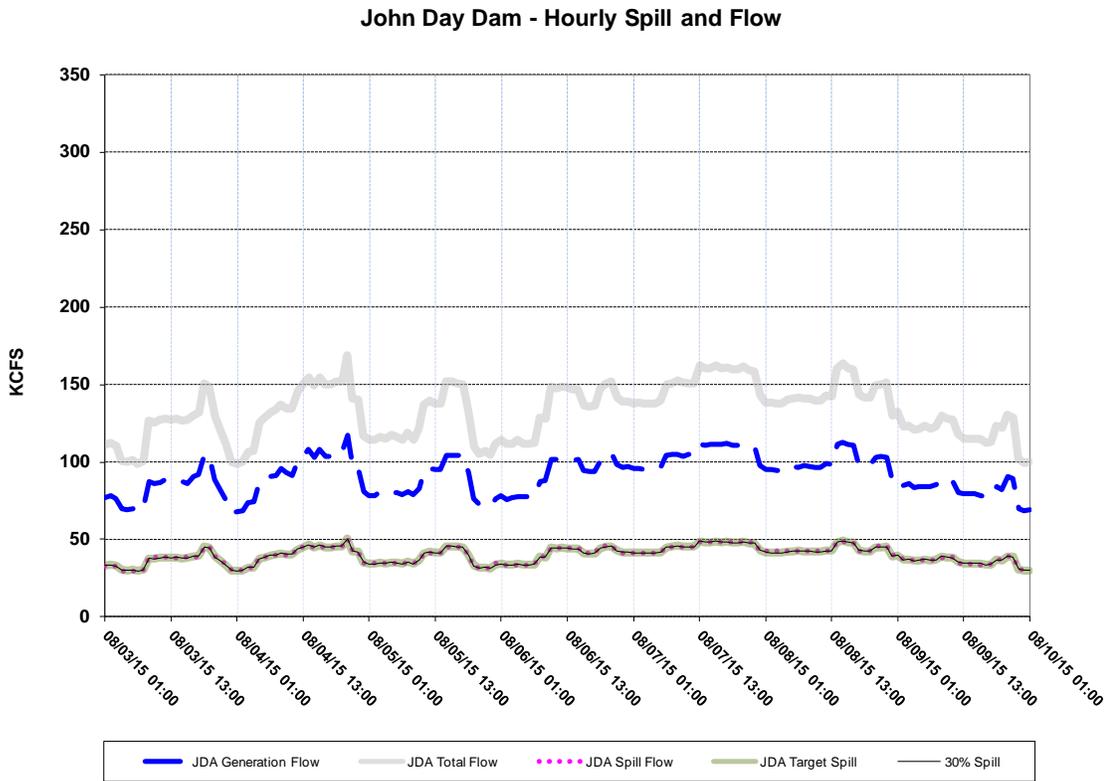
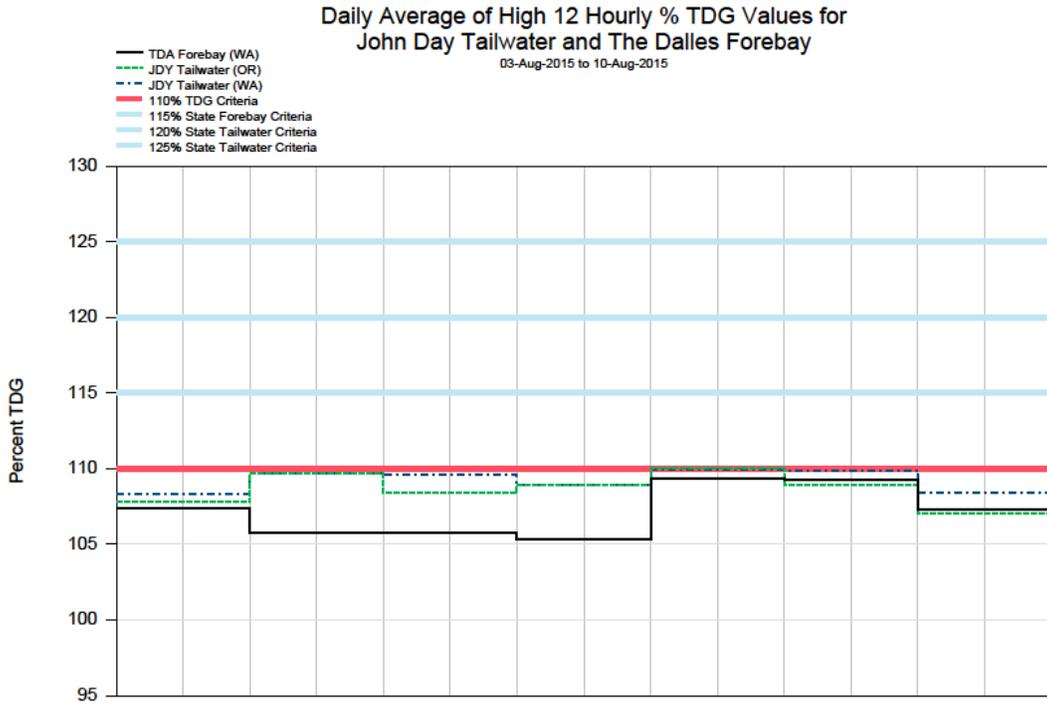


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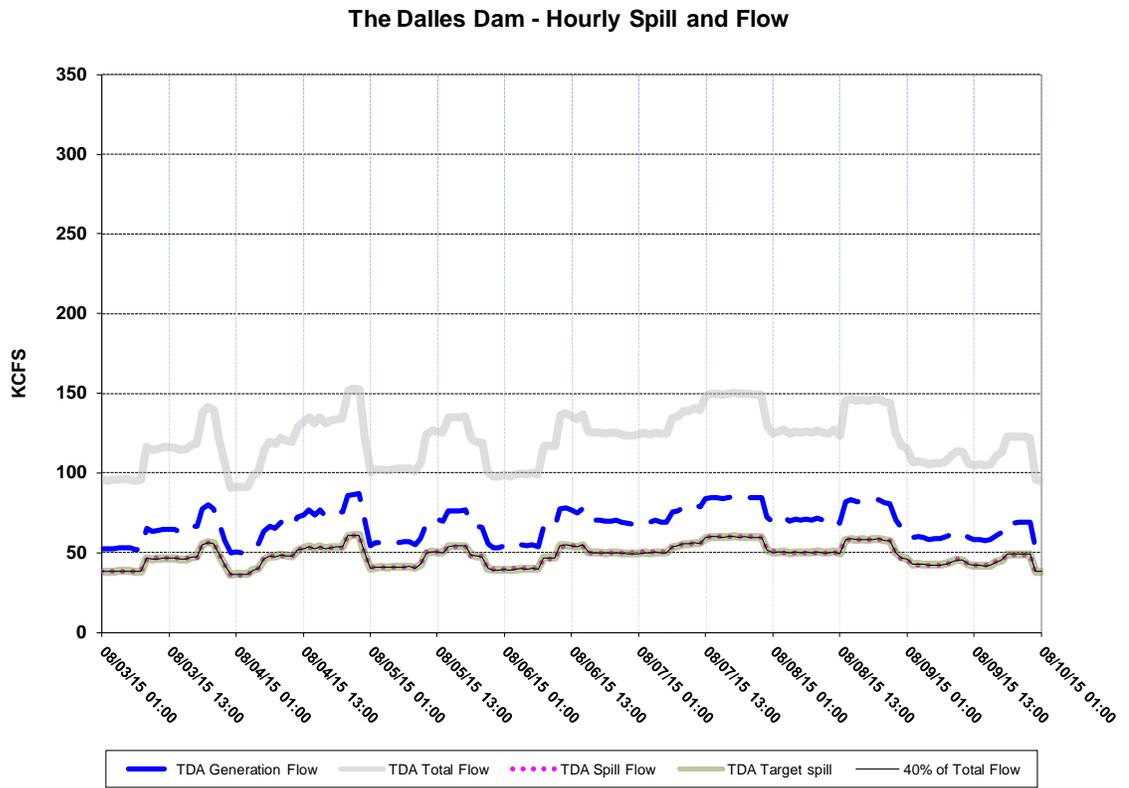
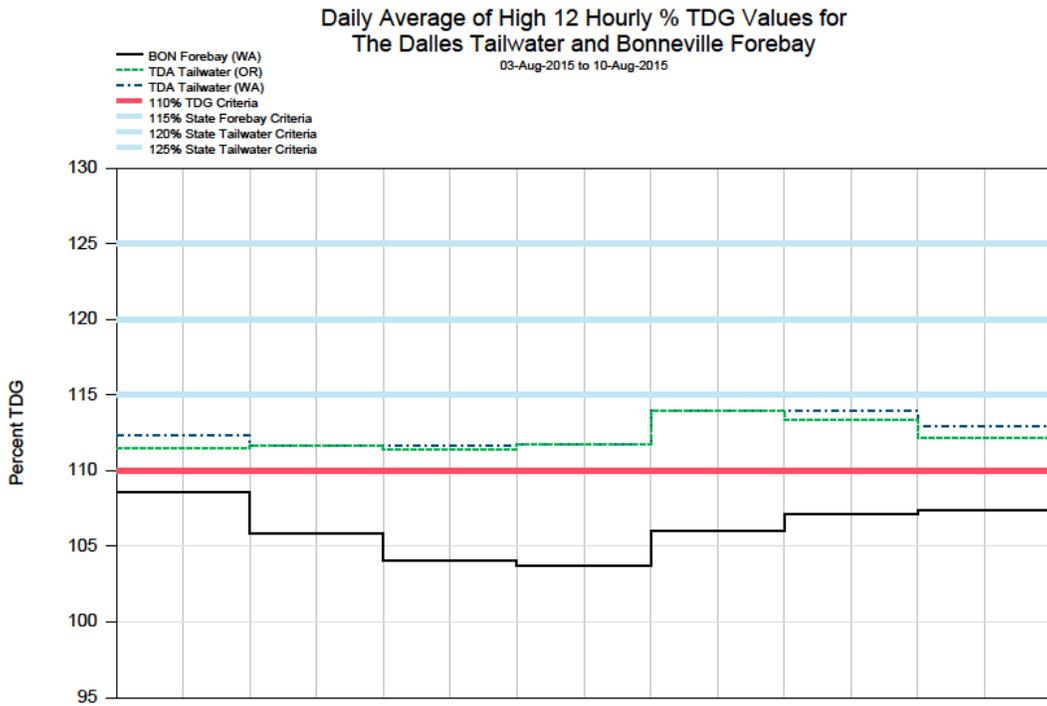


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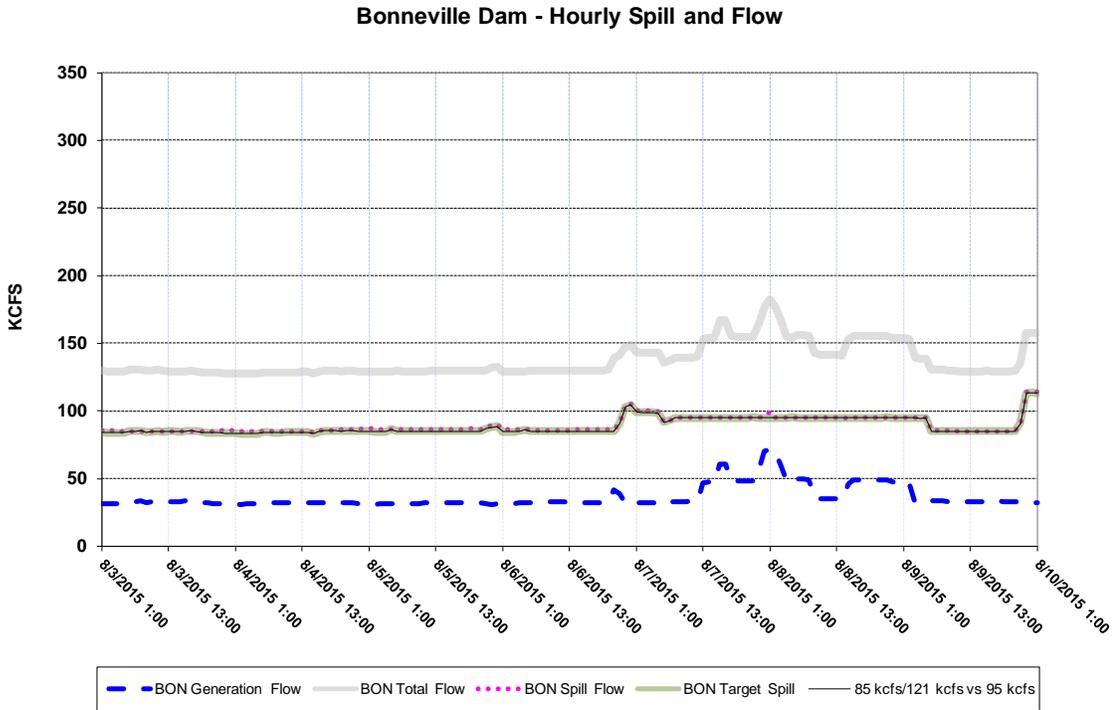
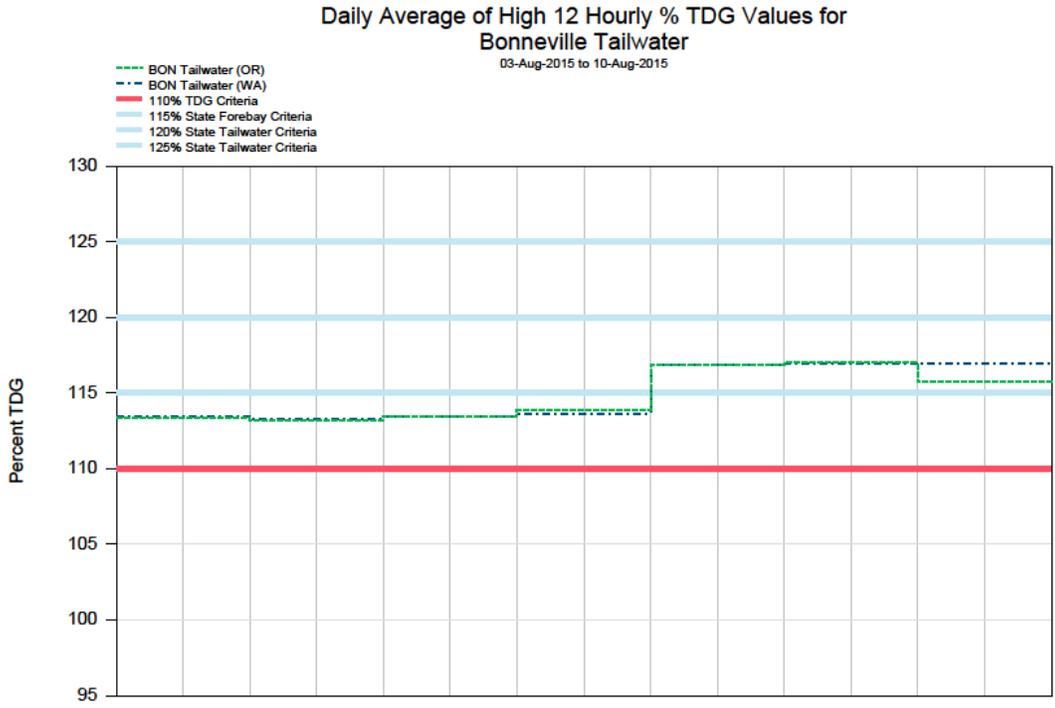


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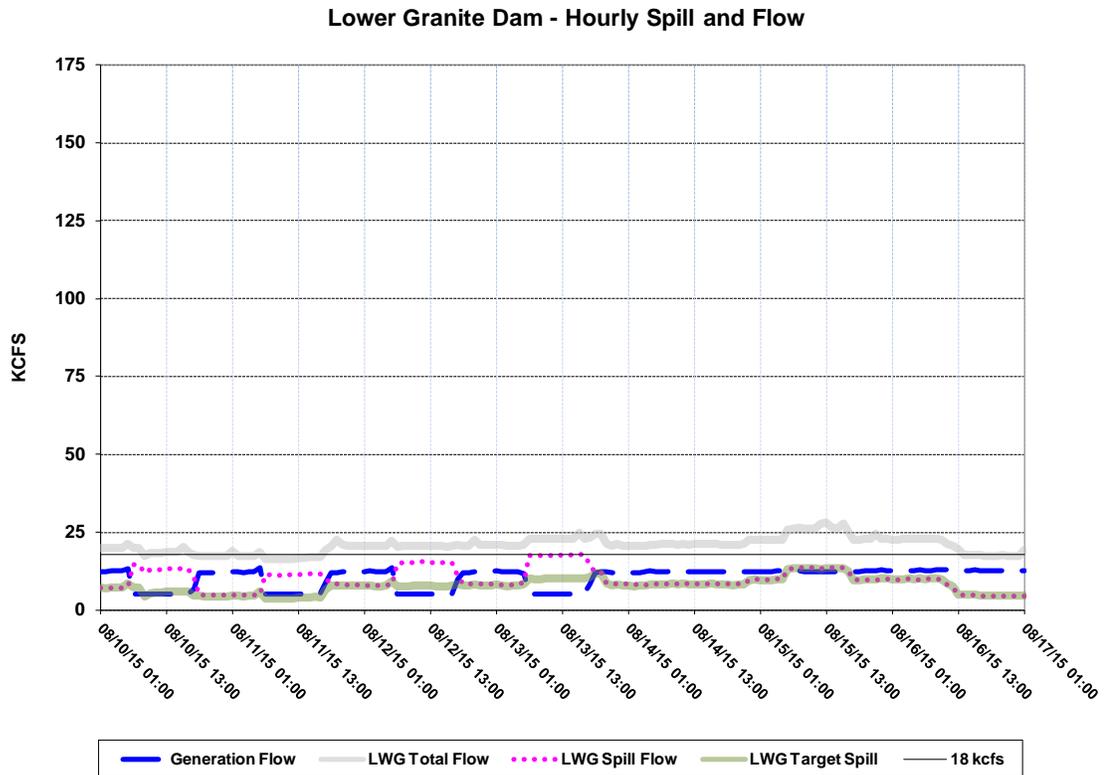
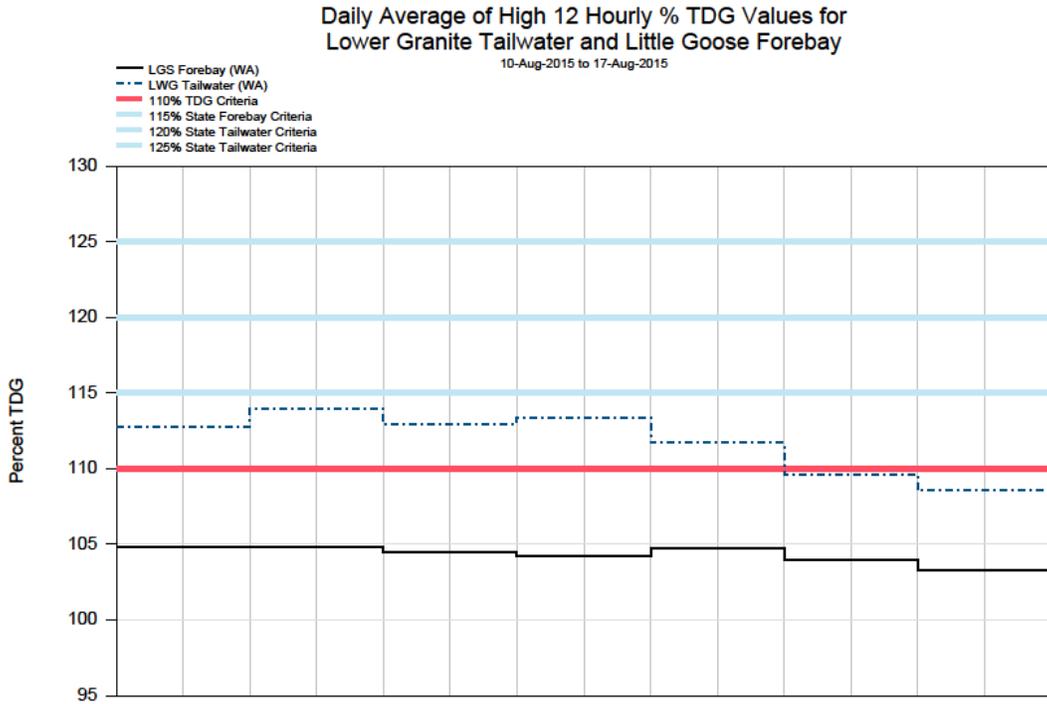


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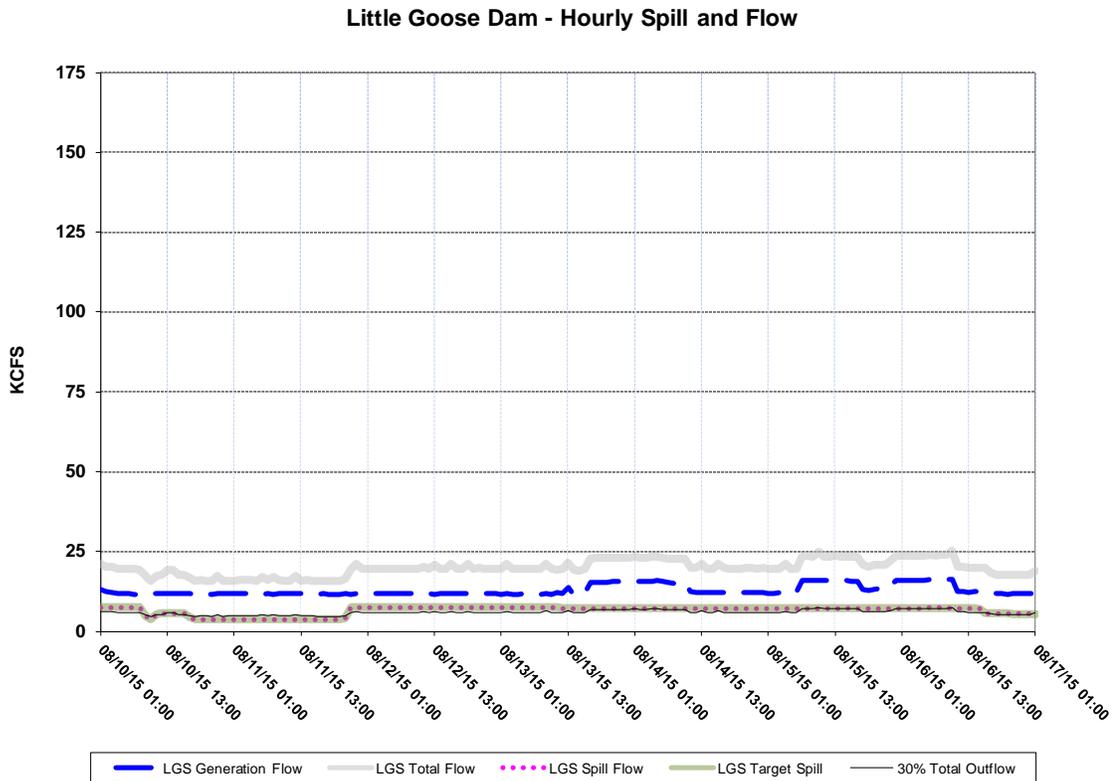
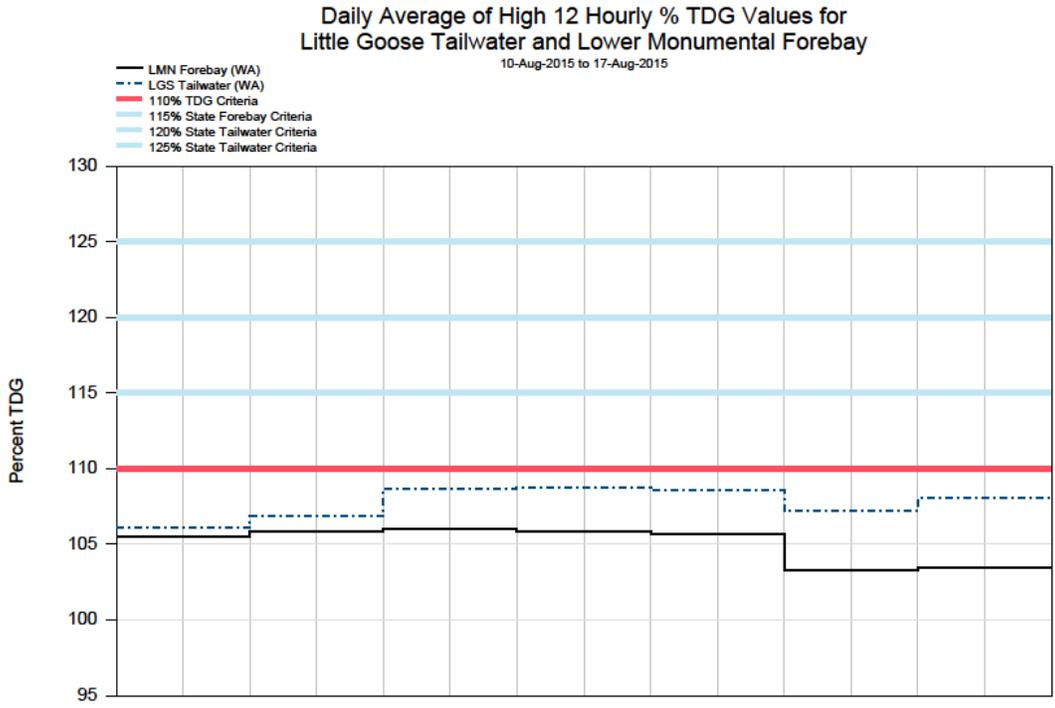


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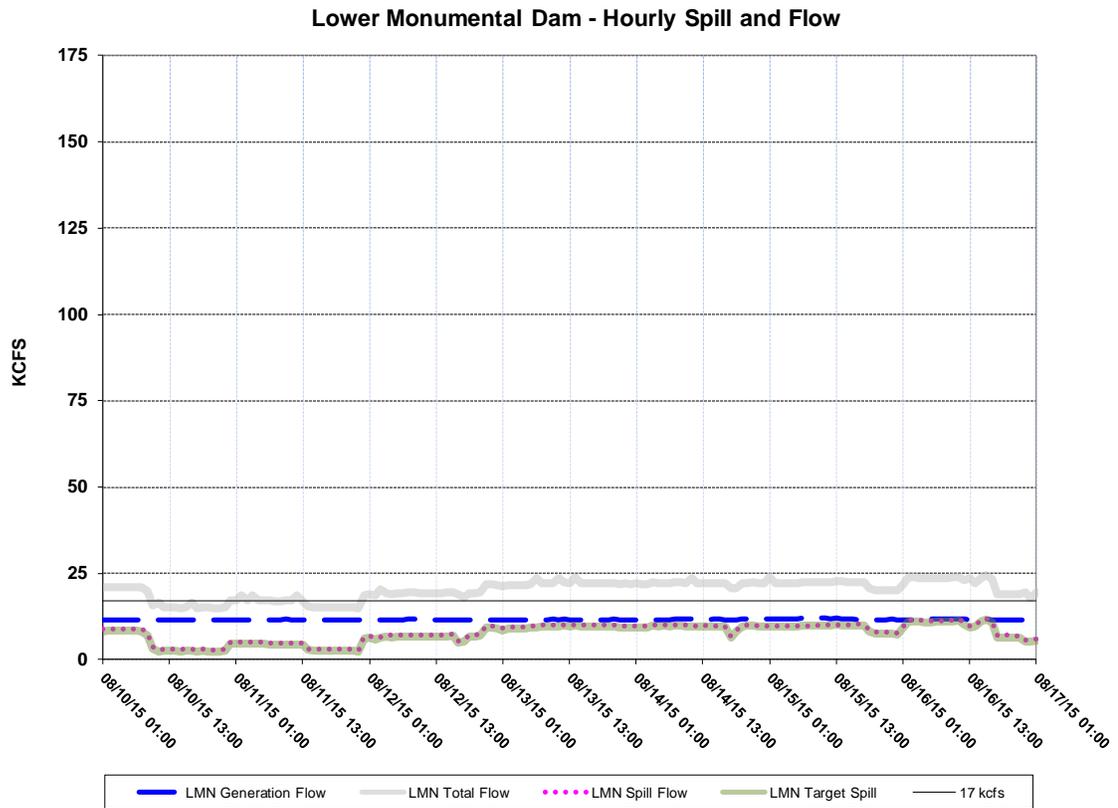
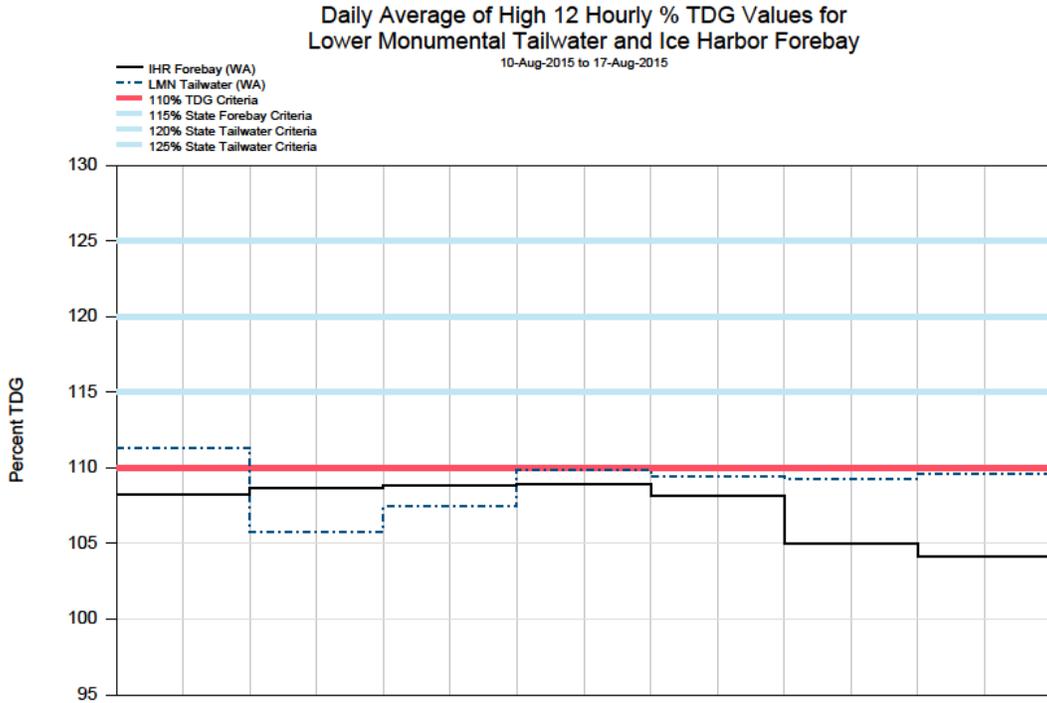
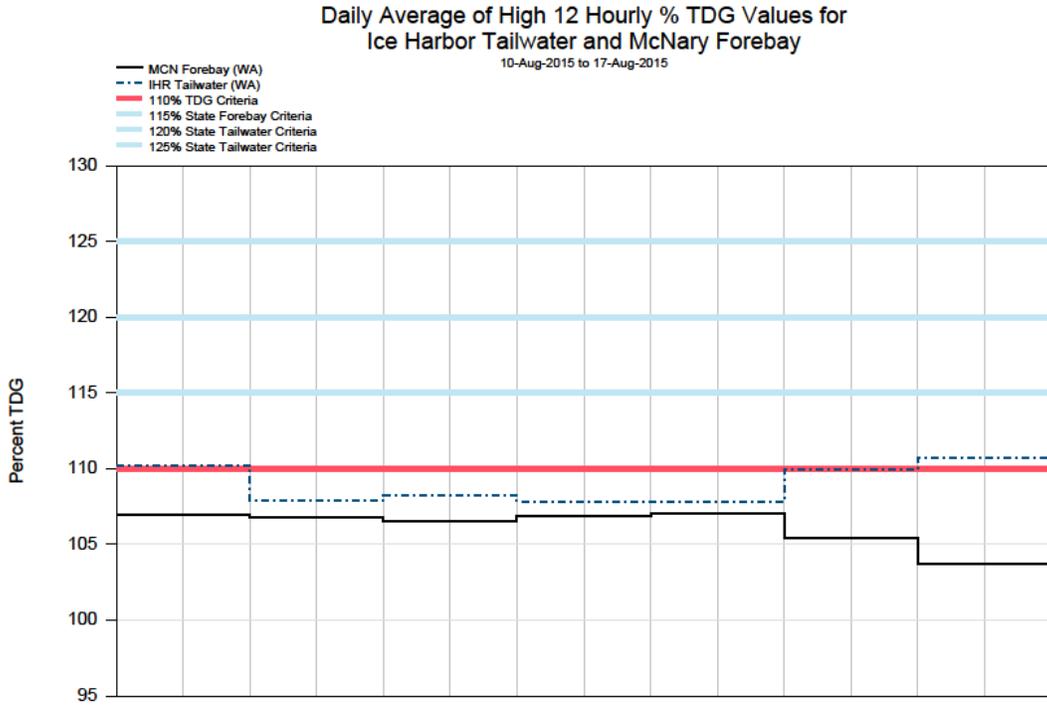


Figure 12



Ice Harbor Dam - Hourly Spill and Flow

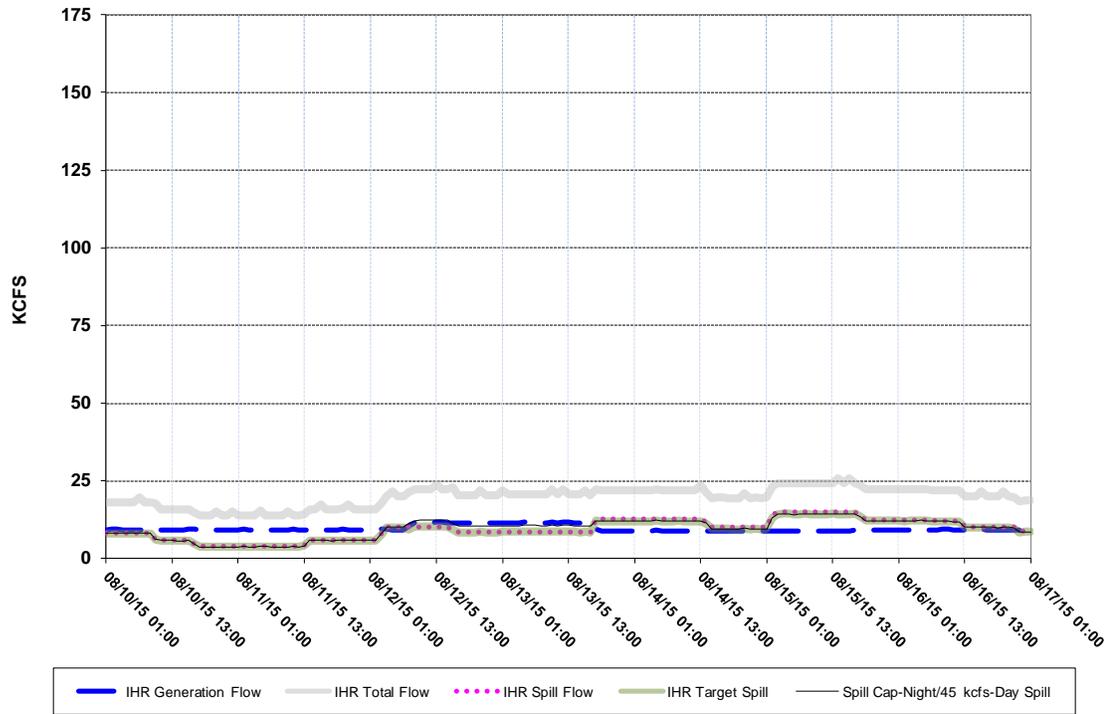


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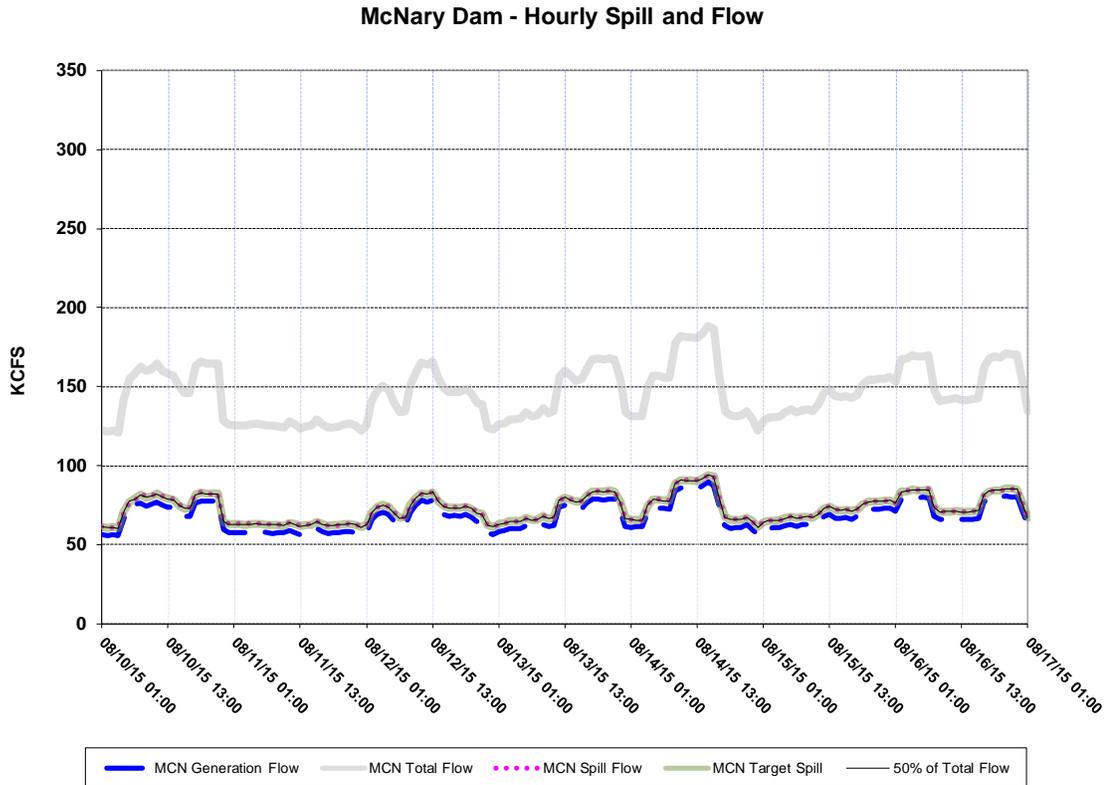
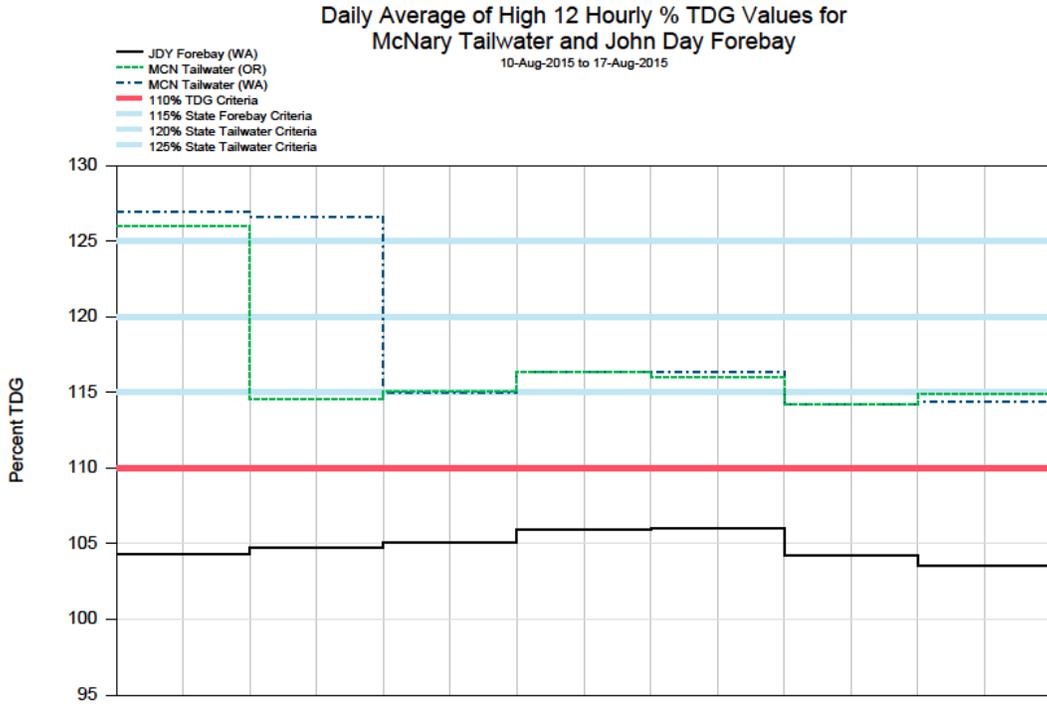


Figure 14

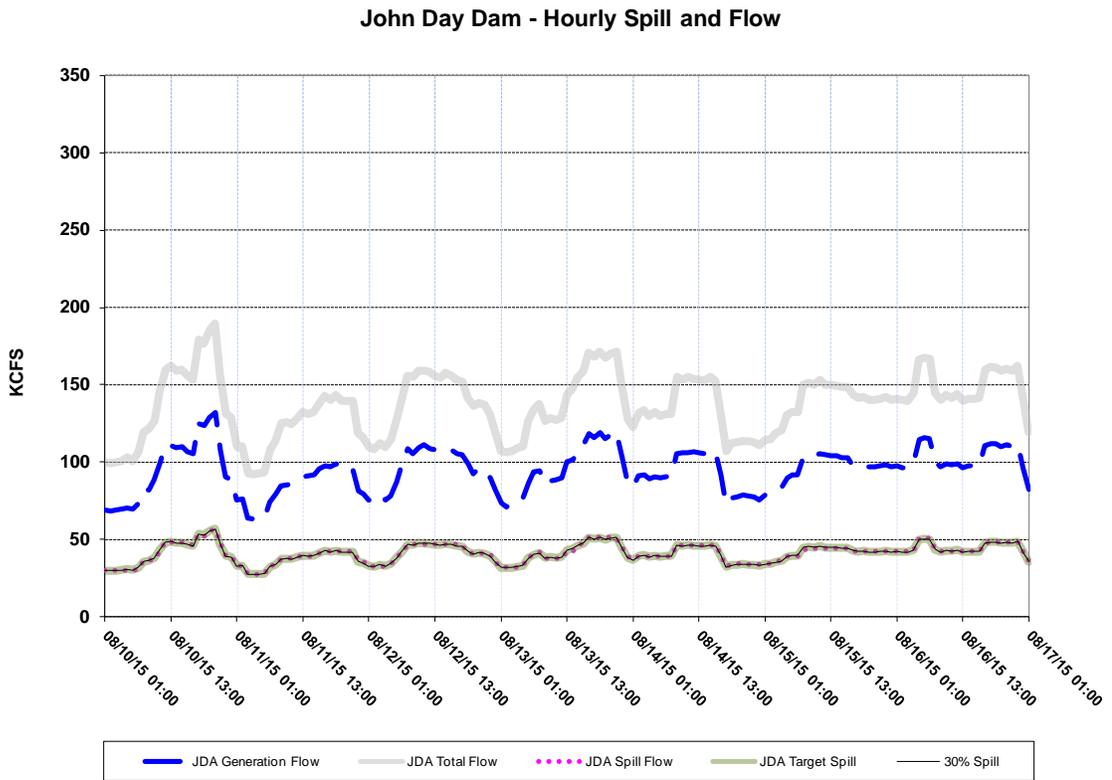
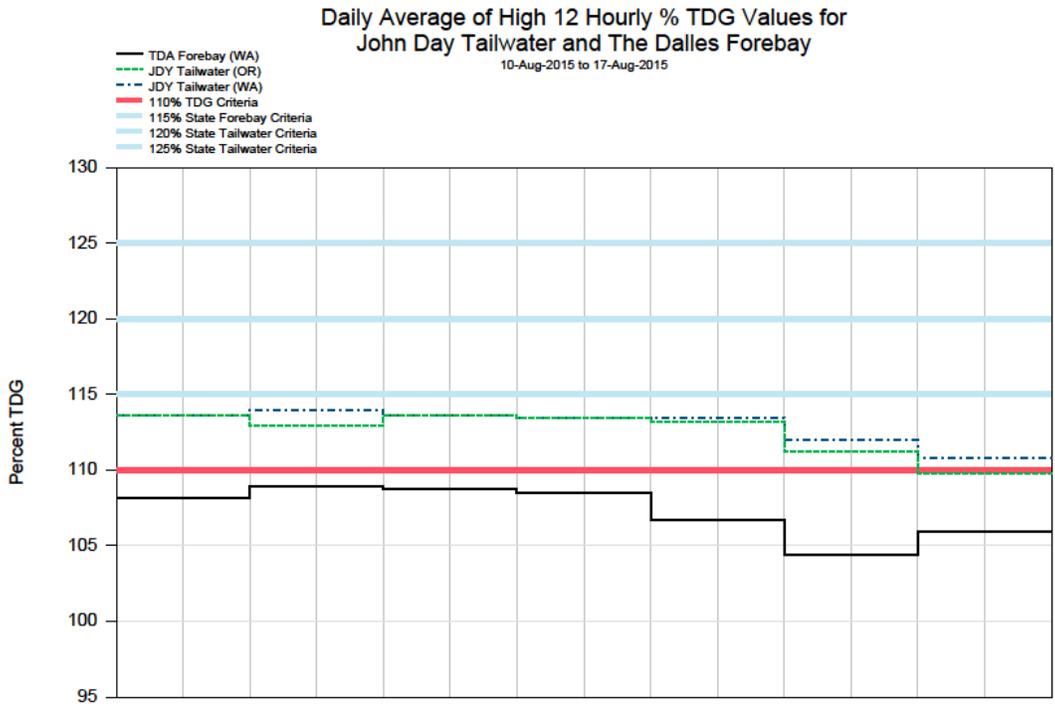
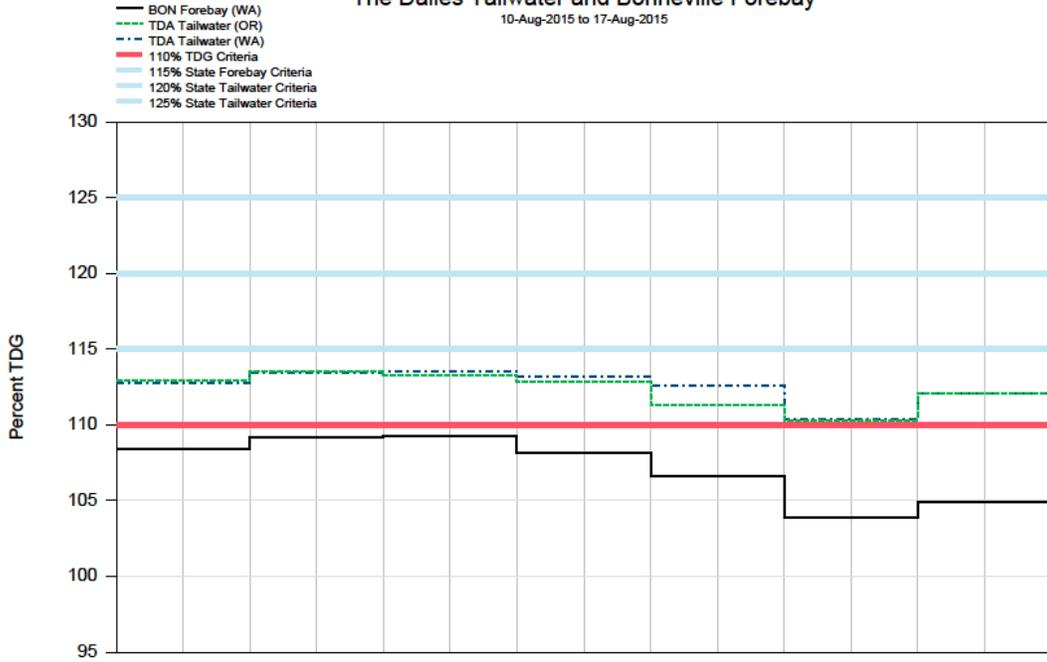


Figure 15

**Daily Average of High 12 Hourly % TDG Values for
The Dalles Tailwater and Bonneville Forebay**
10-Aug-2015 to 17-Aug-2015



The Dalles Dam - Hourly Spill and Flow

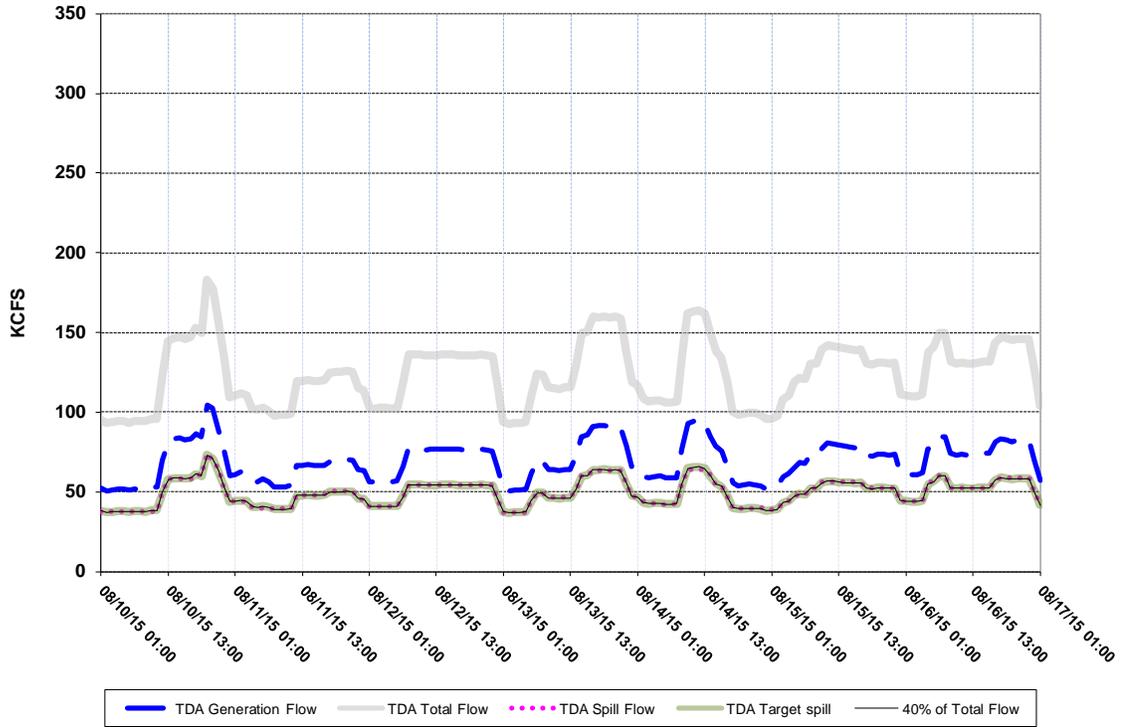
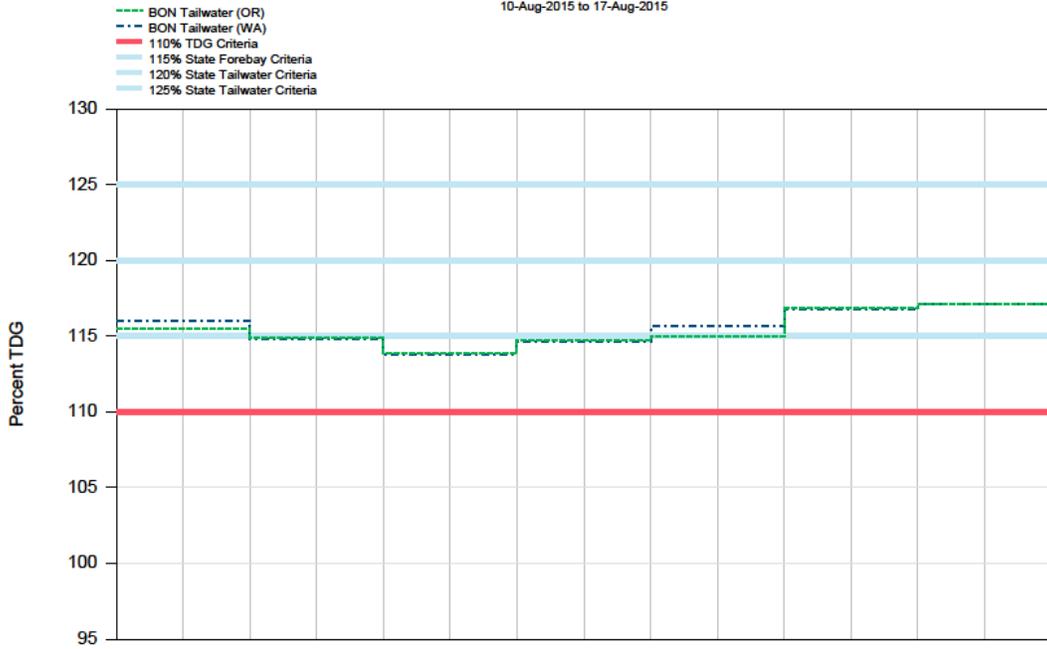


Figure 16

Daily Average of High 12 Hourly % TDG Values for Bonneville Tailwater

10-Aug-2015 to 17-Aug-2015



Bonneville Dam - Hourly Spill and Flow

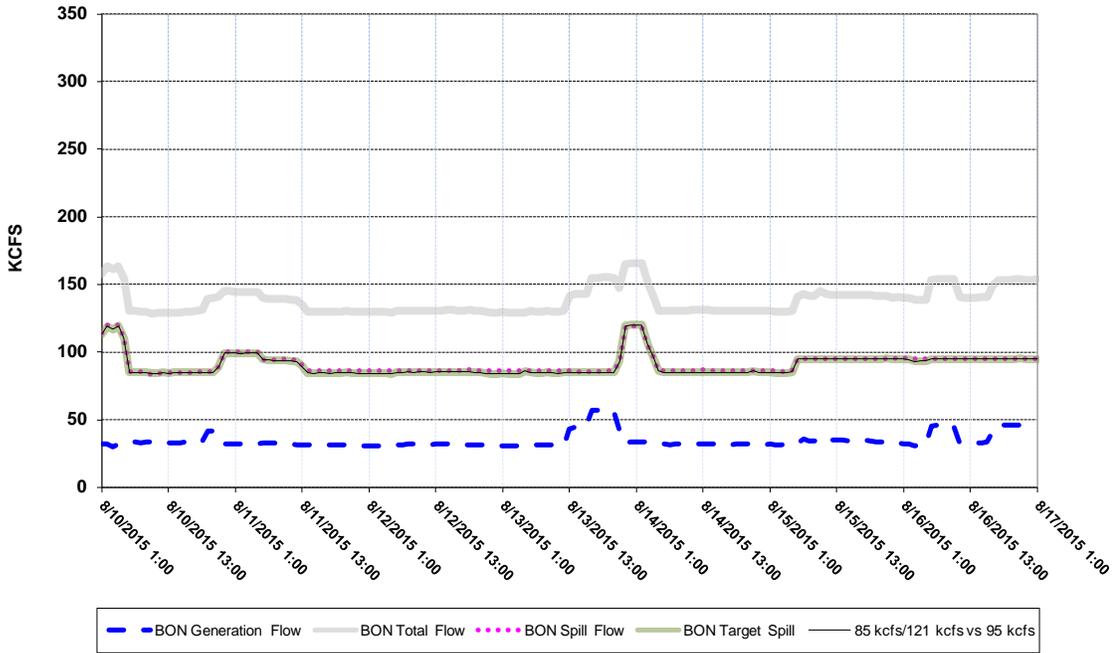


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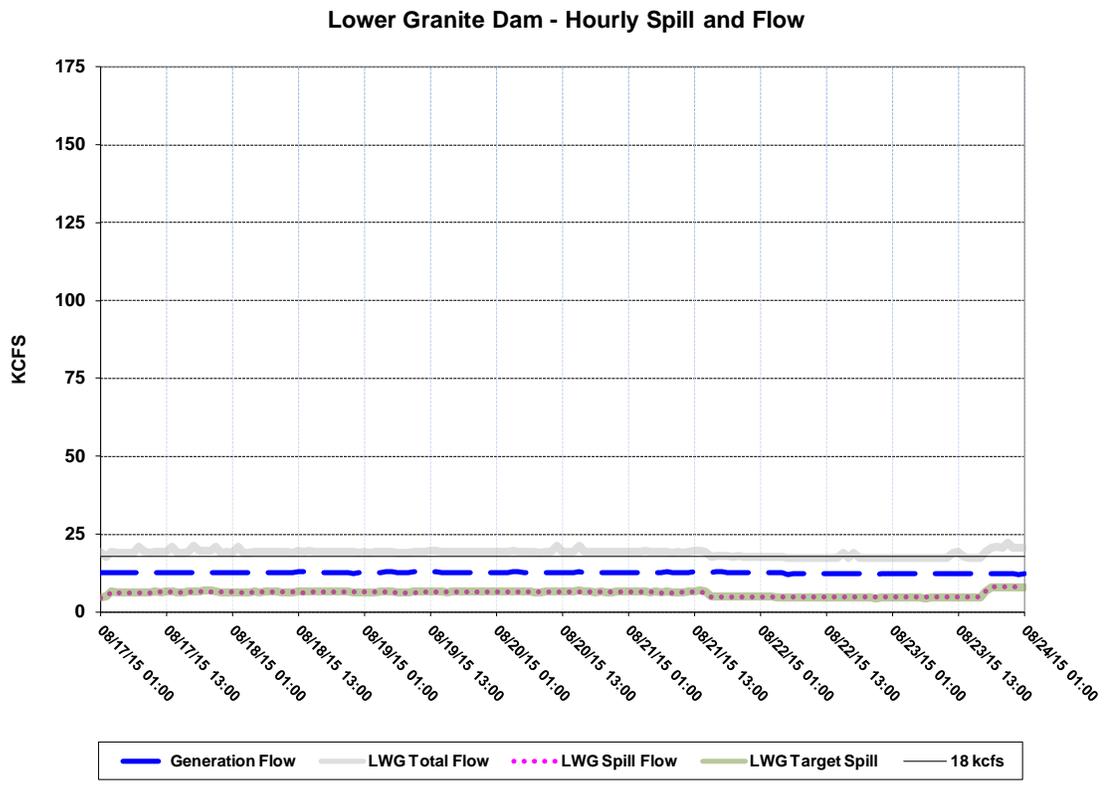
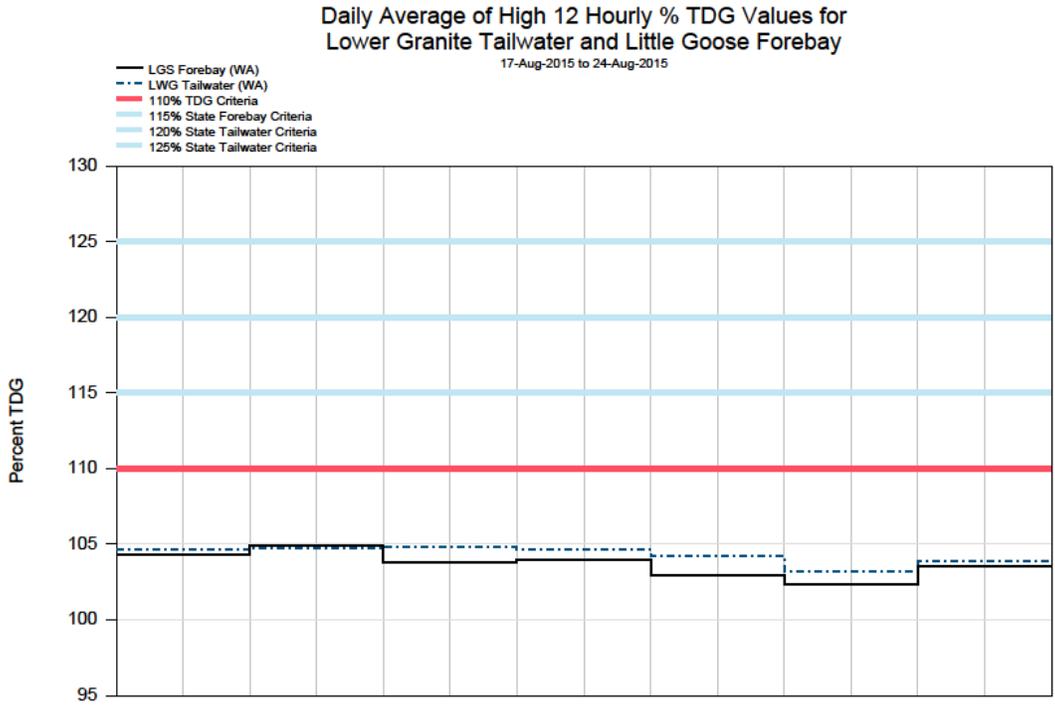


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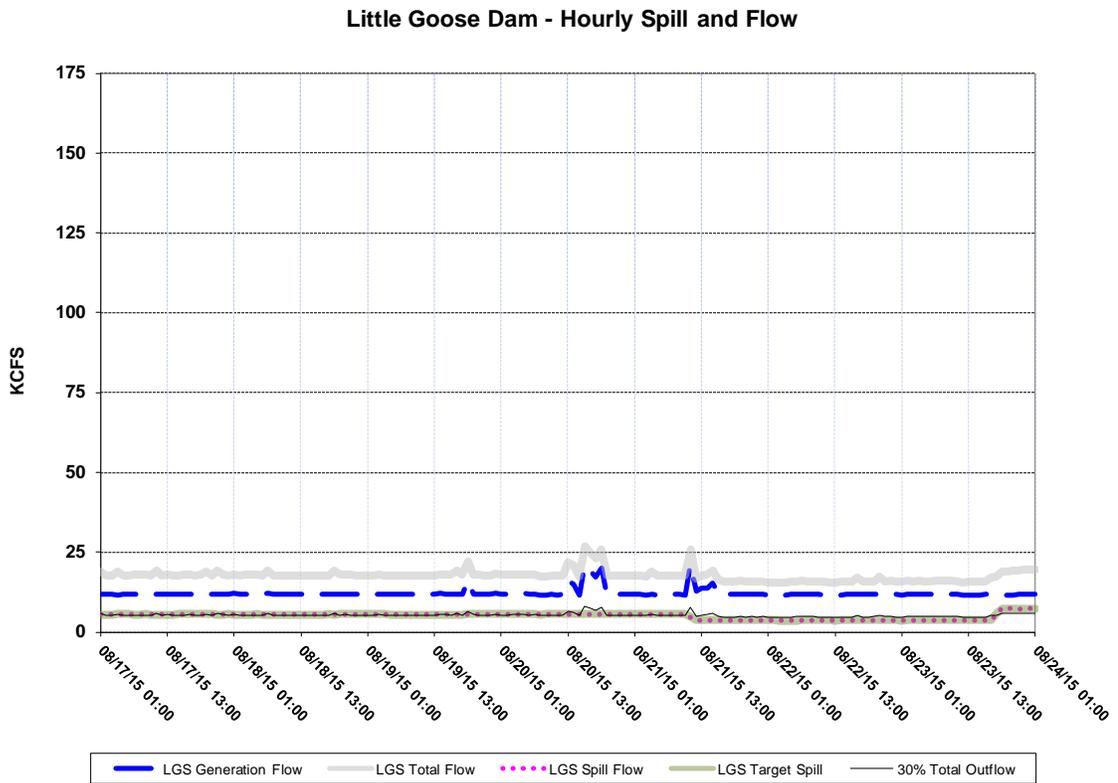
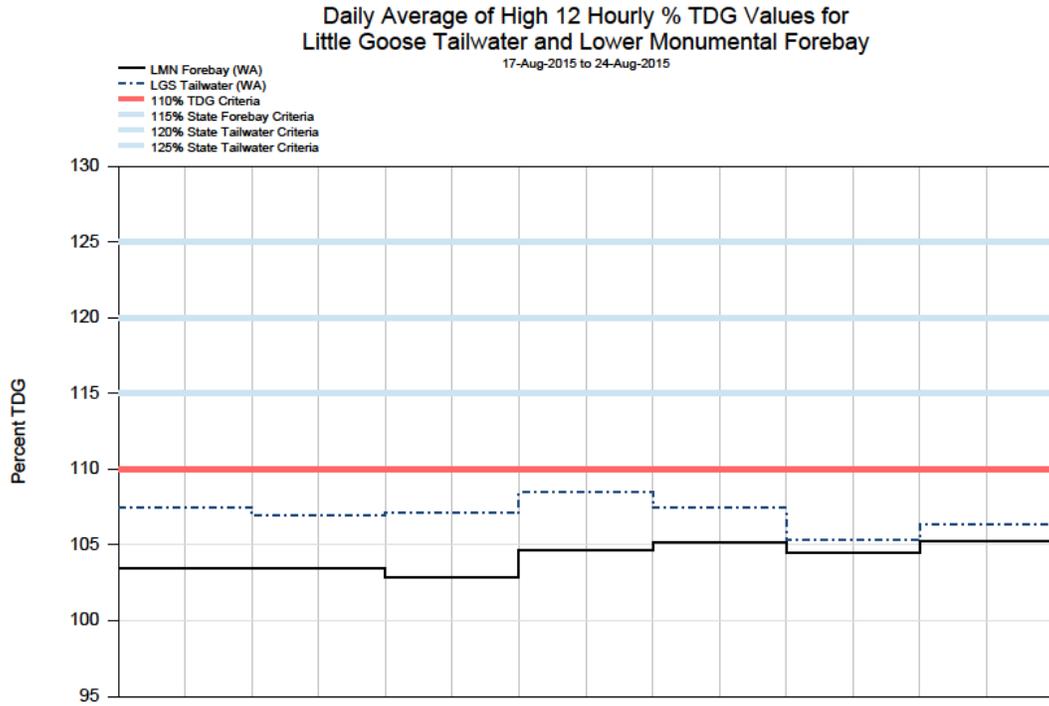


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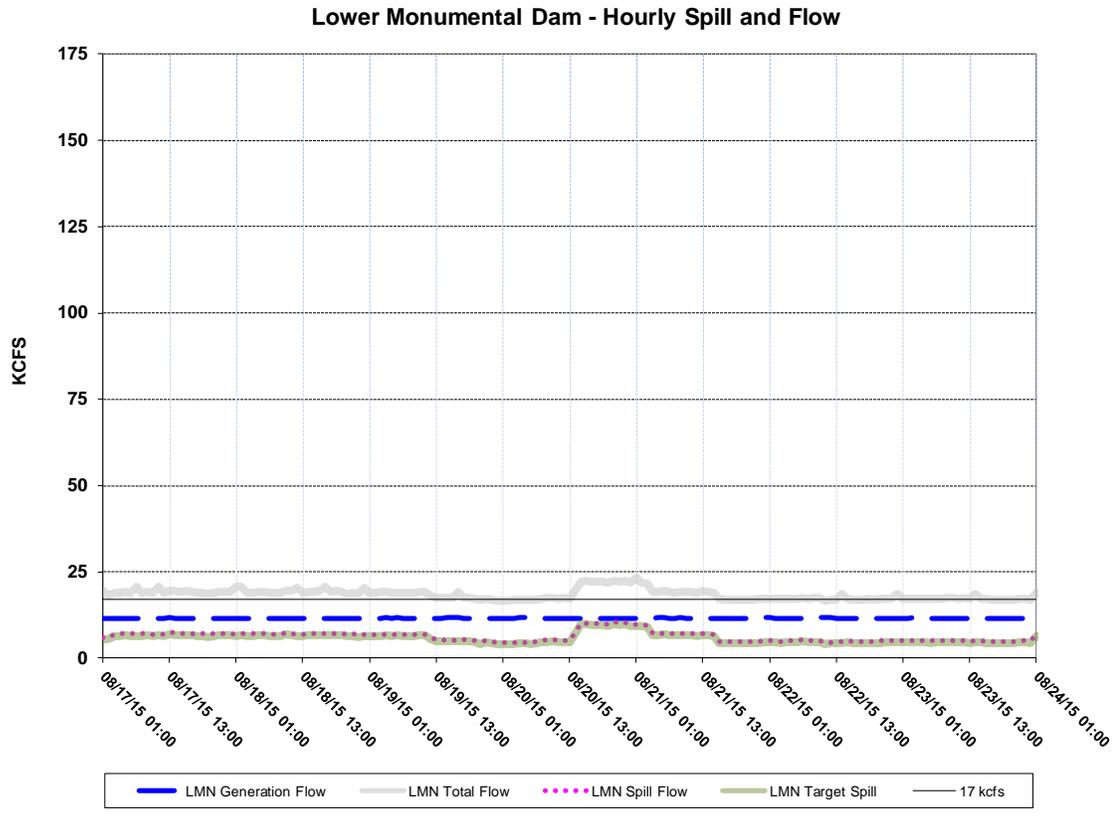
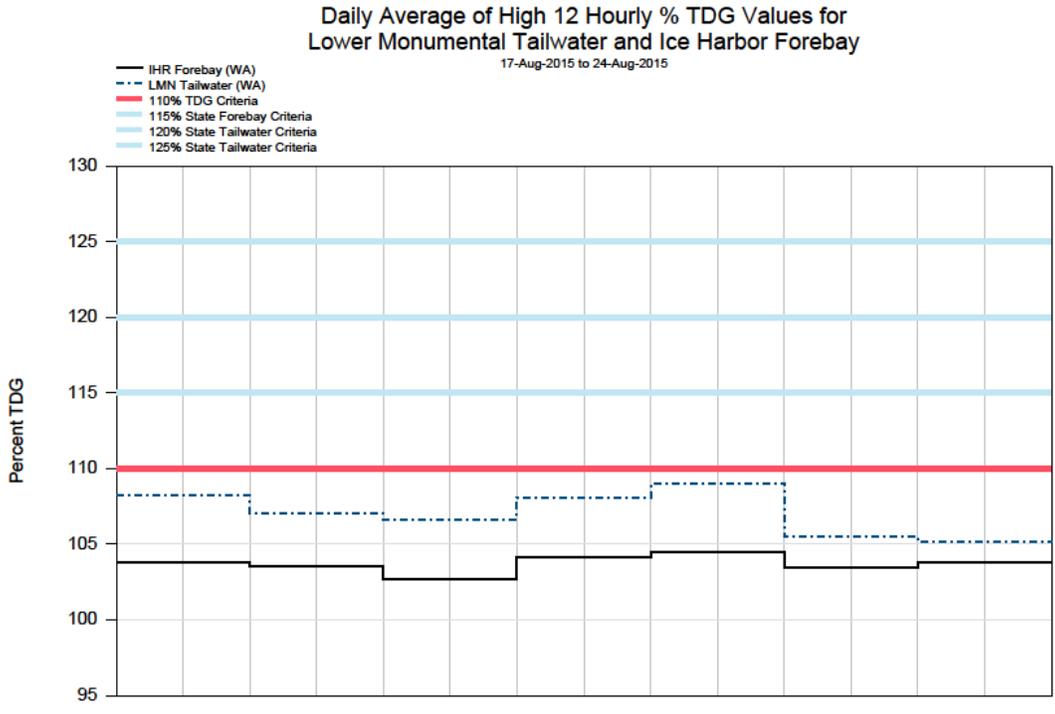


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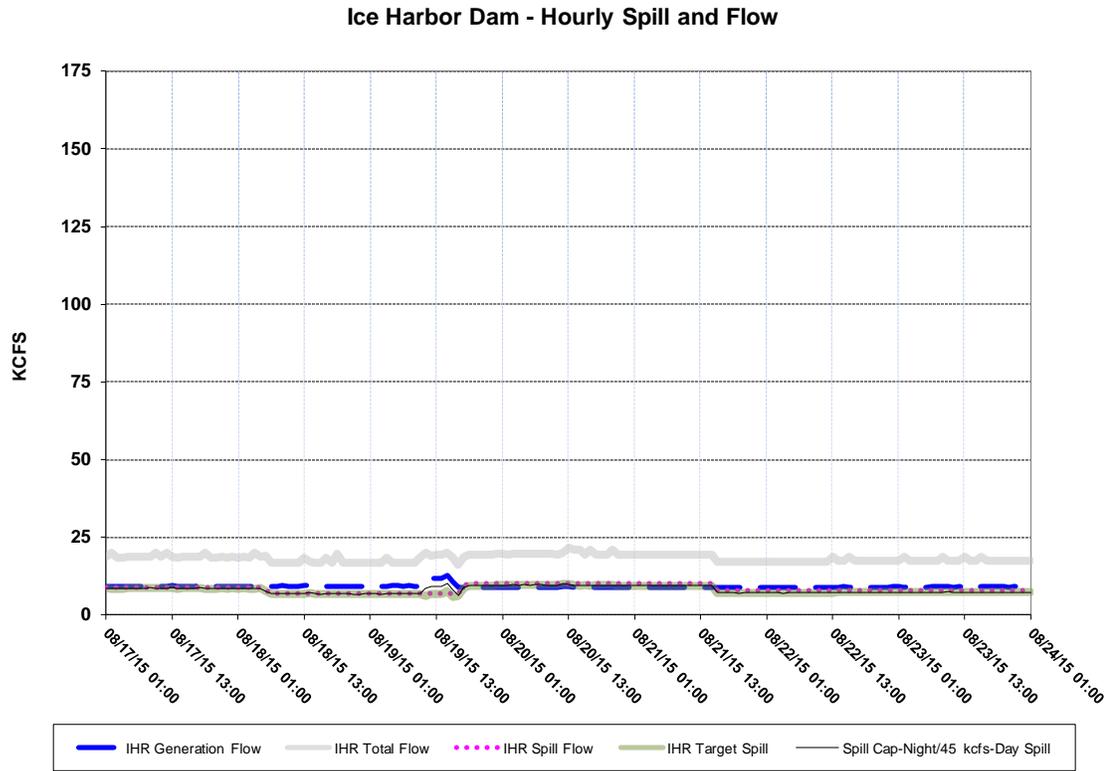
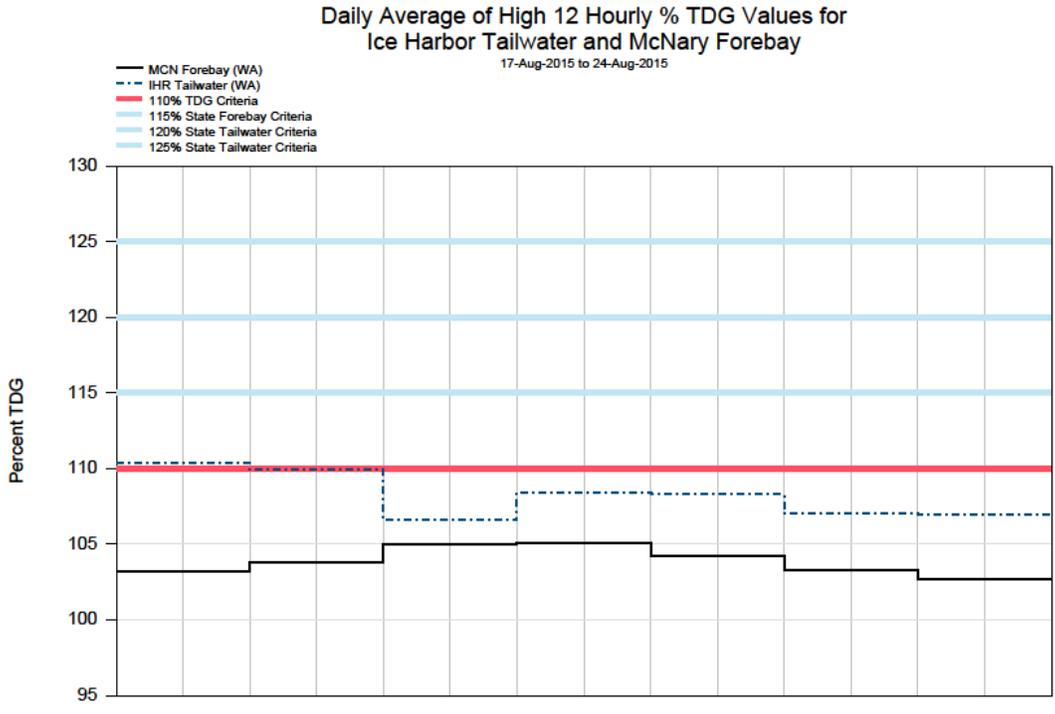


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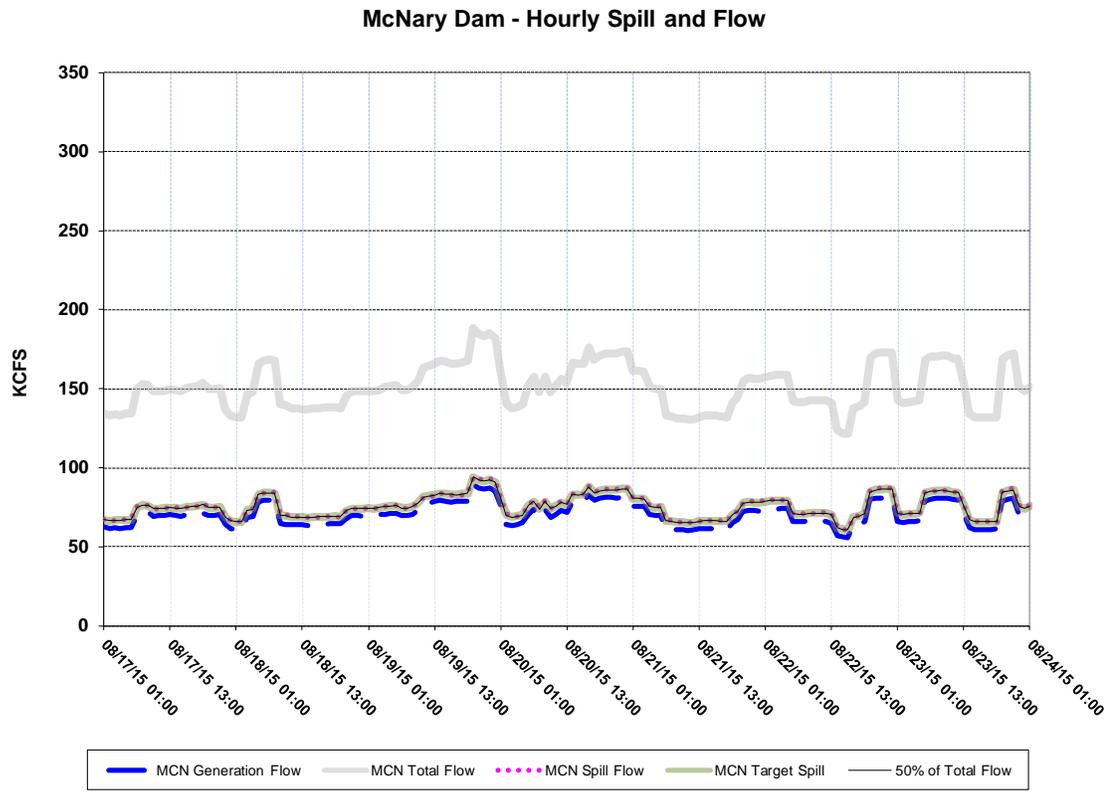
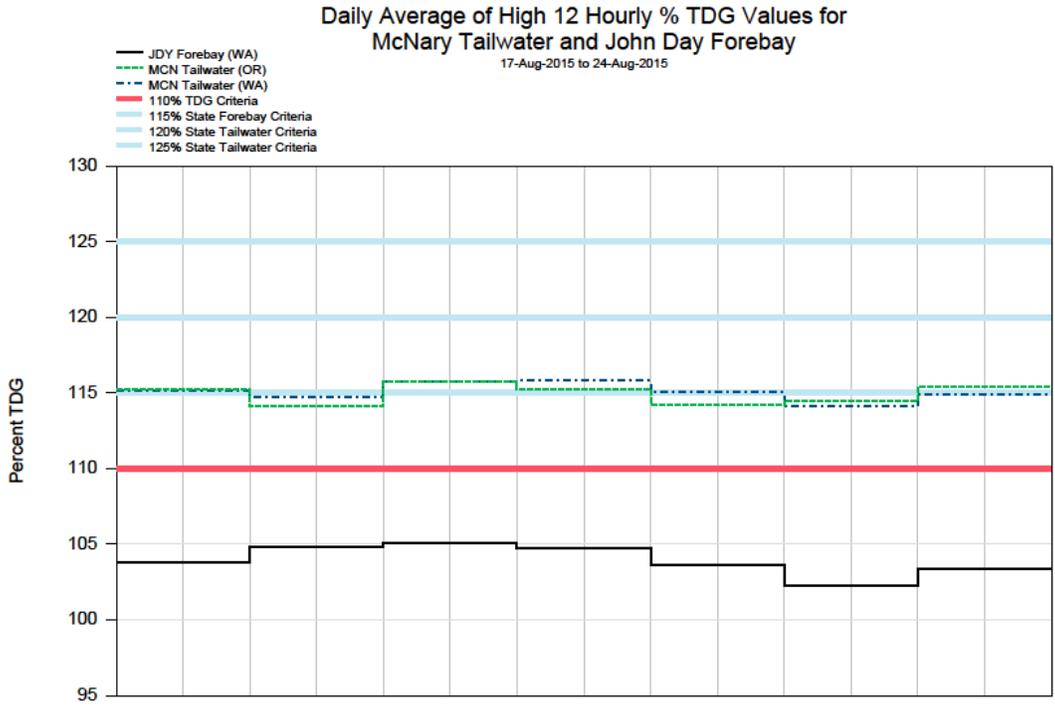


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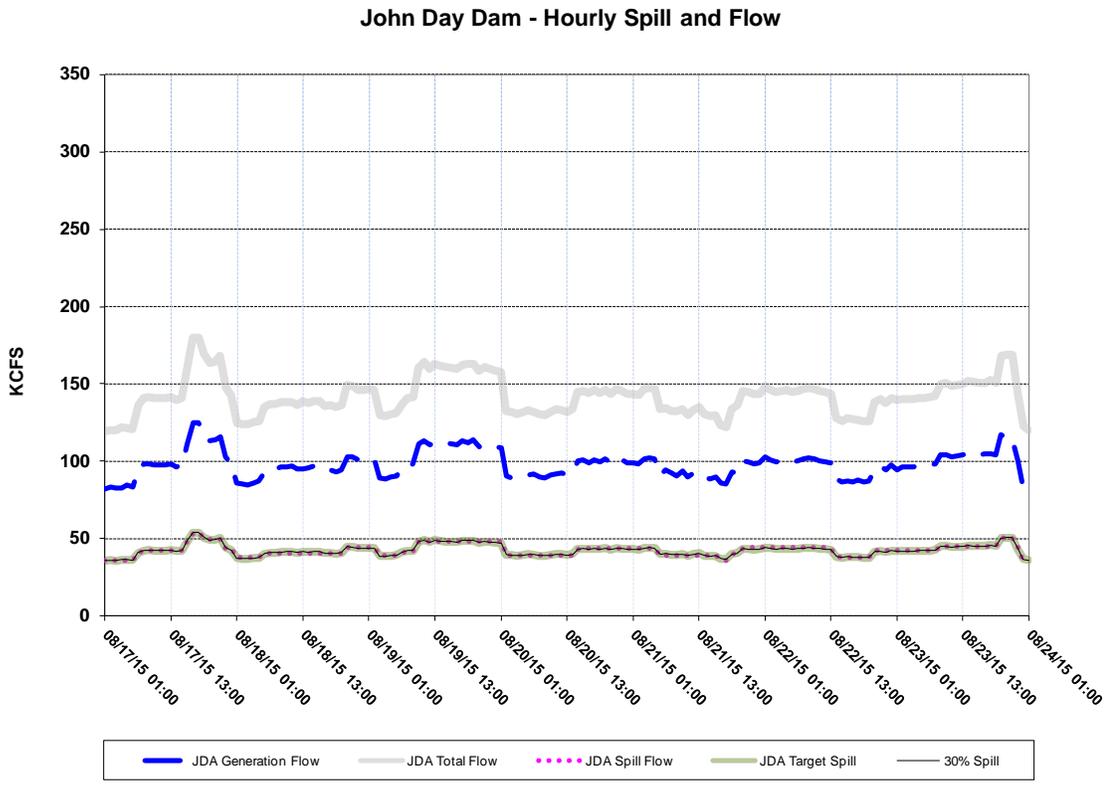
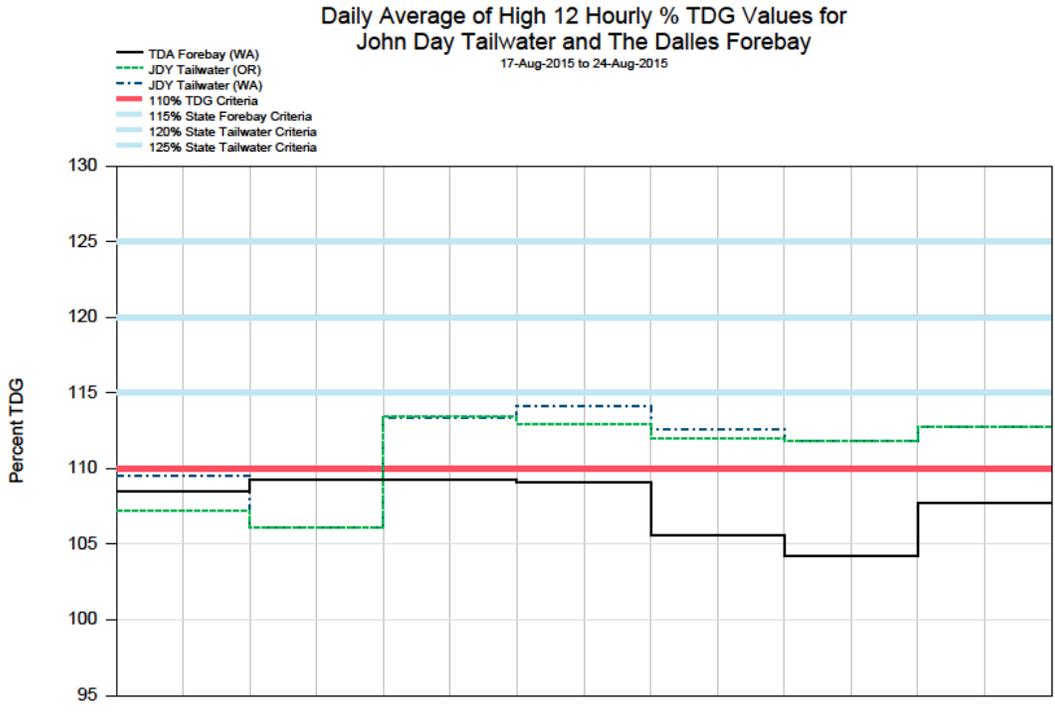


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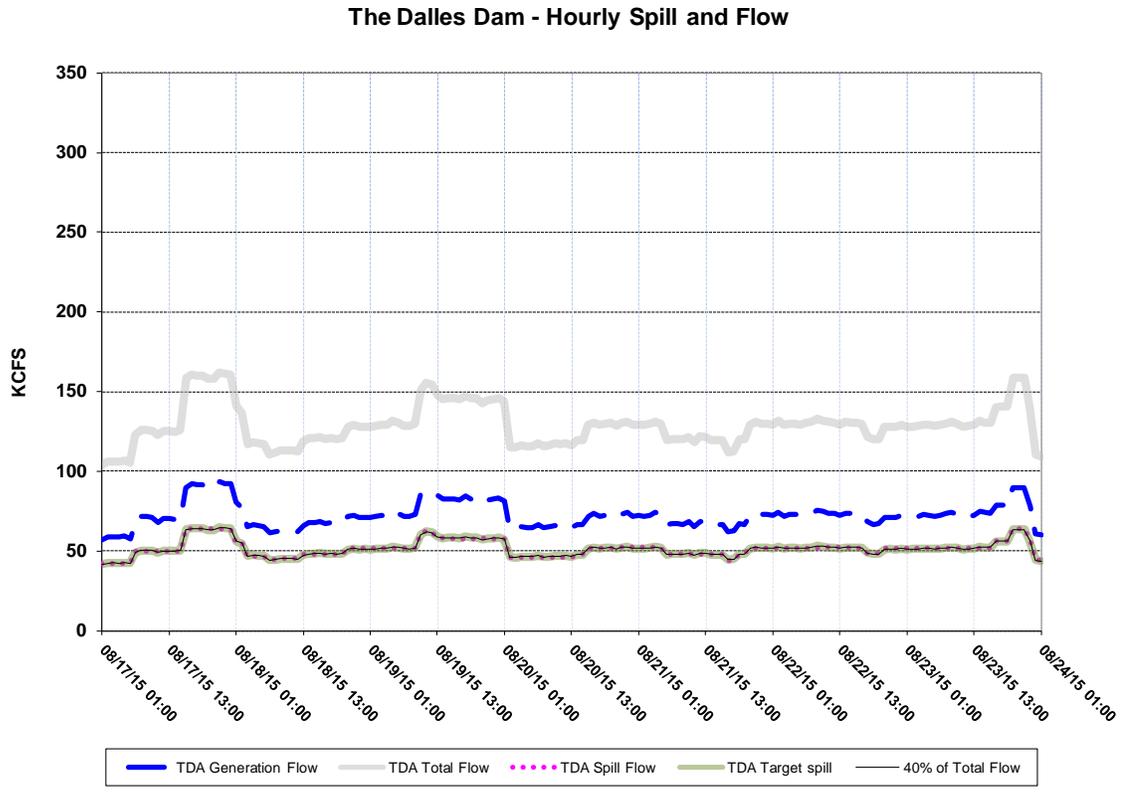
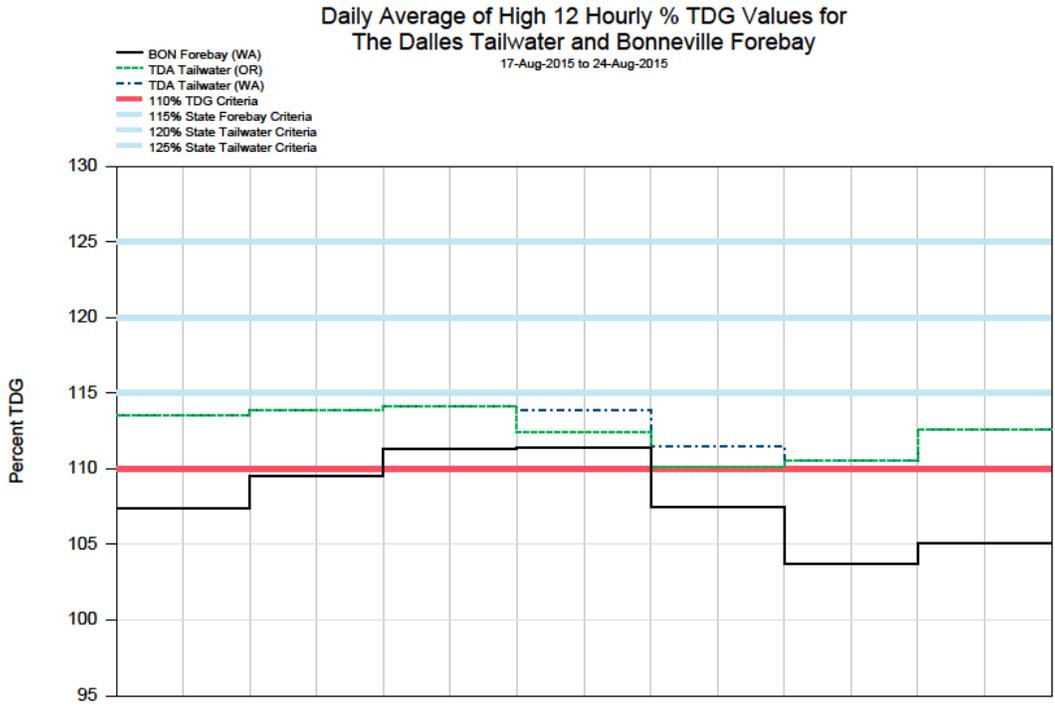


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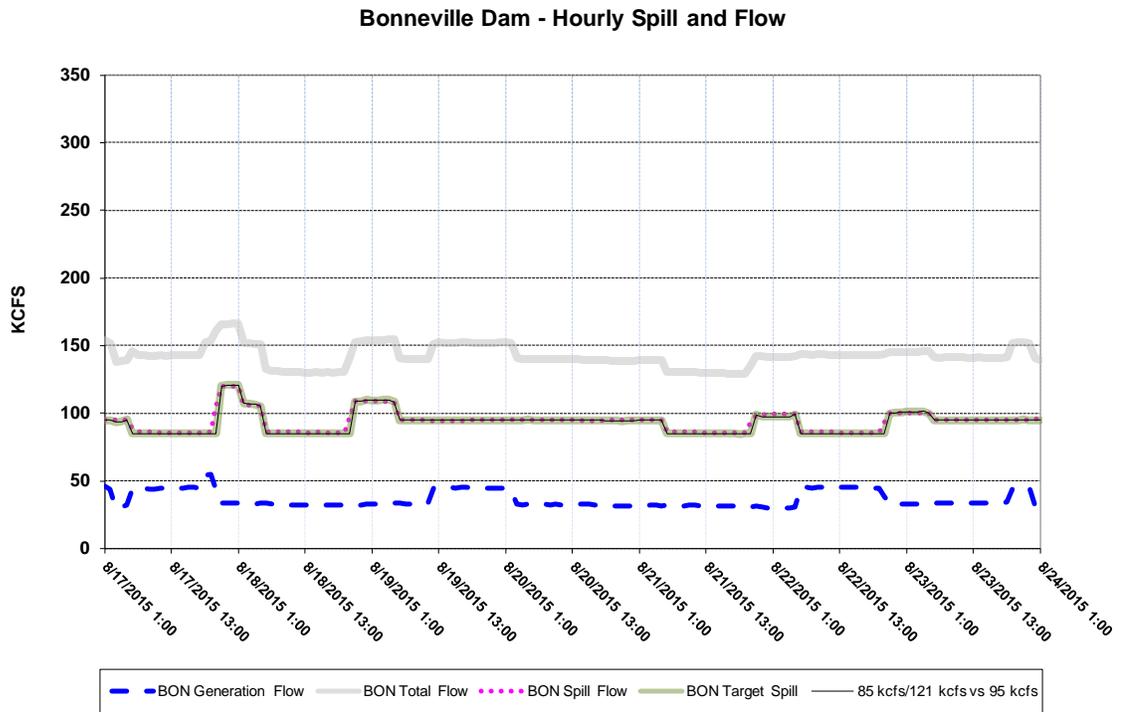
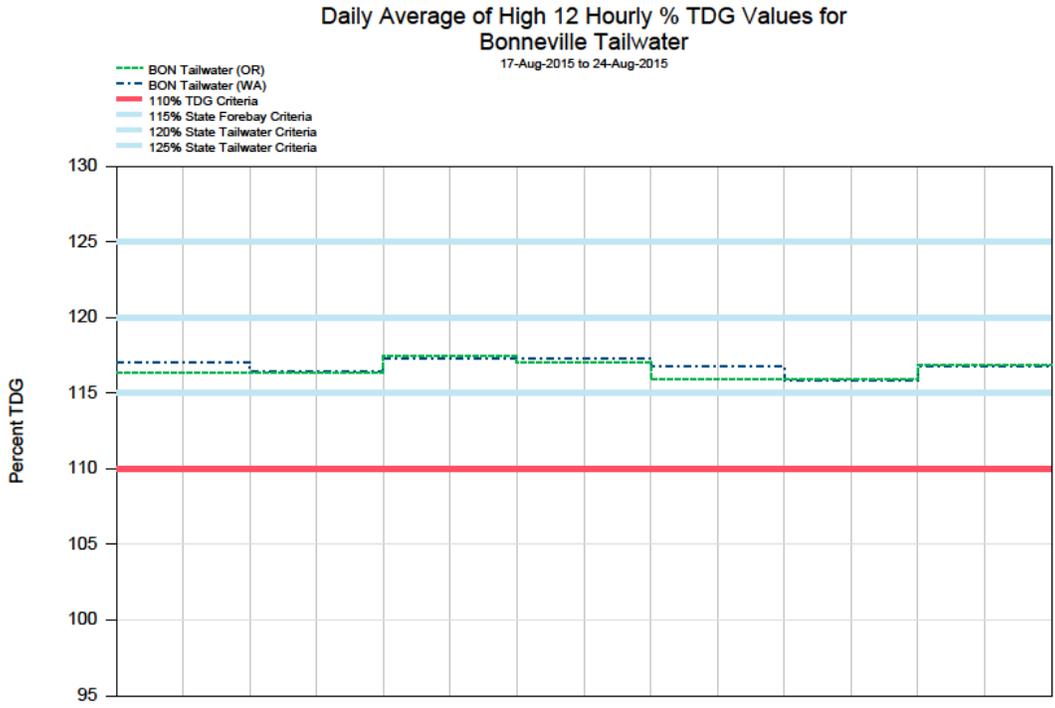


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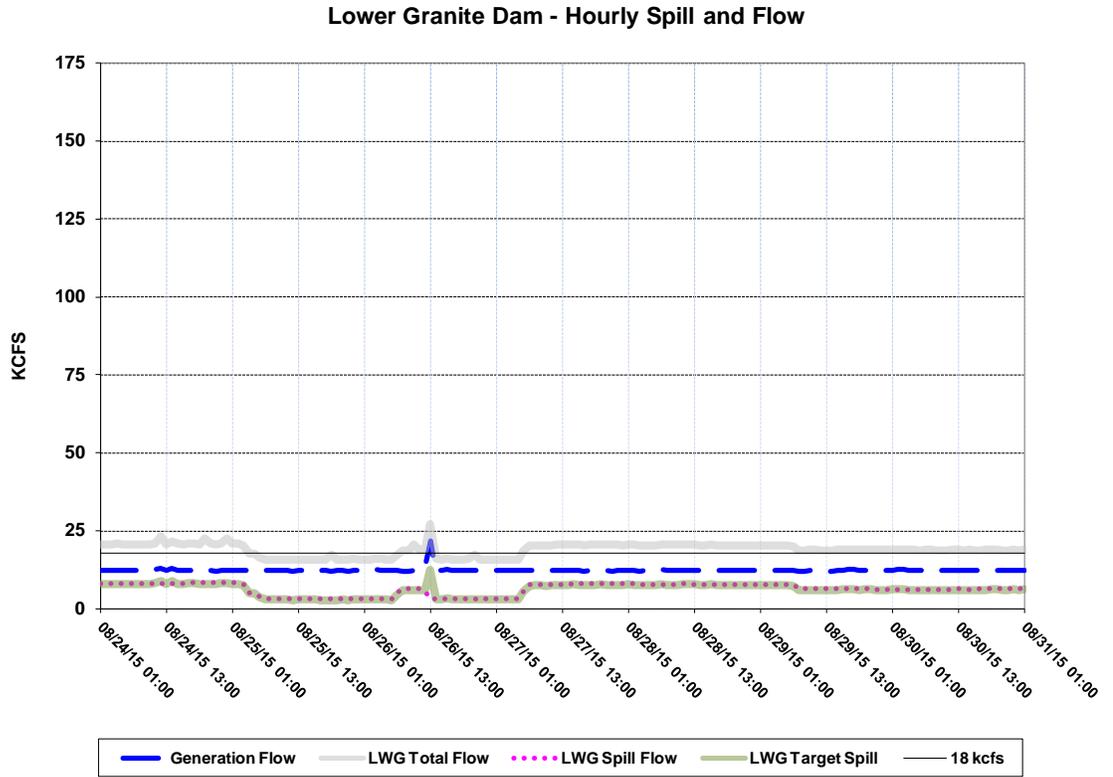
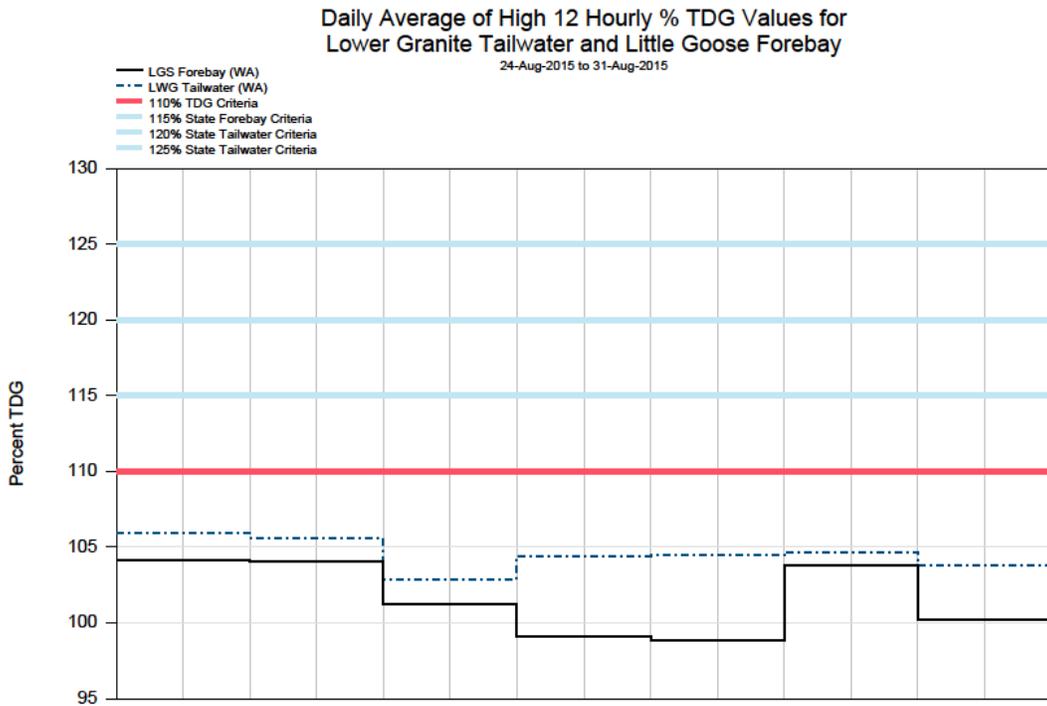


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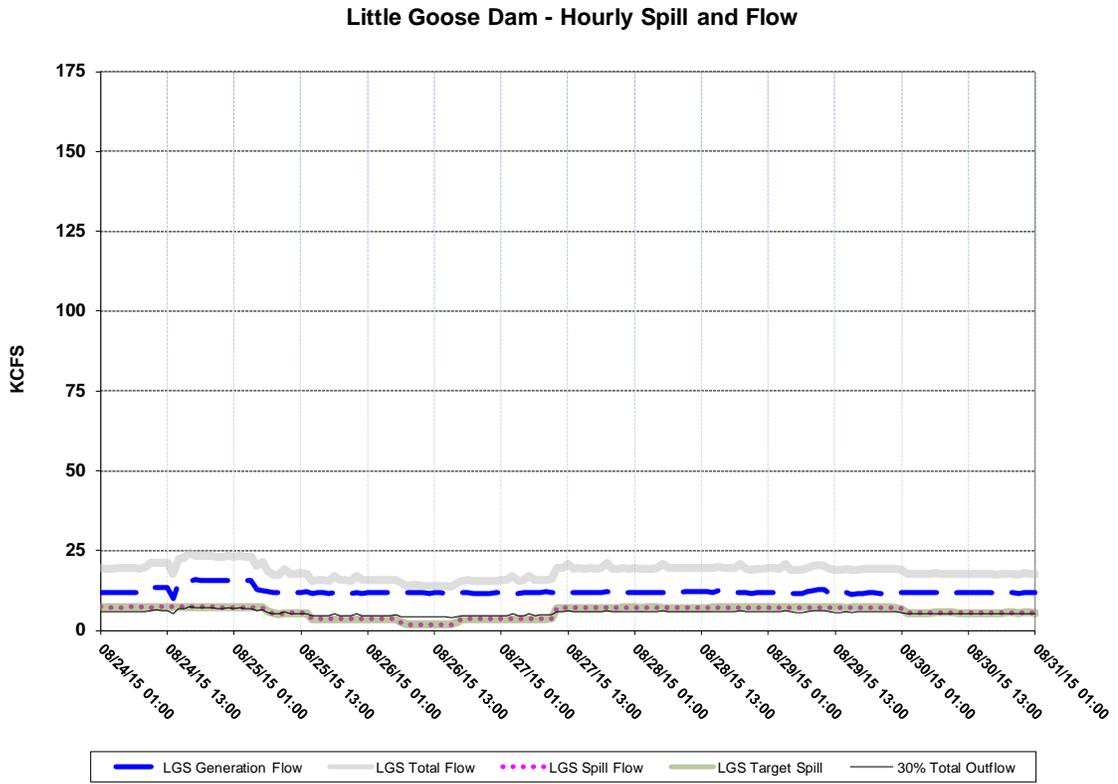
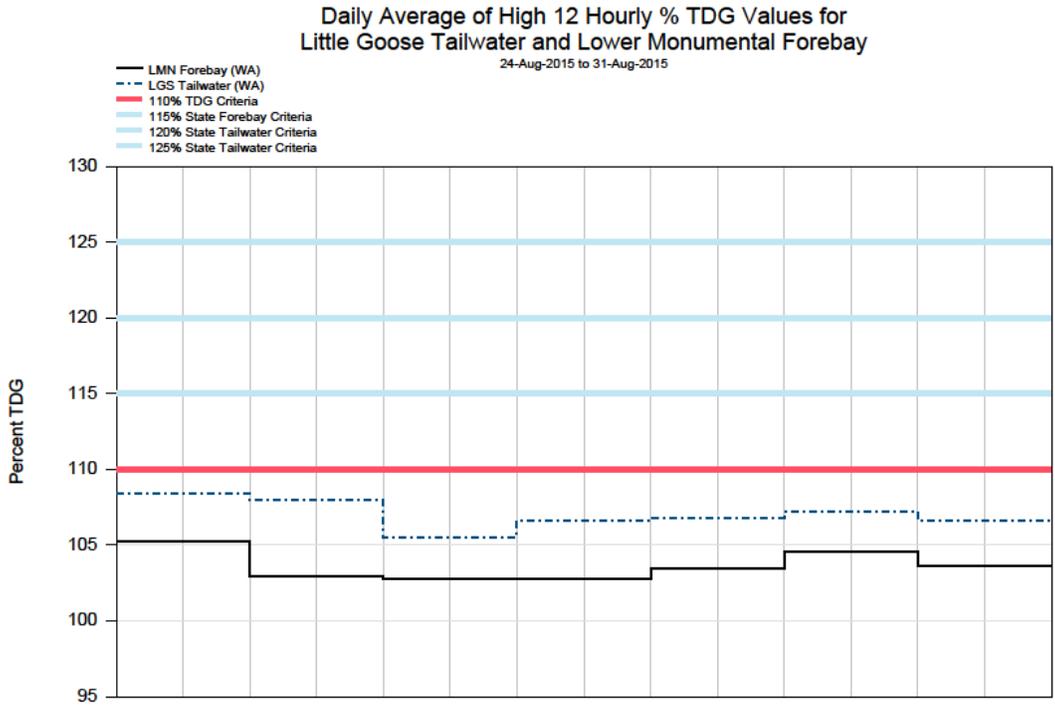


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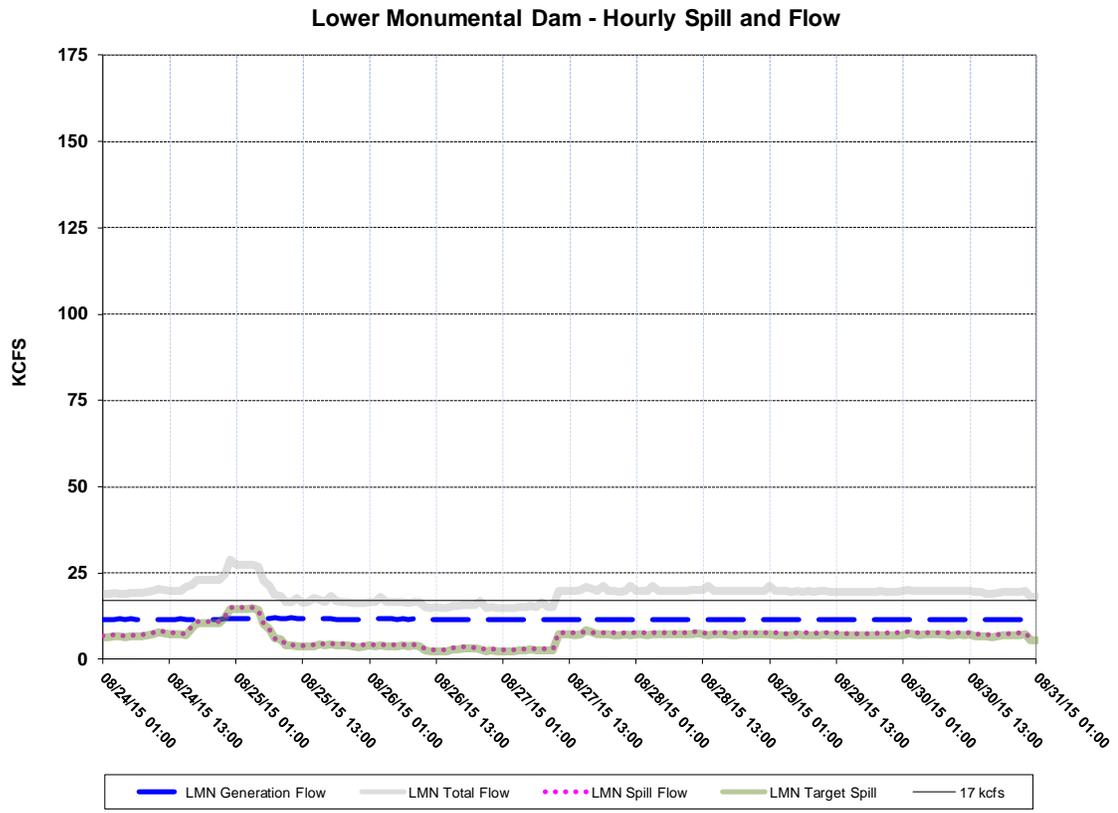
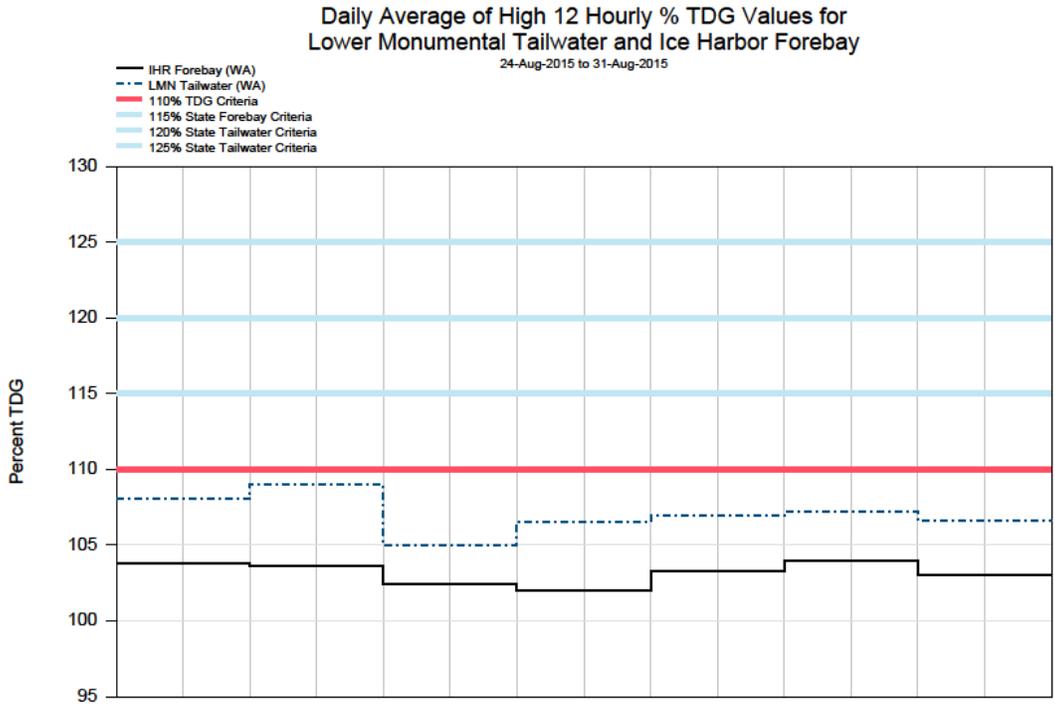


Figure 28

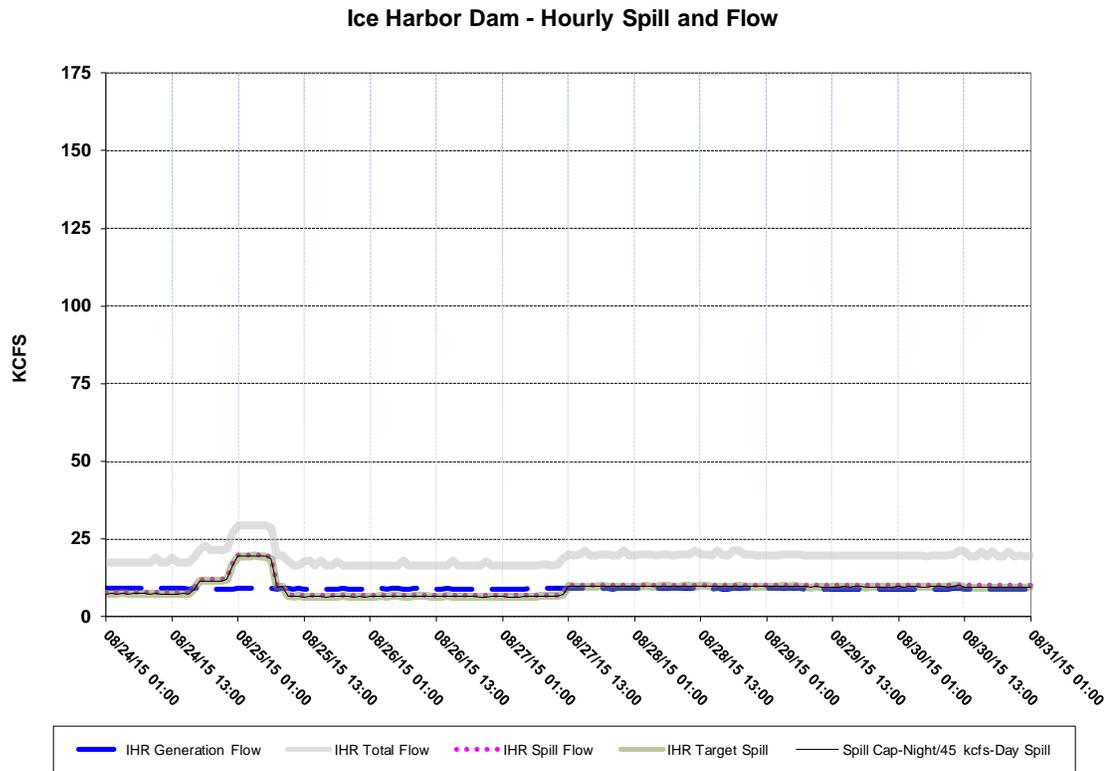
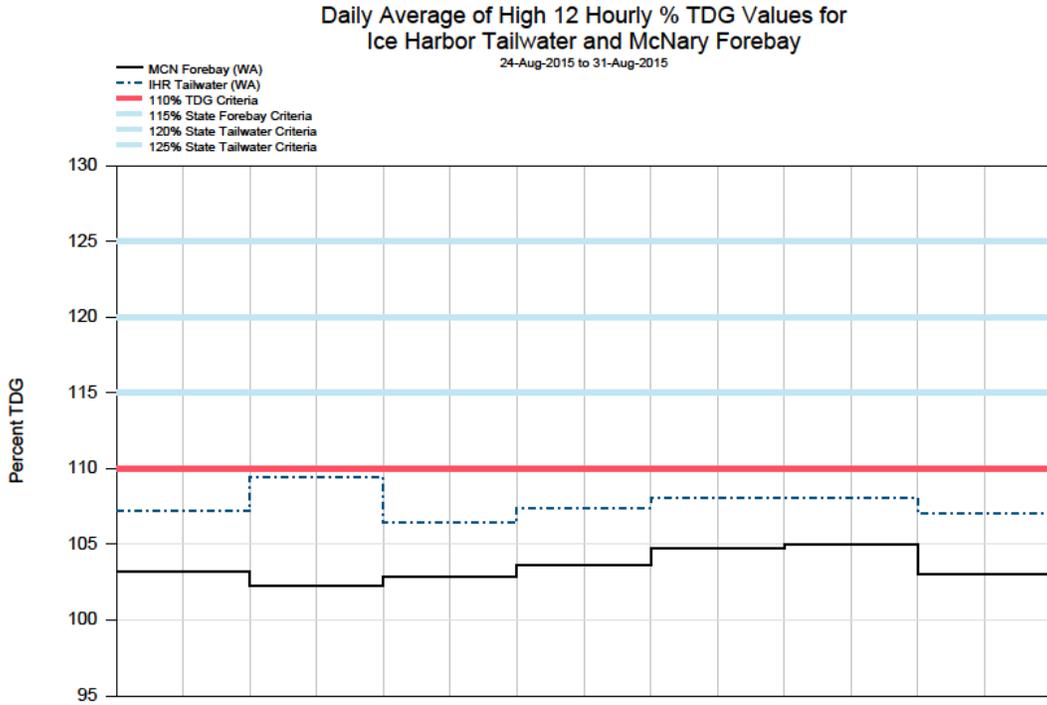


Figure 29

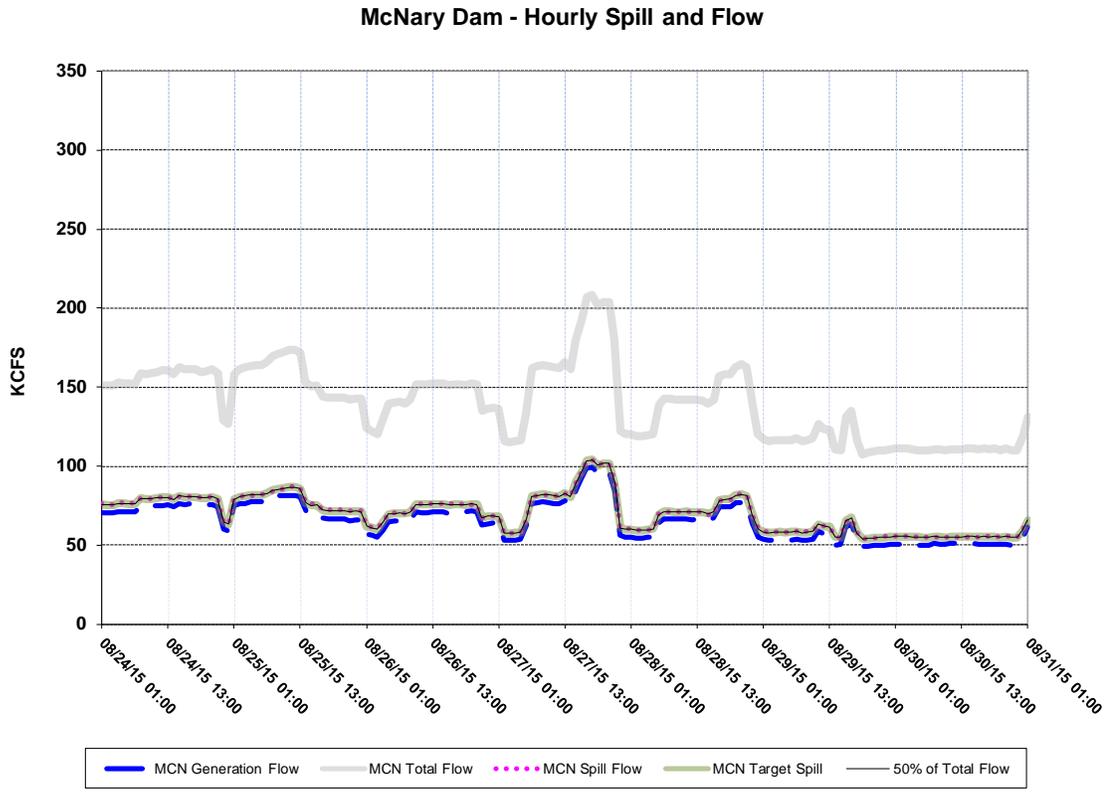
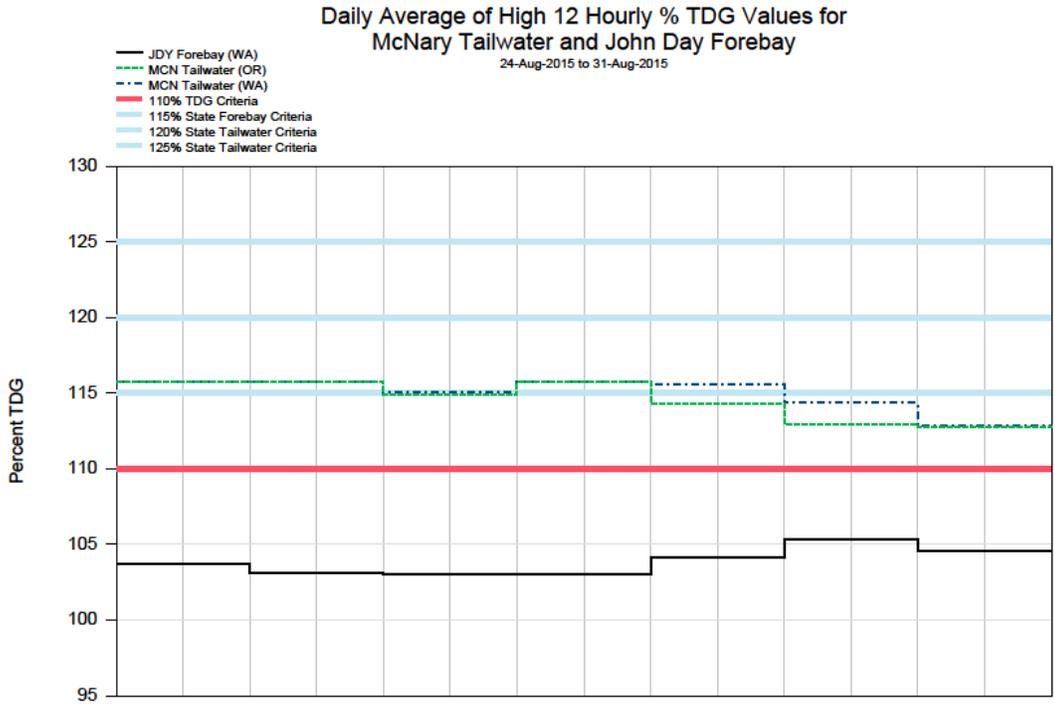
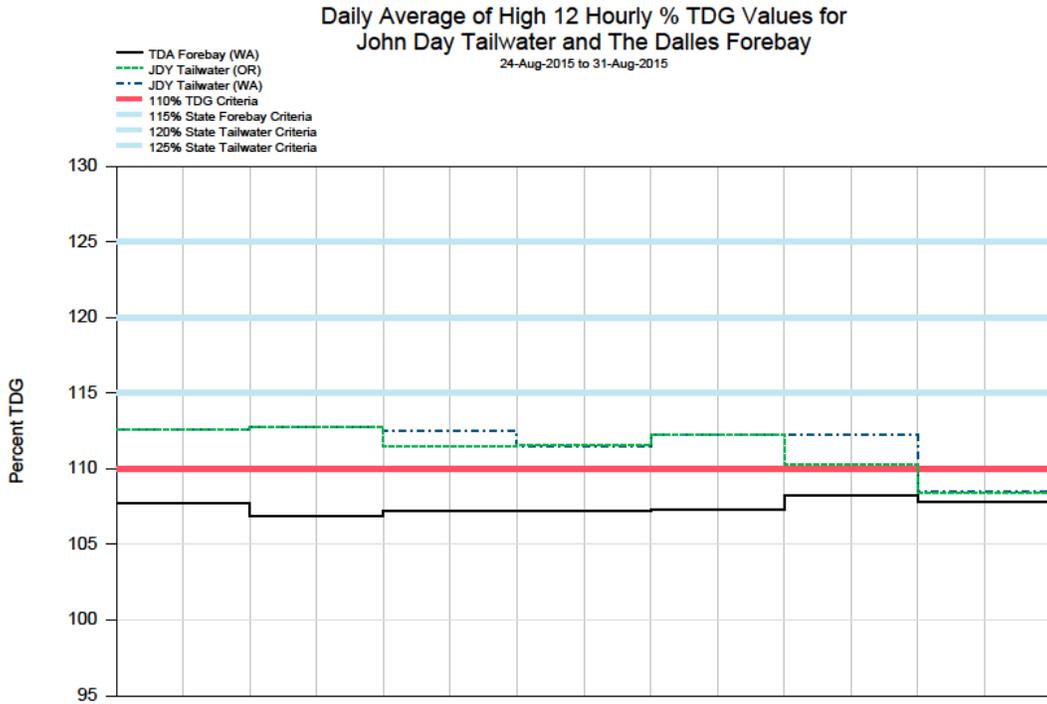


Figure 30



John Day Dam - Hourly Spill and Flow

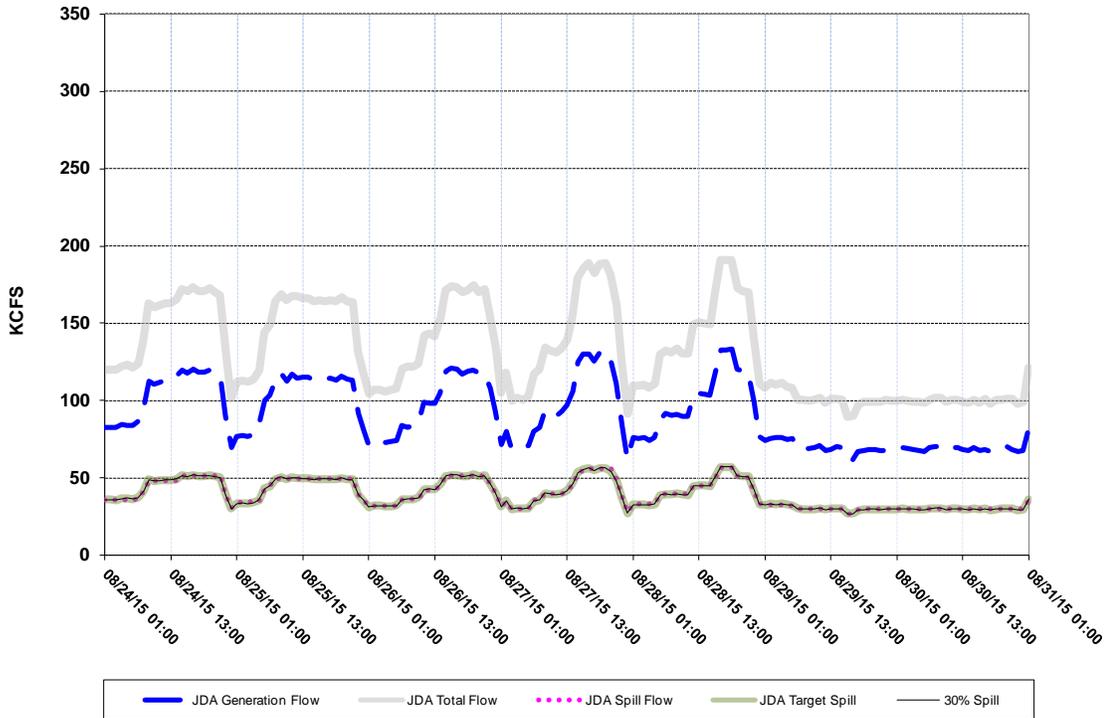


Figure 31

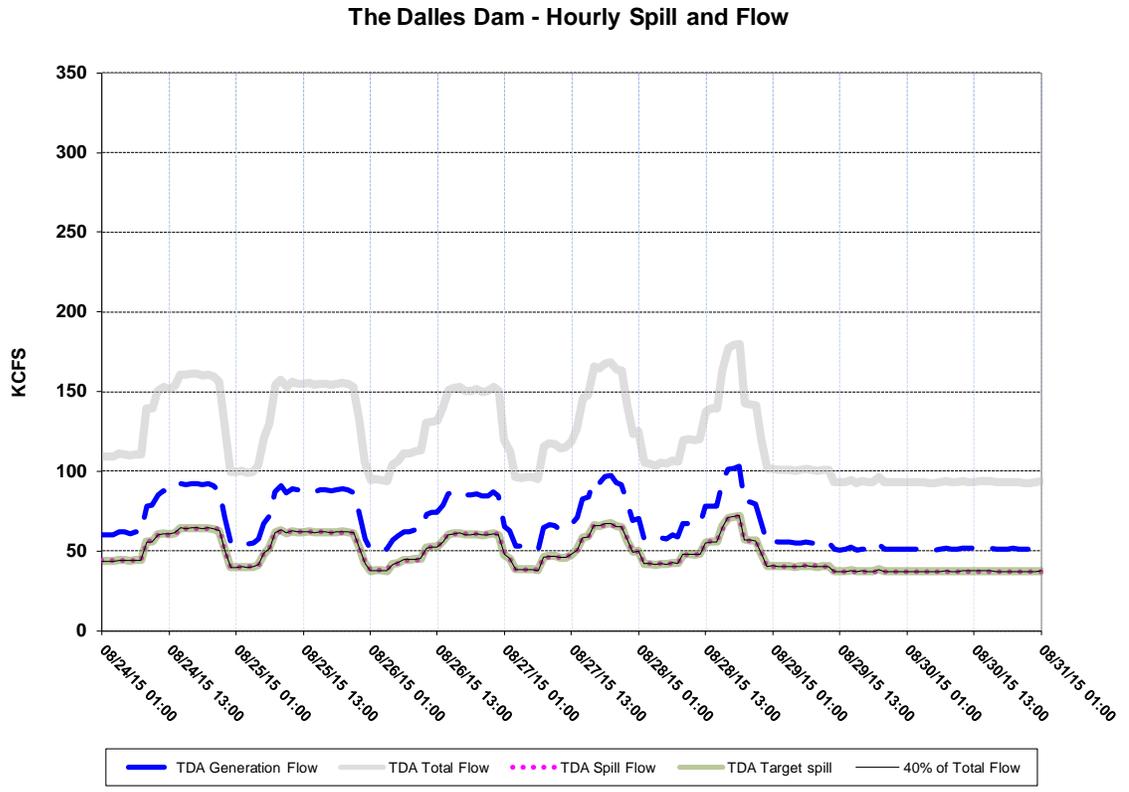
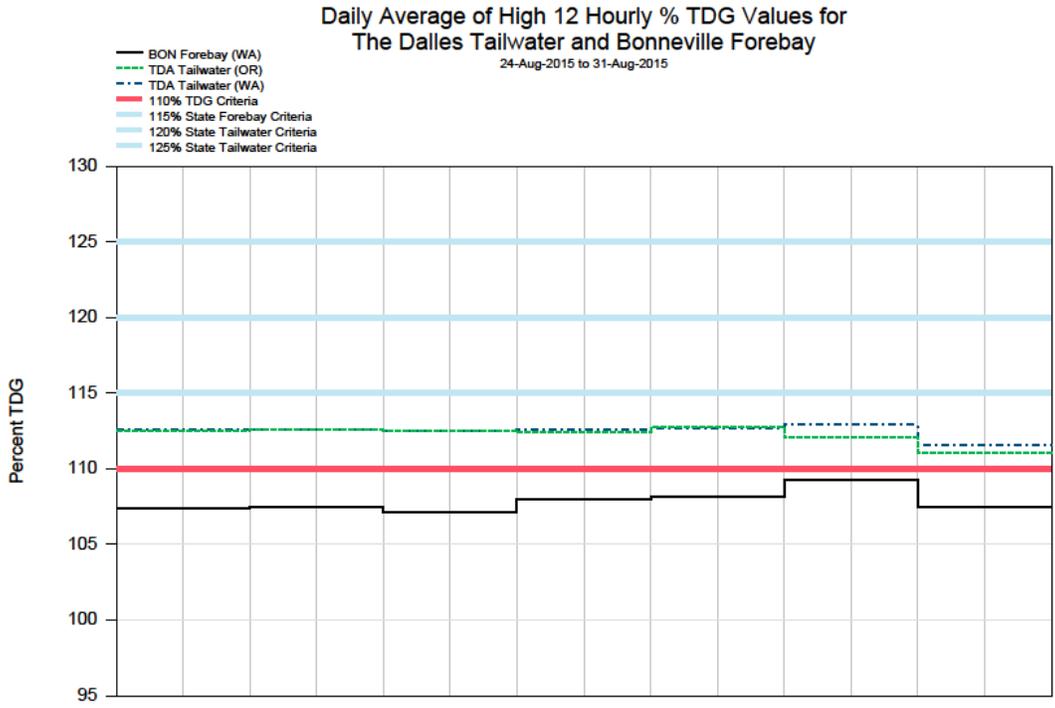


Figure 32

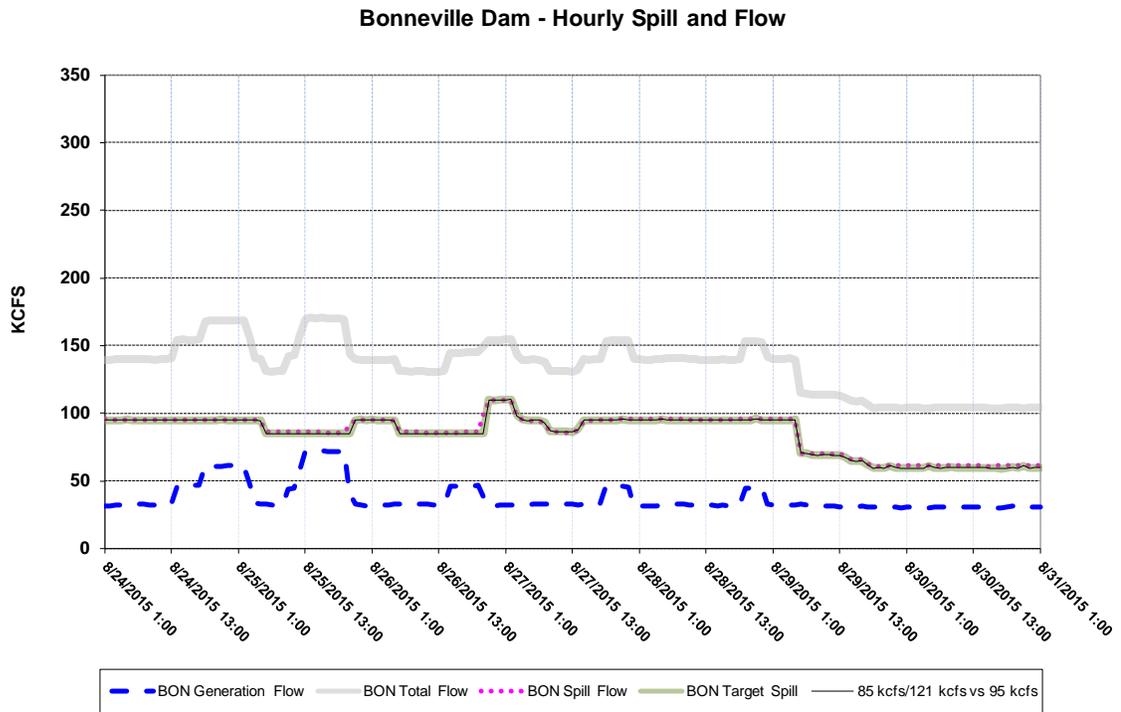
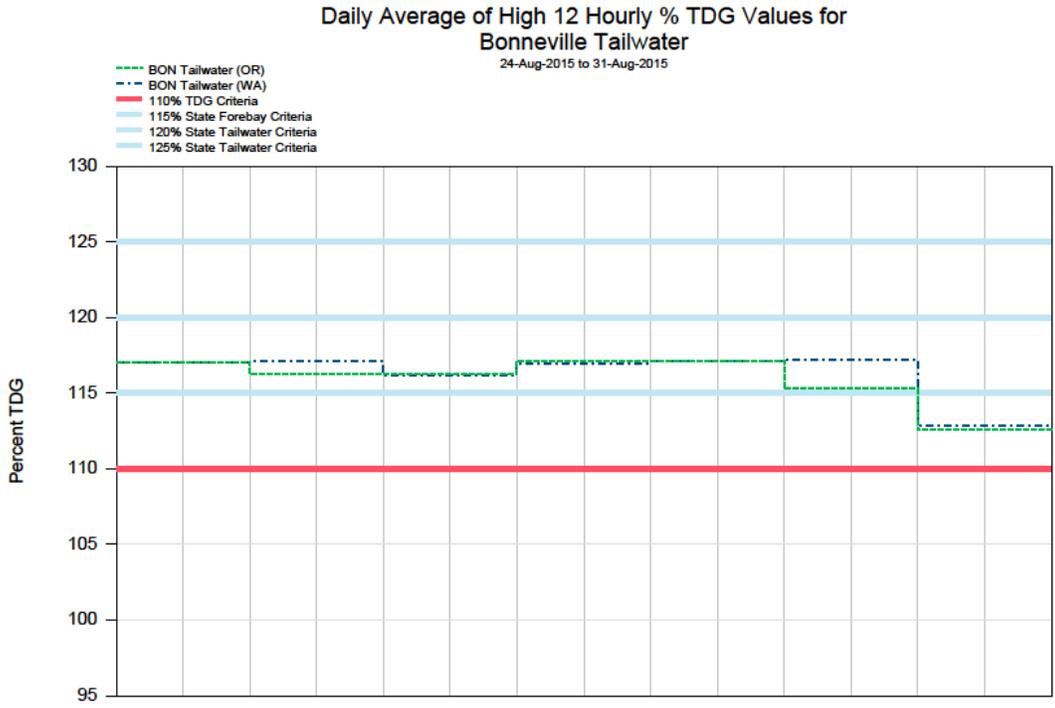


Figure 33

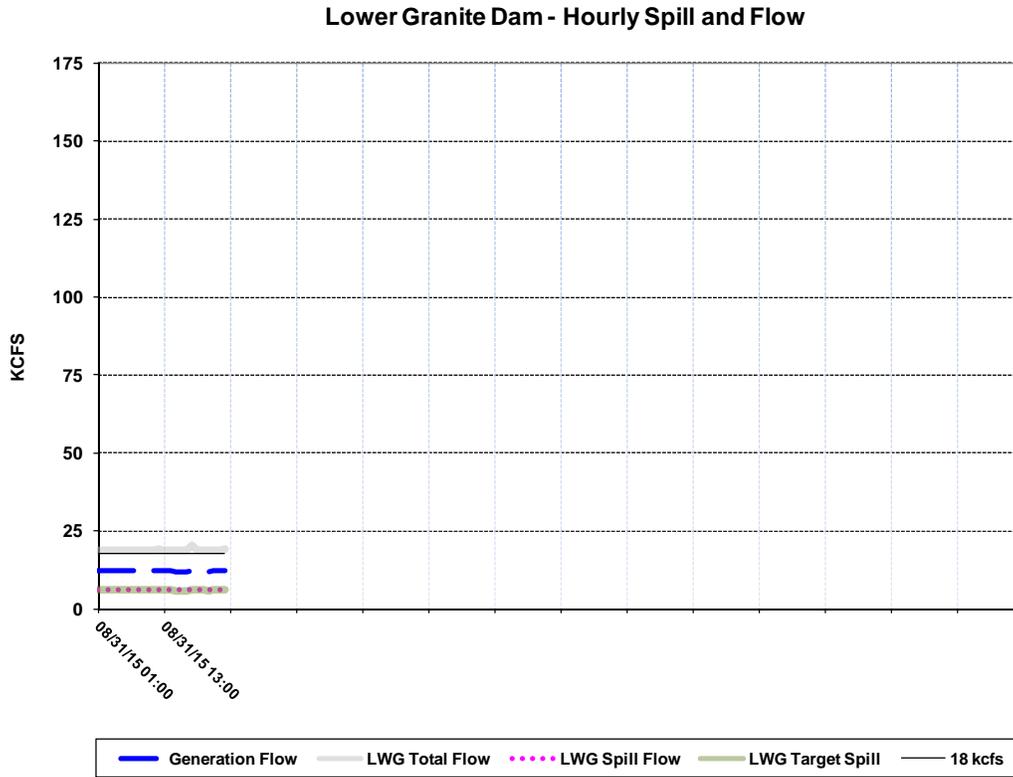
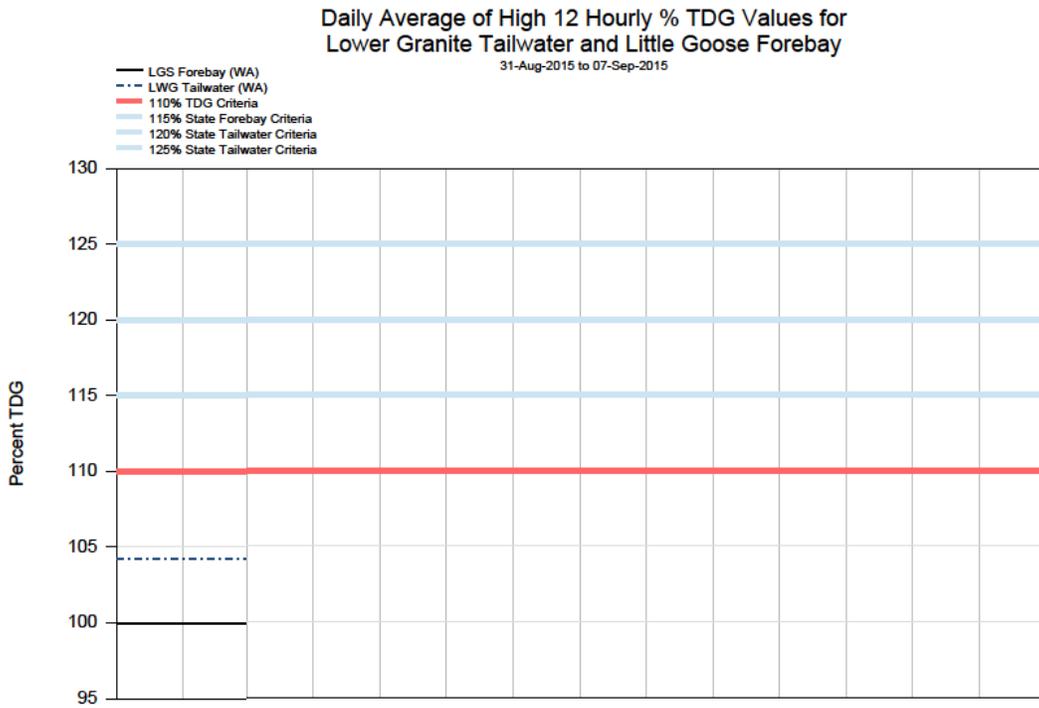


Figure 34

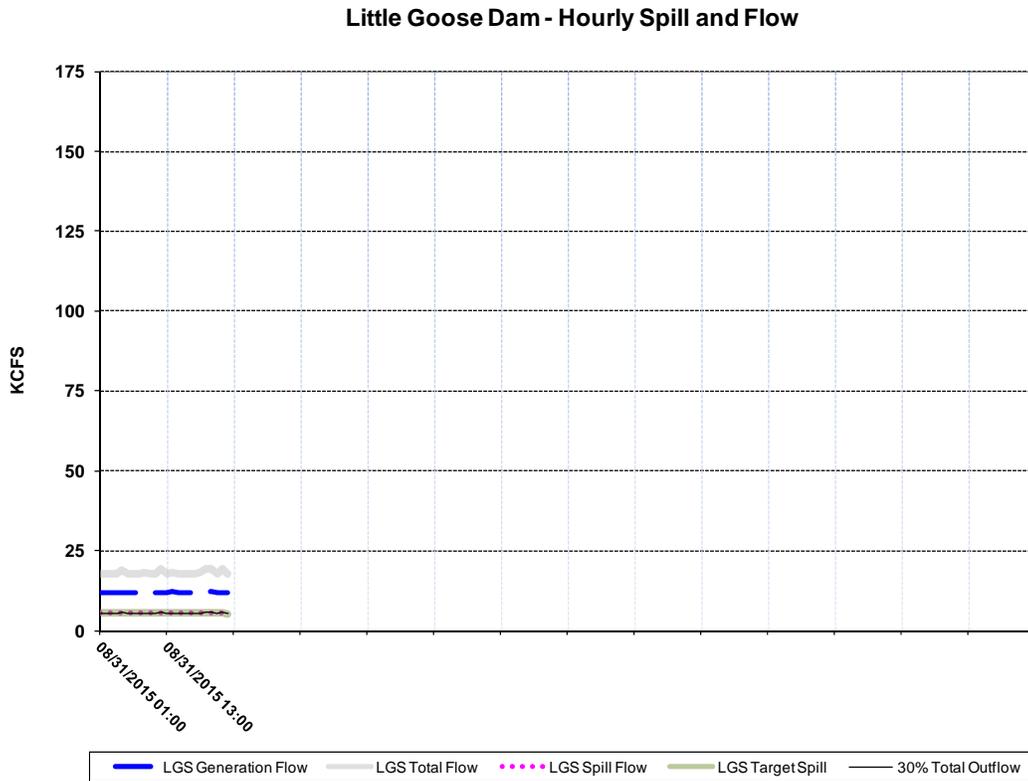
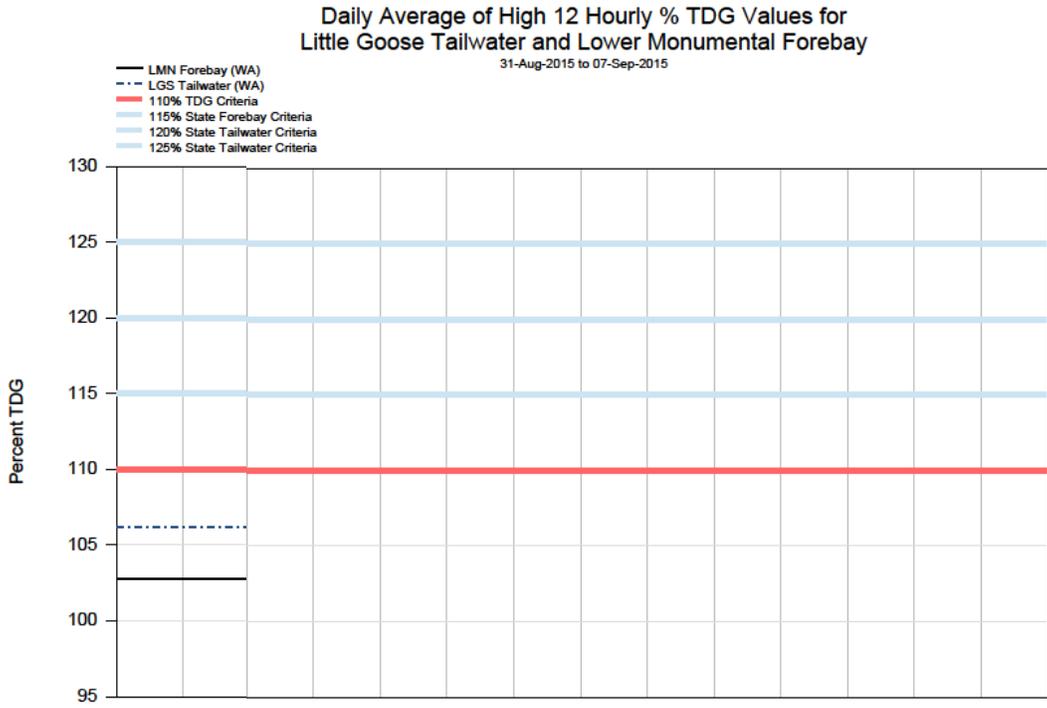


Figure 35

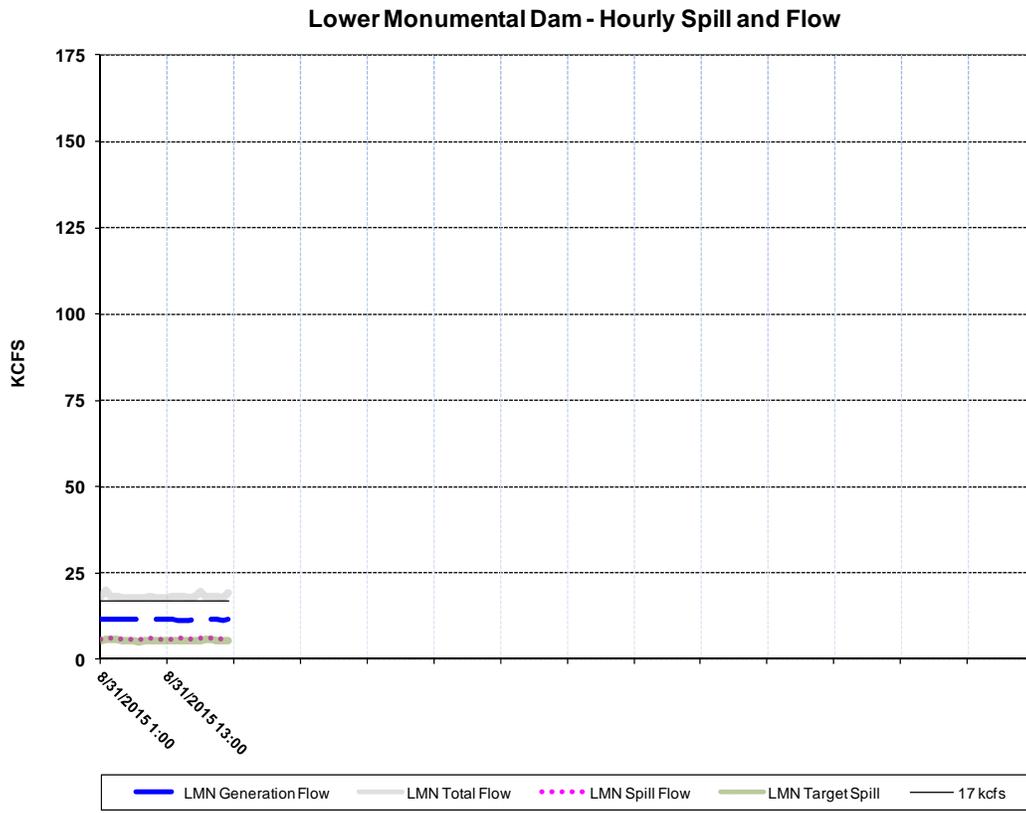
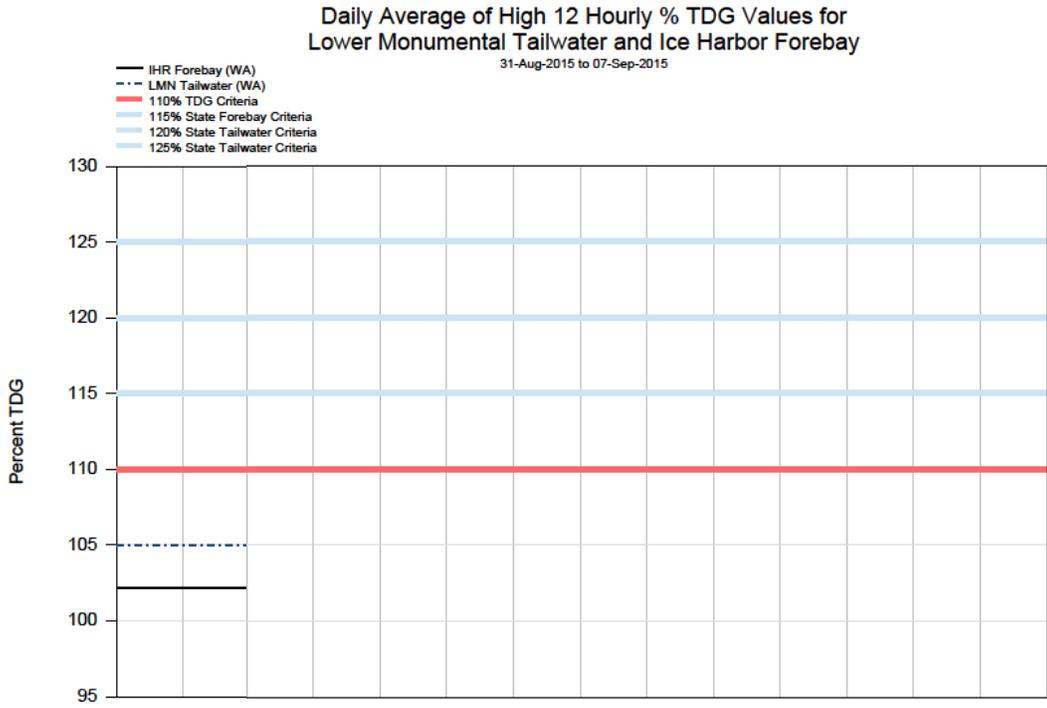


Figure 36

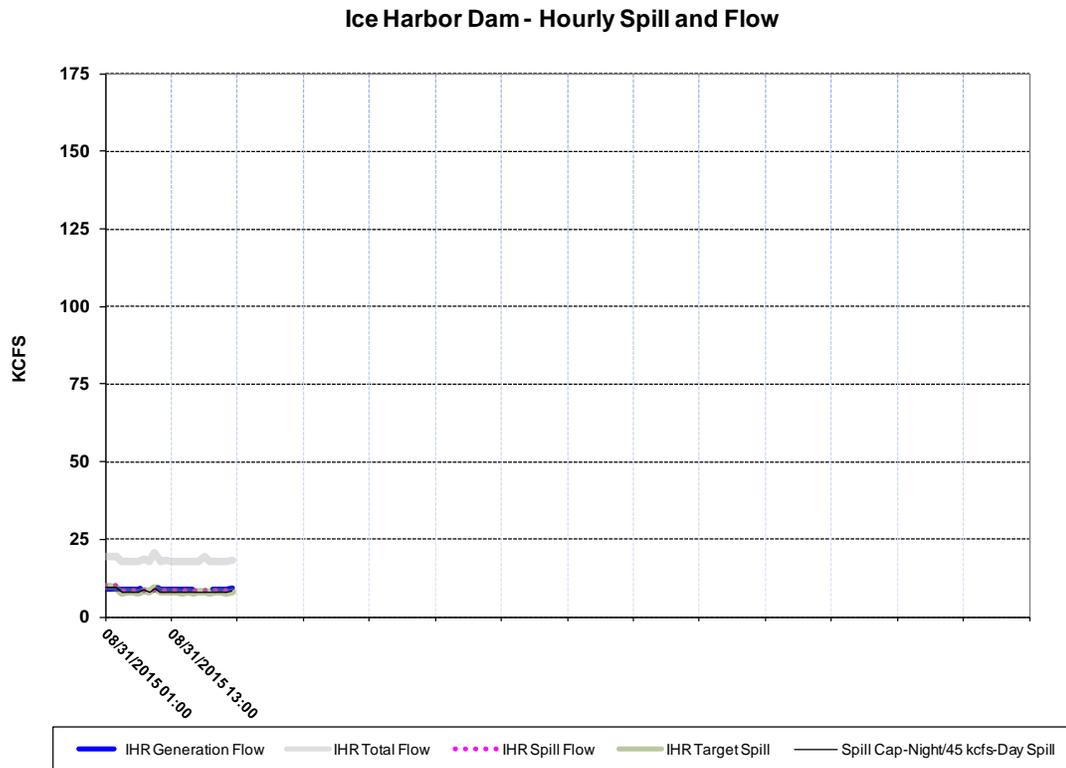
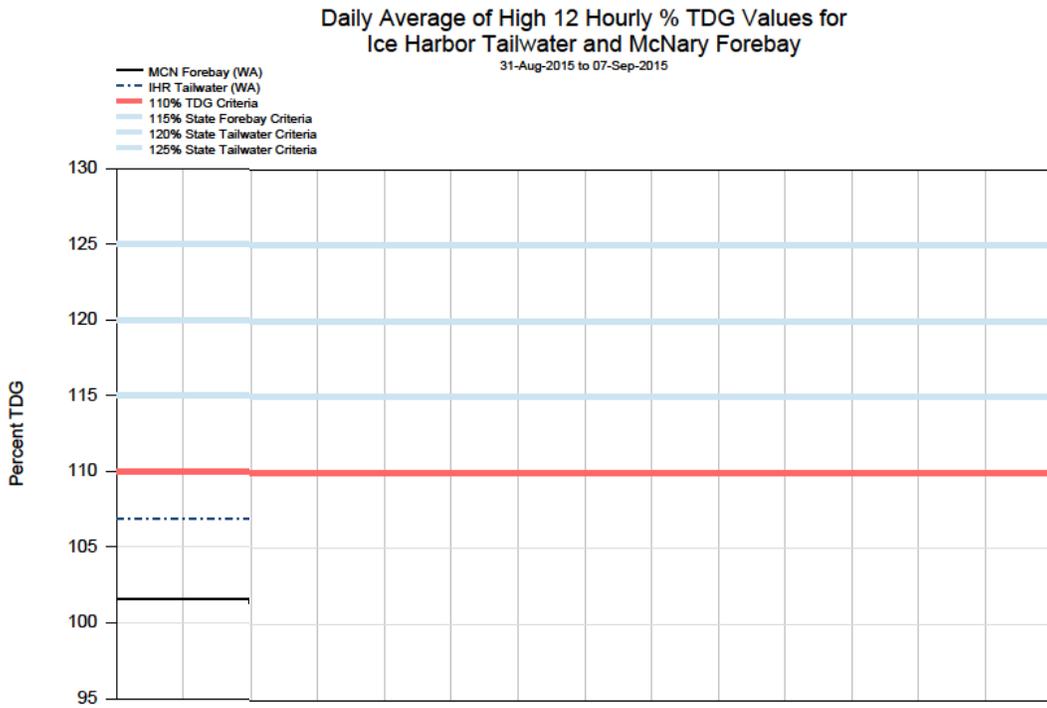


Figure 37

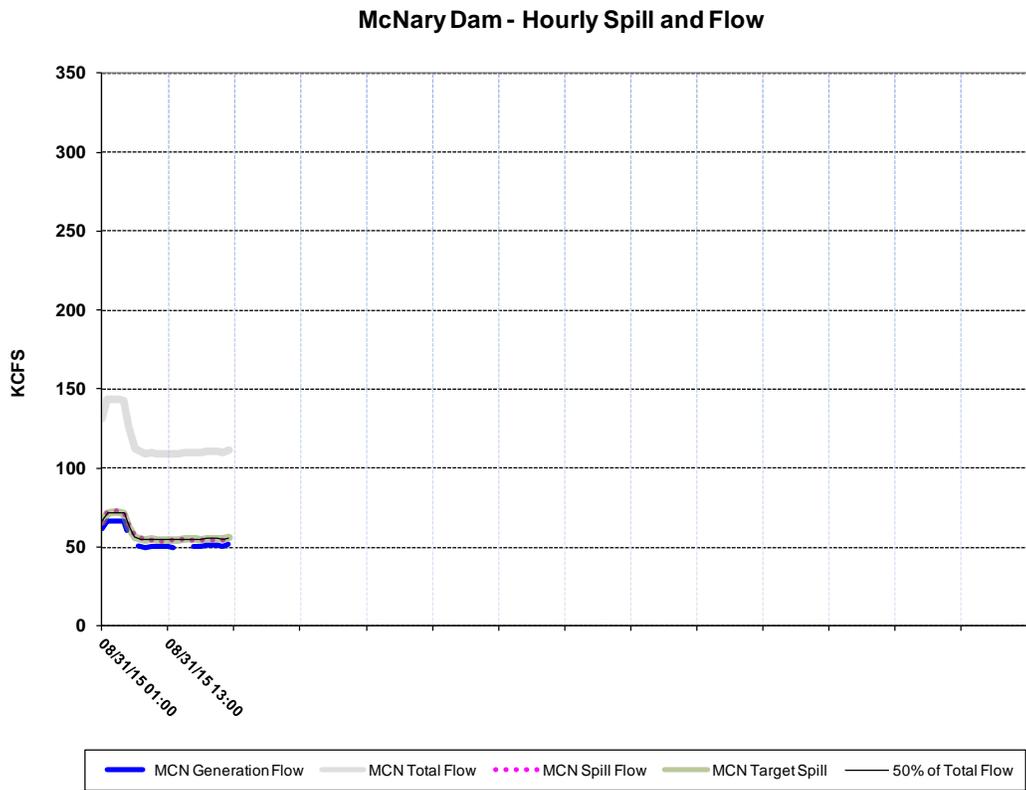
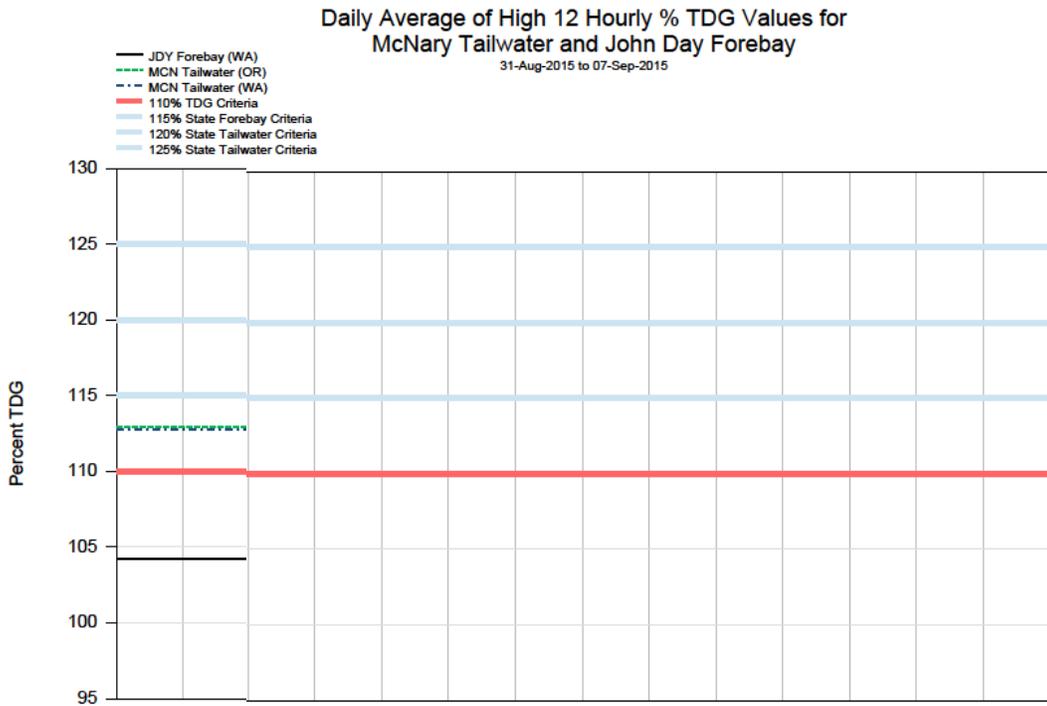
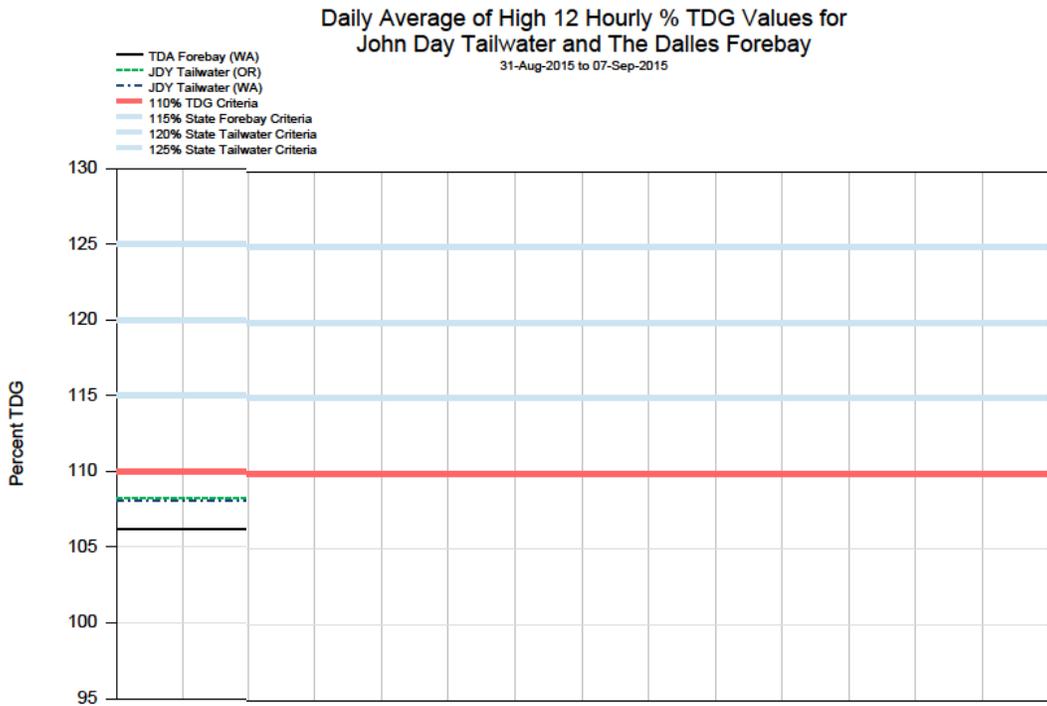


Figure 38



John Day Dam - Hourly Spill and Flow

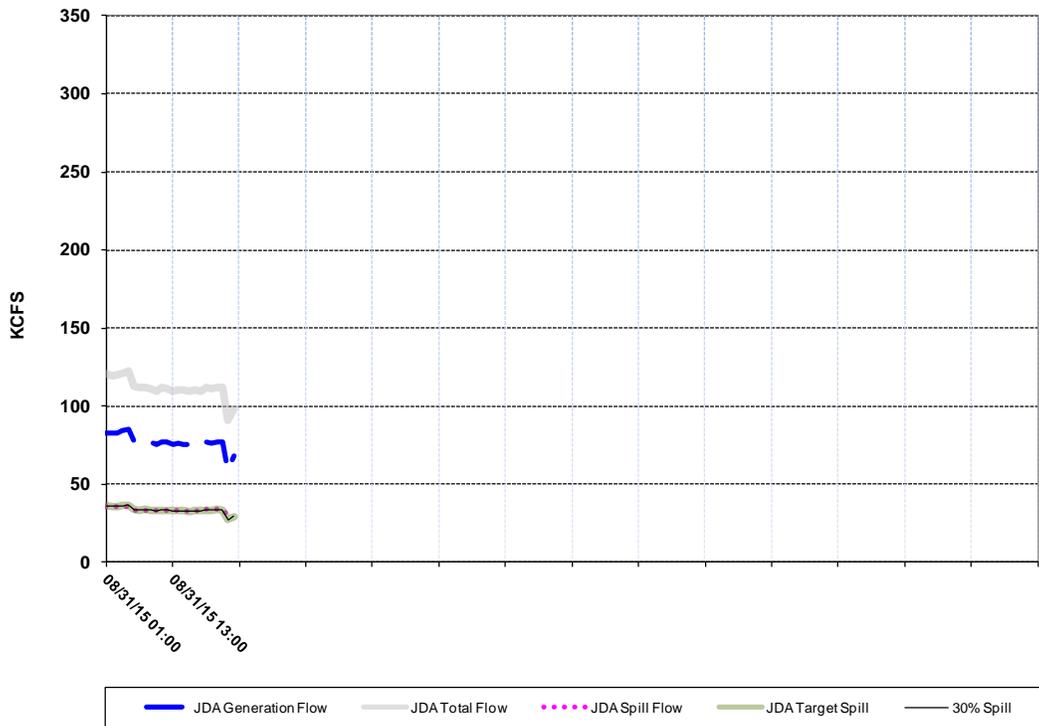


Figure 39

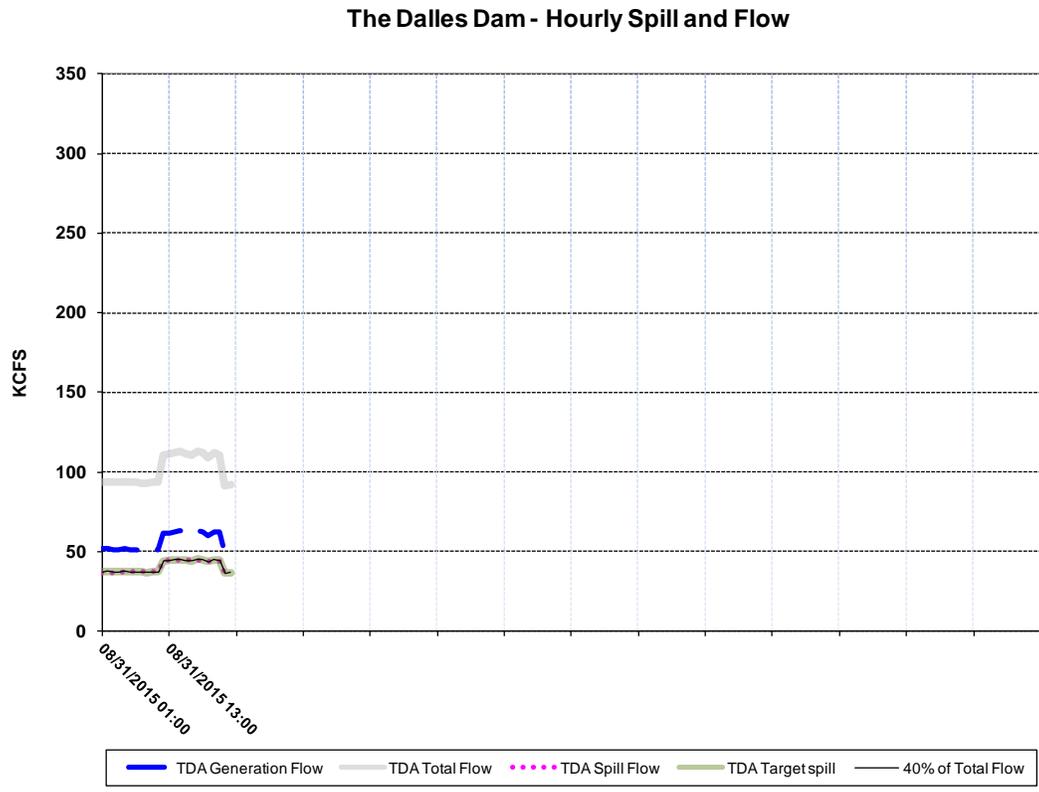
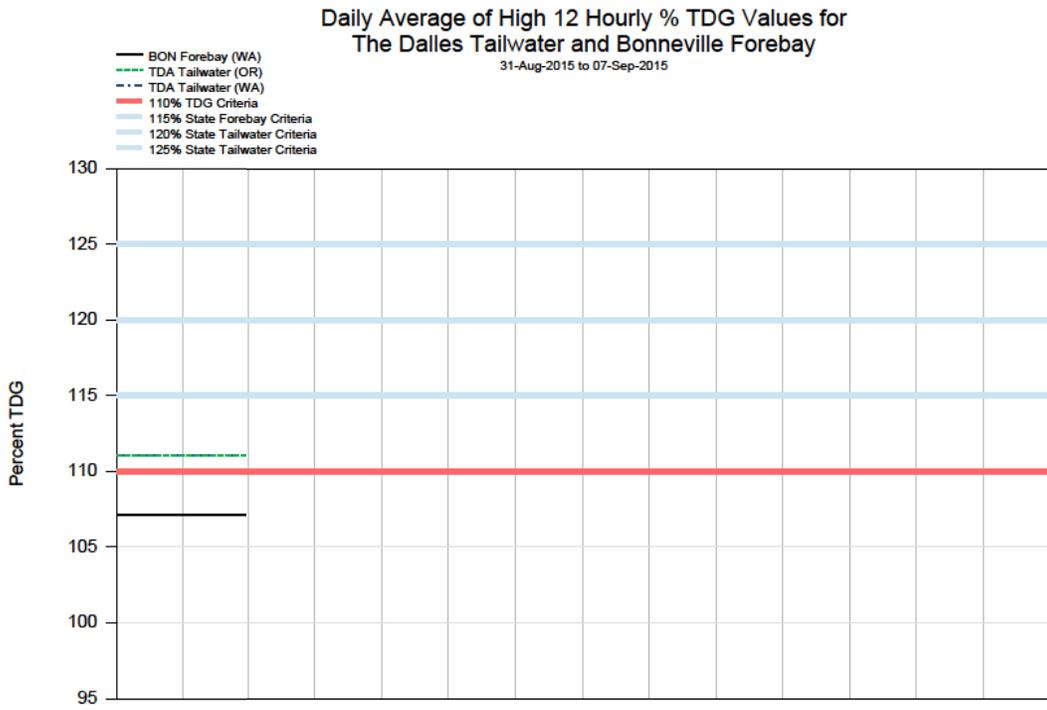


Figure 40

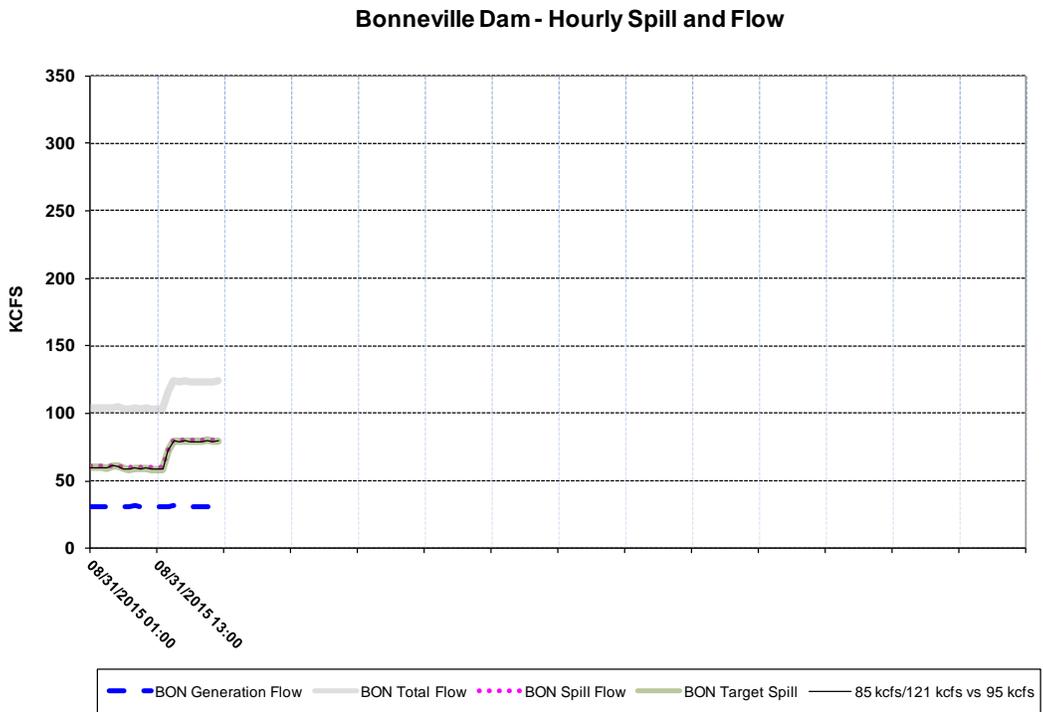
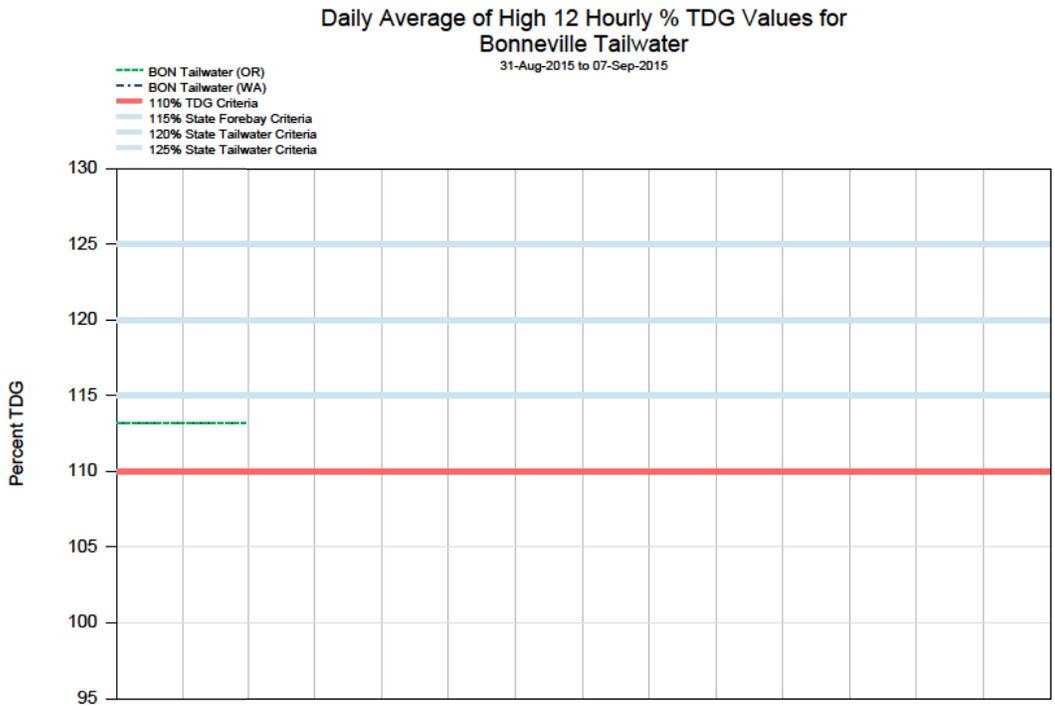


Table 2
Average Percent TDG Values For August 3 – August 31

Date	FIXED MONITORING STATIONS																			
	LWG	LGNW	LGSA	LGSW	LMNA	LMNW	IHRA	IDSW	MCNA	MCPW		JDY	JHAW		TDA	TDDO		BON	CCIW	
	WA	WA	WA	WA	WA	WA	WA	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA	WA	OR	WA
Gas Cap %	115	120	115	120	115	120	115	120	115	120	120	115	120	120	115	120	120	115	120	120
8/3/2015	103.6	111.6	104	106.1	104.7	115	113.6	113.3	111.1	112.7	113.2	105.6	107.8	108.3	107.3	111.4	112.3	108.5	113.5	113.6
8/4/2015	103	110.5	104.5	105.2	105.4	114.2	113.1	112.6	109.9	113.6	113.6	106	109.7	109.7	105.8	111.7	111.6	105.7	113.4	113.4
8/5/2015	102.5	110.6	103.6	103.7	105.6	113.1	112.4	112	109.2	114.8	114.8	106	108.3	109.5	105.6	111.3	111.6	104	113.8	113.7
8/6/2015	102	110	104.2	103.1	105.1	112.6	111.7	112	106.5	114.9	114.9	105.4	109	109	105.4	111.8	111.8	103.8	114.1	114.1
8/7/2015	102.7	109.7	105.6	103.1	106.6	112.9	111.2	110.7	106.2	115	114.9	105.8	110	109.9	109.3	114	114	106.1	117.1	117.1
8/8/2015	102.6	106.9	105.6	101.5	106	112.9	111	110.5	106.7	115.2	114.8	105.8	108.9	109.8	109.2	113.3	113.9	107.2	117.1	117.1
8/9/2015	102	105.6	104.4	100.2	104.7	109.7	109.7	110.4	106.2	113.2	114.5	104.9	107	108.2	107.1	112.2	112.7	107.5	115.9	117.1
8/10/2015	101.1	112.8	104.8	107.6	105.5	111.3	108.1	110.1	106.9	115.3	115.7	104.3	113.6	114.1	108.2	113	112.9	108.5	115.3	116.1
8/11/2015	100.7	113.9	104.8	106.6	105.9	105.8	108.7	107.5	106.7	114.5	114.9	104.8	112.9	114	108.9	113.5	113.5	109.2	115	114.9
8/12/2015	100.7	112.9	104.5	108.7	106	107.5	108.9	108.2	106.5	115	115	105.1	113.6	113.6	108.8	113.3	113.5	109.3	114	114
8/13/2015	99.8	113.4	104.3	108.7	105.9	109.8	108.9	107.8	106.9	116.4	116.4	106	113.5	113.5	108.3	112.8	113.1	108.1	115.1	115.1
8/14/2015	99.5	111.1	104.7	108.4	105.7	109.3	108.1	107.7	107	116	116.3	106	113.2	113.4	106.6	111.2	112.5	106.6	114.9	115.8
8/15/2015	99.3	109.6	103.7	107.2	103.3	109.3	104.8	110	105.2	114.2	114.2	104.2	111.2	111.7	104.2	110.3	110.3	103.8	117	116.9
8/16/2015	99.2	108.2	103.3	108.1	103.5	109.6	104.1	110.7	103.7	114.9	114.5	103.5	109.8	110.6	106	112.1	112.1	105.1	117.2	117.2
8/17/2015	99.1	104.6	104.4	107.4	103.5	107.7	103.8	110.2	103.2	115.2	115.2	103.9	107.1	109.4	108.5	113.5	113.5	107.5	116.4	117.2
8/18/2015	99.4	104.7	104.9	106.8	103.4	106.9	103.4	109.7	103.9	114.1	114.6	104.8	106.3	106.3	109.2	113.9	113.9	109.6	116.6	116.6
8/19/2015	99.9	104.8	103.9	107.1	103	106.6	102.7	106.6	105	115.8	115.8	105	114.1	114.1	109.3	114.1	114.1	111.4	117.5	117.5
8/20/2015	99.9	104.6	104	136.8	104.8	108.4	104.2	108.4	105.1	115.2	115.8	104.6	112.9	114.1	108.9	112.3	113.7	111.3	117.2	117.5
8/21/2015	99.7	104.2	102.8	111	105.2	109	104.5	108.2	104.3	114.1	115.1	103.6	112	112.6	105.4	110.1	111.4	107.3	116	117
8/22/2015	99.6	103.1	102.4	105.4	104.4	105.2	103.3	107	103.2	114.5	114.1	102.4	111.8	111.8	104.4	110.6	110.6	103.7	116	115.9
8/23/2015	103.7	104	103.6	106.5	105.2	105.2	103.8	106.9	102.8	115.4	114.9	103.5	112.7	112.7	107.7	112.6	112.6	105.2	116.9	116.9
8/24/2015	103.8	105.9	104.2	108.4	105.2	108.1	103.8	107.2	103.2	115.7	115.7	103.7	112.6	112.6	107.7	112.5	112.6	107.4	117.2	117.2
8/25/2015	99.5	105.5	103.9	107.9	102.9	109	103.6	109.4	102.3	115.8	115.8	103.1	112.8	112.8	106.7	112.6	112.6	107.4	116.4	117.2
8/26/2015	99.2	102.9	101.2	105.2	102.8	105	102.4	106.3	102.9	114.9	114.9	103	111.5	112.2	107.2	112.6	112.5	107.1	116.4	116.3
8/27/2015	---	104.4	98.9	106.8	102.7	106.6	102	107.5	103.7	115.7	115.7	103	111.5	111.5	107.2	112.4	112.5	108	117.2	117
8/28/2015	98.7	104.5	99	106.8	103.6	106.9	103.4	108	104.7	114.4	115.4	104.3	112.2	112.2	107.3	112.8	112.8	108.2	117.3	117.2
8/29/2015	99.3	104.7	103.8	107.2	104.6	107.2	104	108	105	112.8	114.3	105.4	110.1	112.1	108.3	112	112.9	109.3	115.1	117.3
8/30/2015	98.7	103.8	100	106.6	103.6	106.5	103	107	102.9	112.7	112.9	104.6	108.4	108.4	107.6	111	111.6	107.4	112.7	112.9
8/31/2015	99.3	104.3	100	106.2	102.7	105	102.2	106.9	101.5	112.9	112.8	104.2	108.2	108.1	106.3	111.1	111.1	107.2	113.4	113.4

--- denotes missing data due to gauge malfunctioning.

Note: The Oregon TDG standard modification (OR) and the Washington TDG criteria adjustments (WA) have different methodologies for calculating TDG. When the standards vary or conflict, the Corps applies the more stringent standard. TDG values are presented in Table 1 by displaying the highest value %TDG (more stringent), and the lower value is displayed with a strikethrough.

Total Dissolved Gas Monitoring Stations

Code	Station Name
LWG	Lower Granite Forebay
LGNW	Lower Granite Tailwater
LGSA	Little Goose Forebay
LGSW	Little Goose Tailwater
LMNA	Lower Monumental Forebay
LMNW	Lower Monumental Tailwater
IHRA	Ice Harbor Forebay
IDSW	Ice Harbor Tailwater
MCNA	McNary Forebay
MCPW	McNary Tailwater
JDY	John Day Forebay
JHAW	John Day Tailwater
TDA	The Dalles Forebay
TDDO	The Dalles Tailwater
BON	Bonneville Forebay
CCIW	Bonneville Tailwater (Cascade Island)
CWMW	Camas / Washougal